



## On Polynomial Space Curves with Flc-frame

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**ABSTRACT.** The first and second derivatives of a curve provide us fundamental information in the study of the behavior of curve near a point. However, if a curve is a polynomial space curve of degree  $n$ , we don't know much about the geometric meaning of the  $n$ -th derivative of the curve. There is no doubt that the Frenet frame is not suitable for this purpose because it is constructed by using first and second derivatives of a curve. On the other hand, in this paper by using a new frame called as Flc-frame we are able to give the geometric meaning of the  $n$ -th derivative of a curve. Moreover, we explore some basic concepts regarding polynomial space curves from point of view of Flc-frame in three dimensional Euclidean space.

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**Keywords:** Frenet frame, space curve, adapted frame, polynomial curve.

### 1. INTRODUCTION

As far as our knowledge the geometrical significance of the  $n$ -th order derivative of a curve does not seem to be discussed in literature. However, there is some paper which deals with geometrical interpretation of higher order derivatives of a curve. For instance, the geometrical significance of the third derivative of a curve is discussed in [11]. The third derivative is represented geometrically in terms of the quantity called aberrancy, which measures the asymmetry of a curve about its normal [12]. But, one can ask, what exactly prevented us from accomplishing geometrical significance of the  $n$ -th order derivative of a curve. The major difficulty arises from the fact that we can not write the  $n$ -th order derivative of a curve in term of Frenet frame. It is clear that the Frenet frame is not suitable for the investigation of the geometric interpretation of higher order derivatives of a curve. On the other hand by using the Flc-frame which is constructed by using the higher order derivatives of the curve, we are able to give geometric interpretation of  $n$ -th order derivatives of a curve.

Bishop [2] showed that apart from the Frenet frame, we can construct more frame along a space curve. His approach is based on rotating the Frenet frame by an angle [7, 14]

$$\theta = - \int \tau \|\alpha'(t)\| dt.$$

Despite the fact that Bishop frame is more suitable for applications [8], this frame is not an analytic frame [4]. Recently, Dede introduced a new frame along a polynomial space curve, called as Flc-frame. The computation of Flc-frame is easier than the both Frenet and Bishop frames. Moreover, the Flc-frame has less singular points than the Frenet frame. Therefore, the Flc-frame can be considered as an effective alternative to the RMF. Discussion of the Flc-frame and its

application to the tube surfaces can be found in [3]. Moreover, for some of the recent researchs about the Flc-frame, see [1, 9, 13].

Let  $\alpha(t)$  be a polynomial space curve of degree  $n$ . The Flc-frame is given by

$$\mathbf{t} = \frac{\alpha'}{\|\alpha'\|}, \mathbf{D}_1 = \frac{\alpha' \wedge \alpha^{(n)}}{\|\alpha' \wedge \alpha^{(n)}\|}, \mathbf{D}_2 = \mathbf{D}_1 \wedge \mathbf{t}, \tag{1.1}$$

where the prime ' indicates the differentiation with respect to  $t$  [3]. If the order of derivative exceeds three, we replaced prime by the superscript  $(n)$ , such as  $\alpha^{''''} = \alpha^{(4)}$ . The new vectors  $\mathbf{D}_1$  and  $\mathbf{D}_2$  are called as binormal-like vector and normal-like vector, respectively.

The local rate of change of the Flc-frame called as the Frenet-like formulas can be expressed in the following form

$$\begin{bmatrix} \mathbf{t}' \\ \mathbf{D}_2' \\ \mathbf{D}_1' \end{bmatrix} = \nu \begin{bmatrix} 0 & d_1 & d_2 \\ -d_1 & 0 & d_3 \\ -d_2 & -d_3 & 0 \end{bmatrix} \begin{bmatrix} \mathbf{t} \\ \mathbf{D}_2 \\ \mathbf{D}_1 \end{bmatrix}, \tag{1.2}$$

where  $\|\alpha'\| = \nu$ .

We may define three new invariants of the curve by

$$d_1 = \frac{\langle \mathbf{t}', \mathbf{D}_2 \rangle}{\nu}, d_2 = \frac{\langle \mathbf{t}', \mathbf{D}_1 \rangle}{\nu}, d_3 = \frac{\langle \mathbf{D}_2', \mathbf{D}_1 \rangle}{\nu}. \tag{1.3}$$

**Theorem 1.1** ([3]). *A polynomial space curve is a straight line if and only if the all of the curvatures vanish identically,  $d_1 = d_2 = d_3 = 0$ .*

**Theorem 1.2** ([3]). *A polynomial space curve with the curvature  $d_1 \neq 0$  is planar if and only if the curvatures  $d_2$  and  $d_3$  vanish identically,  $d_2 = d_3 = 0$ .*

The Darboux vector of a frame also known as angular velocity is a crucial information to understand the behaviour of the frame. The Darboux vector  $\mathbf{d}_F = \tau \mathbf{t} + \kappa \mathbf{b}$  of Frenet frame describes the instantaneous rate of change of each of the vectors of Frenet frame at a given instant [5]. Therefore, the instantaneous angular speed satisfies  $\|\mathbf{d}_F\| = \sqrt{\tau^2 + \kappa^2}$ . The RMF is characterized by the fact that the Darboux vector  $\mathbf{d}_{RMF}$  of RMF satisfies  $\langle \mathbf{d}_{RMF}, \mathbf{t} \rangle = 0$ , that is, the normal-plane vectors have no instantaneous rotation around the tangent vector [10].

## 2. FLC-FRAME ALONG A POLYNOMIAL SPACE CURVE

In this chapter, we begin an investigation into the local theory of space curves by using the Flc-frame. Then, we obtain new formulas for calculating the three curvatures  $d_1, d_2$  and  $d_3$  of the curve.

**Theorem 2.1.** *Let  $\alpha(t)$  be a polynomial space curve of degree  $n$ . The curvatures  $d_1, d_2$  and  $d_3$  of the curve can be computed as*

$$d_1 = \frac{\langle \alpha' \wedge \alpha'', \alpha' \wedge \alpha^{(n)} \rangle}{\|\alpha'\|^3 \|\alpha' \wedge \alpha^{(n)}\|}, d_2 = \frac{\det[\alpha'', \alpha', \alpha^{(n)}]}{\|\alpha'\|^2 \|\alpha' \wedge \alpha^{(n)}\|} \tag{2.1}$$

and

$$d_3 = \frac{\det[\alpha', \alpha'', \alpha^{(n)}] \langle \alpha', \alpha^{(n)} \rangle}{\|\alpha'\|^2 \|\alpha' \wedge \alpha^{(n)}\|^2}. \tag{2.2}$$

*Proof.* In order to find the curvature  $d_1$ , we first differentiate the unit tangent vector  $\mathbf{t}$  in (1.1), then by substituting result in (1.3), we get

$$d_1 = \frac{\langle \alpha'', (\alpha' \wedge \alpha^{(n)}) \wedge \alpha' \rangle}{\|\alpha'\|^3 \|\alpha' \wedge \alpha^{(n)}\|}.$$

By using the vector triple product  $(\mathbf{a} \wedge \mathbf{b}) \wedge \mathbf{c} = -\mathbf{a} \langle \mathbf{b}, \mathbf{c} \rangle + \mathbf{b} \langle \mathbf{a}, \mathbf{c} \rangle$  gives

$$d_1 = \frac{\|\alpha'\|^2 \langle \alpha'', \alpha^{(n)} \rangle - \langle \alpha'', \alpha' \rangle \langle \alpha', \alpha^{(n)} \rangle}{\|\alpha'\|^3 \|\alpha' \wedge \alpha^{(n)}\|}. \tag{2.3}$$

Thus, from the Lagrange’s identity, it follows that

$$d_1 = \frac{\langle \alpha' \wedge \alpha'', \alpha' \wedge \alpha^{(n)} \rangle}{\|\alpha'\|^3 \|\alpha' \wedge \alpha^{(n)}\|}.$$

Similar to the previous case, by using a direct computation one can obtain the curvature  $d_2$  as follows

$$d_2 = \frac{\det[\alpha'', \alpha', \alpha^{(n)}]}{\|\alpha'\|^2 \|\alpha' \wedge \alpha^{(n)}\|}.$$

From (1.1) and (1.3), we have

$$d_3 = \frac{\langle \mathbf{D}'_2, \mathbf{D}_1 \rangle}{\|\alpha'\|} = \frac{\langle \mathbf{D}'_1 \wedge \mathbf{t}, \mathbf{D}_1 \rangle}{\|\alpha'\|}.$$

From which the curvature  $d_3$  is given by

$$d_3 = \frac{\langle \mathbf{D}'_1 \wedge \alpha', \alpha' \wedge \alpha^{(n)} \rangle}{\|\alpha'\|^2 \|\alpha' \wedge \alpha^{(n)}\|},$$

and therefore using Lagrange’s identity, we can establish the following formula

$$d_3 = \frac{\langle \mathbf{D}'_1, \alpha' \rangle \langle \alpha', \alpha^{(n)} \rangle - \langle \mathbf{D}'_1, \alpha^{(n)} \rangle \langle \alpha', \alpha' \rangle}{\|\alpha'\|^2 \|\alpha' \wedge \alpha^{(n)}\|}. \tag{2.4}$$

On the other hand, by differentiating  $\mathbf{D}_1$  in (1.1), we have

$$\mathbf{D}'_1 = \frac{(\alpha'' \wedge \alpha^{(n)} + \alpha' \wedge \alpha^{(n+1)})}{\|\alpha' \wedge \alpha^{(n)}\|} - \frac{\|\alpha' \wedge \alpha^{(n)}\|' (\alpha' \wedge \alpha^{(n)})}{\|\alpha' \wedge \alpha^{(n)}\|^2}. \tag{2.5}$$

Note that the  $n + 1$ -th derivative of the curve vanishes therefore by substituting (2.5) into (2.4), we get

$$d_3 = \frac{\det[\alpha', \alpha'', \alpha^{(n)}] \langle \alpha', \alpha^{(n)} \rangle}{\|\alpha'\|^2 \|\alpha' \wedge \alpha^{(n)}\|^2}.$$

□

Thus, we state the following fundamental corollary.

**Corollary 2.2.** *The curvatures  $d_1, d_2$  and  $d_3$  of the Flc-frame can be computed directly from the parametric curve.*

**Theorem 2.3.** *The new curvatures  $d_1, d_2$  and  $d_3$  of the curve does not depend on the parameter representation of the curve. Thus, the curvatures form a complete system of differential invariants.*

*Proof.* Let  $\beta(t)$  be a space curve of degree  $n$  with curvature  $d_1$  and let  $\alpha(s) = \beta(\phi(t))$  be an another parametrization of the same curve with curvature  $\tilde{d}_1$ . Without loss of generality, we can choose  $\phi(t) = s^m$ . Since the degree of the curve  $\alpha$  is  $n + m$ , we need to calculate the  $(n+m)$ -th derivative.

The first three derivatives of  $\alpha$  are evaluated as follows:

$$\alpha' = \beta'(\phi)\phi', \tag{2.6}$$

$$\alpha'' = \beta''(\phi)\phi'^2 + \beta'(\phi)\phi'', \tag{2.7}$$

$$\alpha''' = \beta'''(\phi)\phi'^3 + 3\beta''(\phi)\phi'\phi'' + \beta'(\phi)\phi'''. \tag{2.7}$$

Similarly,  $n$ -th derivative of the curve  $\alpha$  is obtained by

$$\alpha^{(n)} = \beta^{(n)}(\phi)\phi'^m + \frac{n(n-1)}{2}\beta^{(n-1)}(\phi)\phi'^{m-2}\phi'' \dots + \beta'(\phi)\phi^{(n)}.$$

Differentiating again  $\alpha^{(n)}$ , then using  $\beta^{(n+1)} = (0, 0, 0)$ , we have

$$\alpha^{(n+1)} = n\beta^{(n)}(\phi)\phi'^{m-1}\phi' + \frac{(n+1)n}{2}\beta^{(n)}(\phi)\phi'^{m-1}\phi'' + \dots + \beta'(\phi)\phi^{(n+1)}.$$

Similarly differentiating up to order  $m+n$  and using  $\phi^{(n+m)} = 0$  gives

$$\alpha^{(n+m)} = \delta\beta^{(n)}(\phi), \tag{2.8}$$

where

$$\delta = ([n(n - 1) \dots (n - m + 1)]\phi^{m-m}\phi^m + n\phi^{m-1}\phi^{(m)} + \dots).$$

Substituting (2.6), (2.7) and (2.8) into (2.1) gives

$$\tilde{d}_1 = \frac{\phi'^4 \delta \langle \beta'(\phi) \wedge \beta''(\phi), \beta'(\phi) \wedge \beta^{(n)}(\phi) \rangle}{\phi'^4 \delta \|\beta'(\phi)\| \|\beta'(\phi) \wedge \beta''(\phi), \beta'(\phi) \wedge \beta^{(n)}(\phi)\|} \Bigg|_t,$$

which implies that

$$\tilde{d}_1 = \frac{\langle \beta' \wedge \beta'', \beta' \wedge \beta^{(n)} \rangle}{\|\beta'\| \|\beta' \wedge \beta'', \beta' \wedge \beta^{(n)}\|} \Bigg|_{\phi(t)} = d_1 \circ \phi(t).$$

The proof of the invariance of the curvatures  $d_2$  and  $d_3$  are similar. □

For example, let us consider the curve given by

$$\beta(t) = (t, t^2, t^3).$$

The curvature  $d_1$  is obtained by

$$d_1 = \frac{12t^3 + 6t}{\sqrt{4t^2 + 1(9t^4 + 4t^2 + 1)^{3/2}}}.$$

For  $\phi(t) = s^2$ , we have another curve given by

$$\alpha(s) = (s^2, s^4, s^6).$$

Now,  $\alpha(s)$  is a curve of degree six. Then, the curvature  $\tilde{d}_1$  is obtained by

$$\tilde{d}_1 = \frac{12s^6 + 6s^2}{\sqrt{4s^4 + 1(9s^8 + 4s^4 + 1)^{3/2}}}.$$

It is easy to see that  $\tilde{d}_1 = d_1 \circ \phi(t)$ .

**Corollary 2.4.** *Let  $\alpha(t)$  be a polynomial space curve of degree  $n$ . Apart from the Frenet frame, there are  $(n - 2)$  type frames which can be obtained by using this method. For example, we can obtain a new binormal vector by using the first and third derivatives of the curve. But, there is just one frame (Flc-frame) which is invariant under the reparameterization of the curve.*

**Corollary 2.5.** *If the degree of polynomial space curve is two, then the Flc-frame coincides with the Frenet frame with curvatures  $d_1 = \kappa, d_2 = 0$  and  $d_3 = \tau = 0$ .*

**Theorem 2.6.** *Let  $\alpha(t)$  be a polynomial space curve of degree  $n$ . The relation between curvatures  $d_1, d_2$  and  $d_3$  of the Flc-frame is obtained by*

$$-\frac{\left(\frac{d_3}{d_2}\right)'}{1 + \left(\frac{d_3}{d_2}\right)^2} = \nu d_1.$$

*Proof.* Let  $\psi$  be an Euclidean angle between the normal-like vector  $\mathbf{D}_2$  and the  $n$ -th derivative of the curve  $\alpha^{(n)}$ , shown in Figure 1, then we have

$$\langle \alpha^{(n)}, \mathbf{D}_2 \rangle = \|\alpha^{(n)}\| \cos \psi. \tag{2.9}$$

From (1.1) we see that, the vectors  $\alpha^n$  and  $\mathbf{D}_1$  are orthogonal and so

$$\langle \alpha^{(n)}, \mathbf{t} \rangle = \|\alpha^{(n)}\| \sin \psi, \tag{2.10}$$

which implies that

$$\langle \alpha^{(n)}, \alpha' \rangle = \nu \|\alpha^n\| \sin \psi. \tag{2.11}$$

Combining (2.1), (2.2) and (2.10), we have

$$\frac{d_3}{d_2} = -\frac{\langle \alpha', \alpha^{(n)} \rangle}{\|\alpha' \wedge \alpha^{(n)}\|} = -\tan \psi. \tag{2.12}$$

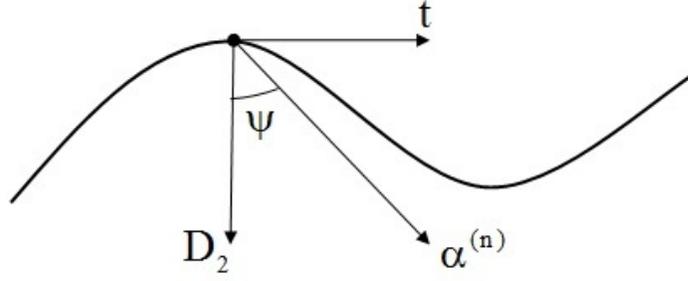


FIGURE 1. The angle between the vectors  $\mathbf{D}_2$  and  $\alpha^{(n)}$ .

It follows that,

$$\psi = \arctan\left(-\frac{d_3}{d_2}\right),$$

and differentiating the above equation yields

$$d\psi = -\frac{\left(\frac{d_3}{d_2}\right)'}{1 + \left(\frac{d_3}{d_2}\right)^2}. \tag{2.13}$$

On the other hand by using  $\alpha' = v\mathbf{t}$  and  $\alpha'' = v'\mathbf{t} + v^2(d_1\mathbf{D}_2 + d_2\mathbf{D}_1)$ , we have

$$\langle \alpha'', \alpha' \rangle = v'v. \tag{2.14}$$

Differentiating (2.11) yields

$$\langle \alpha'', \alpha^{(n)} \rangle = v' \|\alpha^n\| \sin \psi + v \|\alpha^n\| \cos \psi d\psi. \tag{2.15}$$

Substituting (2.10), (2.14) and (2.15) into (2.3) gives

$$d_1 = \frac{d\psi}{v}. \tag{2.16}$$

Combining (2.13) and (2.16), we have the desired formula.  $\square$

**Theorem 2.7.** Let  $\alpha(t)$  be a polynomial space curve of degree  $n$ . The  $n$ -th derivative of curve can be written in term of the basis  $\{\mathbf{t}, \mathbf{D}_1, \mathbf{D}_2\}$  in the following form

$$\alpha^{(n)}(t) = \|\alpha^{(n)}\| (\sin \psi \mathbf{t} + \cos \psi \mathbf{D}_2),$$

where  $\psi = \int d_1 v dt$ .

*Proof.* By using (2.9) and (2.10) the  $n$ -th derivative of the curve can be written as

$$\alpha^{(n)}(t) = \|\alpha^n\| (\sin \psi \mathbf{t} + \cos \psi \mathbf{D}_2.) \tag{2.17}$$

By differentiating (2.17) with respect to  $t$  gives

$$\mathbf{t} \cos \psi (d\psi - vd_1) + \mathbf{D}_2 \sin \psi (vd_1 - d\psi) + \mathbf{D}_1 (\sin \psi vd_2 + \cos \psi vd_3) = 0.$$

Since the vectors  $\mathbf{t}, \mathbf{D}_2$  and  $\mathbf{D}_1$  are linearly independent, the above equation is satisfied if and only if

$$\begin{cases} d\psi - vd_1 & = & 0 \\ v \sin \psi d_2 + v \cos \psi d_3 & = & 0. \end{cases} \tag{2.18}$$

From (2.12), we have  $\sin \psi d_2 + \cos \psi d_3 = 0$ , therefore the solution of the equation (2.18) is  $d\psi - vd_1 = 0$ , that is

$$\psi = \int d_1 v dt.$$

In addition, the tangential  $\alpha_T^{(n)}$  and normal  $\alpha_N^{(n)}$  components of the  $n$ -th derivative of the curve  $\alpha^{(n)}$  can be written as

$$\alpha^{(n)}(t) = \alpha_T^{(n)}(t)\mathbf{t} + \alpha_N^{(n)}(t)\mathbf{D}_2,$$

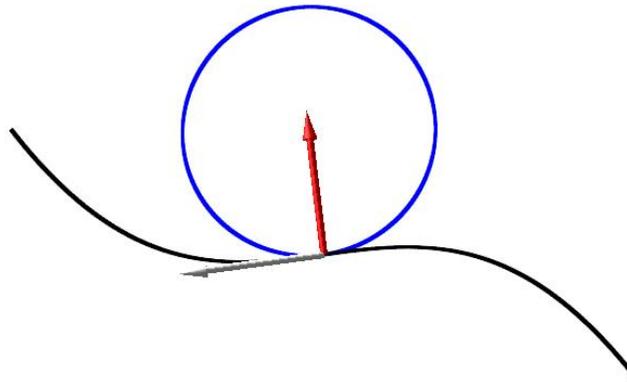


FIGURE 2. The circle (blue) has the same tangent (grey) and normal-like vector (red) with the curve (black).

where

$$\alpha_T^{(n)}(t) = \frac{\|\alpha' \wedge \alpha^{(n)}\|}{\|\alpha'\|}, \alpha_N^{(n)}(t) = \frac{\langle \alpha', \alpha^{(n)} \rangle}{\|\alpha'\|}.$$

Note that, a osculating-like plane of a curve  $\alpha(t)$  at point  $t_0$  is the plane spanned by  $\mathbf{t}(t_0)$  and  $\mathbf{D}_2(t_0)$  with normal vector  $\mathbf{D}_1(t_0)$ . The equation of osculating-like plane is given by

$$\langle X - \alpha(t_0), \mathbf{D}_1(t_0) \rangle = 0.$$

It follows that

$$\left[ X - \alpha(t_0), \alpha'(t_0), \alpha^{(n)}(t_0) \right] = 0,$$

where  $X = (x, y, z)$  is the coordinate system. □

Now we can give the geometric meaning of the  $n$ -th derivative of a polynomial space curve of degree  $n$ .

**Theorem 2.8.** Let  $\alpha(t) : I \rightarrow R^3$  be a polynomial space curve of degree  $n$ . A new circle  $\beta(\psi)$  with radius  $\|\alpha^{(n)}\|$  can be parametrized by

$$\beta(\psi) = p_0 - \|\alpha^{(n)}\| (\sin(\psi)\mathbf{t}(t_0) + \cos(\psi)\mathbf{D}_2(t_0)) \tag{2.19}$$

in the osculating-like plane of the curve at the point  $t_0 \in I$  and the center of the circle  $p_0$  is given by

$$p_0 = \alpha(t_0) + \|\alpha^{(n)}\| \mathbf{D}_2(t_0)$$

In Figure 2, the circle has the same tangent and normal-like vectors with the curve at the point  $t_0$ .

*Proof.* If  $\psi = 0$ , then we have  $\beta(0) = p_0 - \|\alpha^{(n)}\| \mathbf{D}_2(t_0) = \alpha(t_0)$  which implies

$$p_0 = \alpha(t_0) + \|\alpha^{(n)}\| \mathbf{D}_2(t_0).$$

Differentiating (2.19) with respect to  $\psi$  gives

$$\beta'(\psi) = -\|\alpha^{(n)}\| (d\psi \cos(\psi)\mathbf{t}(t_0) + d\psi \sin(\psi)\mathbf{D}_2(t_0)),$$

which implies that the tangent vector  $\mathbf{t}_\beta$  of the circle coincides with the tangent vector of the curve as follows

$$\mathbf{t}_\beta(0) = \frac{\beta'(0)}{\|\beta'(0)\|} = \mathbf{t}(t_0),$$

and this concludes that the curve and circle have the common normal-like vector  $\mathbf{D}_2(t_0)$ . □

Note that, the new circle is the unique circle which passes through  $t_0$ , has the same tangent in  $t_0$  as  $\alpha$  as well as the same curvature  $d_1$ , and whose center lies in the direction of the unit normal-like vector.

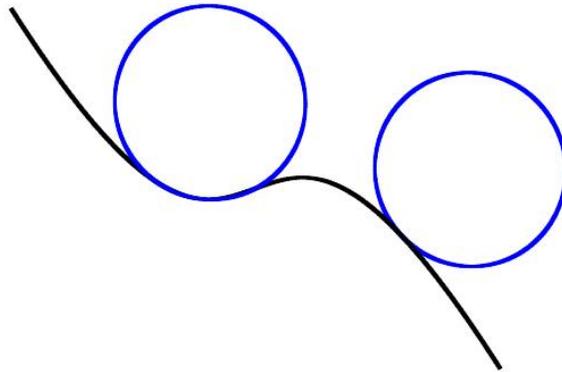
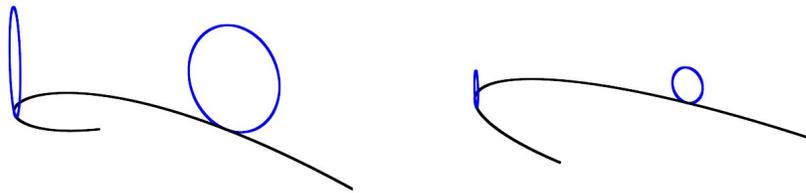


FIGURE 3. The curve  $\alpha(t) = (t, t, t^3/10)$  with two circles at the points  $t_0 = -1.3$  and  $t_0 = 0.9$



(a) The curve  $a(t) = (t, t^2, t^3/10)$  with circles. (b) The curve  $a(t) = (t, t^2, t^3/30)$  with circles.

FIGURE 4. The circles at the points  $t=-1.3$  and  $t=0.9$ . The effect of of leading coefficients.

**Corollary 2.9.** Let  $\alpha(t)$  be a polynomial space curve of degree  $n$  parametrized by

$$\alpha(t) = \left( \sum_{i=0}^n a_i t^i, \sum_{i=0}^n b_i t^i, \sum_{i=0}^n c_i t^i \right),$$

where  $a_i, b_i$  and  $c_i$  are coefficients.

The circle  $\beta(\psi)$  can be characterized by the following properties:

- Since the radius of the circle is  $\|\alpha^{(n)}\| = n!c$  where  $c = \sqrt{a_n^2 + b_n^2 + c_n^2}$ , the radius of the circle is constant. Figure 3 demonstrated that just the position of the circle changes when the circle moves along the curve.
- The radius of the circle is just depend on leading coefficients  $a_n, b_n$  or  $c_n$  and degree of the curve.
- This circle is a global property of polynomial space curves. For the curves have the same degree, if  $c$  decreases then the radius of the circle decreases. The Figure 4 demonstrates that if  $c$  decrease then the curve approximates the osculating-like plane.

**Theorem 2.10.** The Darboux vector  $\mathbf{d}_{Flc}$  of the Flc-frame can be obtained as in the following form

$$\mathbf{d}_{Flc} = v(d_3 \mathbf{t} - d_2 \mathbf{D}_2 + d_1 \mathbf{D}_1).$$

*Proof.* The variation of the Flc-frame in terms of its Darboux vector  $\mathbf{d}_{Flc}$  can be written as

$$\mathbf{t}' = \mathbf{d}_{Flc} \wedge \mathbf{t}, \mathbf{D}'_2 = \mathbf{d}_F \wedge \mathbf{D}_2, \mathbf{D}'_1 = \mathbf{d}_F \wedge \mathbf{D}_1. \tag{2.20}$$

Since  $\{\mathbf{t}, \mathbf{D}_2, \mathbf{D}_1\}$  are mutually orthogonal, they form a basis for the vector fields along. Hence, there exist functions  $a, b, c$  such that

$$\mathbf{d}_{Flc} = a\mathbf{t} + b\mathbf{D}_2 + c\mathbf{D}_1. \tag{2.21}$$

Thus, from (1.2), (2.20) and (2.21) we have

$$\mathbf{d}_{Flc} = v(d_3 \mathbf{t} - d_2 \mathbf{D}_2 + d_1 \mathbf{D}_1).$$

□

It is easy to see that, the Darboux vector  $\mathbf{d}_{Flc}$  of the Flc-frame does not satisfy  $\langle \mathbf{d}_{Flc}, \mathbf{t} \rangle = 0$ , therefore it is not a RMF.

Thus, the instantaneous angular speed of the Flc-frame is calculated as follows

$$\|\mathbf{d}_{Flc}\| = v \sqrt{d_1^2 + d_2^2 + d_3^2}.$$

In this section we will compare the angular speed of the frames: Frenet  $\|\mathbf{d}_F\| = v \sqrt{\tau^2 + \kappa^2}$ , Bishop  $\|\mathbf{d}_B\| = v \sqrt{\kappa^2}$  and Flc-frame  $\|\mathbf{d}_{Flc}\| = v \sqrt{d_1^2 + d_2^2 + d_3^2}$ .

**Example 2.11.** Let us consider a curve given by

$$\alpha(t) = (2t, t^2, t^3).$$

In Figure 5, we are able to compare the instantaneous angular speed of the Flc-frame against two standard methods of curve framing: the RMF and the Frenet frame.

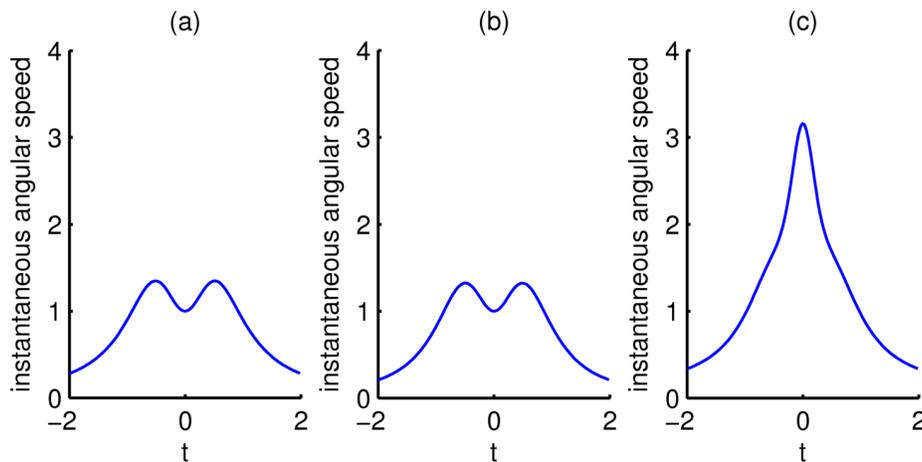


FIGURE 5. Comparison of the instantaneous angular speed of the Flc-frame (left), RMF (center) and the Frenet frame (right).

Observe that although the Flc-frame is not rotation-minimizing frame with respect to  $\mathbf{t}$ , there is almost no difference between the instantaneous angular speeds of the frames: the RMF and the Flc-frame.

### 3. CONCLUSION

In this paper we propose a new method to examine the geometric meaning of the  $n$ -th derivative of a polynomial space curve of degree  $n$ . Summarizing, the norm of  $n$ -th derivative of a polynomial space curve of degree  $n$  is a radius of a circle in the osculating-like plane of the curve.

### CONFLICTS OF INTEREST

The author declares that there are no conflicts of interest regarding the publication of this article.

### AUTHORS CONTRIBUTION STATEMENT

The author has read and agreed to the published version of the manuscript.

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