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# An Adroit Randomized Response New Additive Scrambling Model

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# ABSTRACT

In this paper, an improved new additive model has been proposed. The proposed model is found to be more efficient than the randomized response models studied by Gjestvang and Singh (2009) and Singh (2010). The relative efficiency of the proposed model has been studied with respect to the Gjestvang and Singh (2009) and Singh (2010) model. It is found that the envisaged model is superior to those additive models earlier considered by Gjestvang and Singh (2009) and Singh (2010).Numerical illustrations are also given in support of the present study. **Key Words**: Randomized response sampling, Estimation of proportion, sensitive quantitative variable.

## **1. INTRODUCTION**

Warner (1965) was first to introduce a randomized response (RR) model to estimate proportion for sensitive attributes including sexual orientation, criminal activity, child abuse, suicidal tendency in teenagers, all cases of AIDS, abortion or drug addiction, such that the respondent's privacy should be protected. Some recent contribution to randomized response sampling is given by Fox and Tracy (1986), Singh and Mathur (2004, 2005), Gjestvang and Singh (2006,

2009), Gupta et al. (2010,2012) and Singh and Tarray (2013, 2014, 2015). We below give the description of the models due toGjestvang and Singh (2009) and Singh (2010) additive models:

## 1.1 Gjestvang and Singh (2009) additive model:

Let  $\alpha$  and  $\beta$  be two known positive real numbers. Then Gjestvang and Singh (2009) proposed an additive model in which each respondent in the sample is requested to

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draw a card secretly from a well – shuffled deck of cards. In the deck, let P be the proportion of cards bearing the statement, "Multiply scrambling variable S with  $\alpha$  and add to the real value of the sensitive variable Y<sub>i</sub>", and (1-P) be the proportion of cards bearing the statement, "Multiply scrambling variable S with  $\beta$  and subtract it from the real value of the sensitive variable Y<sub>i</sub>". Mathematically, each respondent is requested to report the scrambled response Z<sub>i</sub> as:

$$\begin{split} Z_i = \begin{cases} Y_i + \alpha S & \text{ with probabilit y } P = \beta/(\alpha + \beta) \\ Y_i - \beta S & \text{ with probabilit y } (1 - P) = \alpha/(\alpha + \beta) \end{cases} \tag{1.1} \end{split}$$

Gjestvang and Singh (2009) defined an unbiased estimator of the population mean  $\mu_{Y}$  as

$$\hat{\mu}_{GS} = \frac{1}{n} \sum_{i=1}^{n} Z_i$$
(1.2)

and the variance of  $\mu_{Y}$  is given by

$$V(\hat{\mu}_{GS}) = \frac{1}{n} \left[ \sigma_y^2 + \alpha \beta (\theta^2 + \gamma^2) \right]$$
(1.3)

# 1.2 Singh (2010) additive model:

Suppose there are k scrambling variables denoted by  $S_j$ ,  $j = 1, 2, \ldots, k$  whose mean  $\theta_j$  (i.e.  $E(S_j) = \theta_j$ ) and variance  $\gamma_j^2$  (i.e.  $V(S_j) = \gamma_j^2$ ) are known. In Singh (2010) proposed optimal new orthogonal additive model named as (POONAM), each respondent selected in the sample is requested to rotate a spinner, as shown in Fig. 1, in which the proportion of the k shaded areas, say  $P_1, P_2, \ldots P_k$  are orthogonal to the means of the k

scrambling variables, say  $\theta_1, \theta_2, \dots, \theta_k$  such that:

$$\sum_{j=1}^{k} P_j \theta_j = 0 \tag{1.4}$$

and

$$\sum_{j=1}^{k} \mathbf{P}_j = 1 \tag{1.5}$$

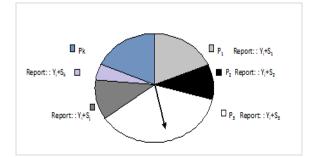


Fig. 1 Spinner for POONAM (Singh (2010))

Now if the pointer stops in the  $j^{th}$  shaded area, then the  $i^{th}$  respondent with real value of the sensitive variable, say  $Y_i$ , is requested report the scrambled response  $Z_i$  as:

$$Z_i = Y_i + S_i \tag{1.6}$$

Assuming that the sample of size n is drawn from the population using simple random sampling with replacement (SRSWR).Singh (2010) suggested an

unbiased estimator of the population mean  $\mu_{Y}$  as

$$\hat{\mu}_{Y} = \frac{1}{n} \sum_{j=1}^{k} Z_{j}$$

$$(1.7)$$

The variance of  $\mu_{Y}$  is given by

$$V(\hat{\mu}_{Y}) = \frac{1}{n} \left[ \sigma_{y}^{2} + \sum_{j=1}^{k} P_{j}(\theta_{j}^{2} + \gamma_{j}^{2}) \right]$$
(1.8)

## 2. The proposed procedure

It is to be noted that the mean  $\theta_j$  and variance  $\gamma_j^2$  of the j<sup>th</sup> scrambling variable  $S_j$  (j=1,2,...,k) are known. But these information's have not utilized by the previous authors in building up the randomization models. It is possibility that the use of the prior information regarding the parameters of the scrambling variable  $S_j$  may improve the efficiency of the randomized response model. This led authors to propose a new additive model based on standardized scramblingvariable

$$S_{j}^{*} = \left(\frac{S_{j} - \theta_{j}}{\gamma_{j}}\right), j = 1, 2, ..., k \text{ whose mean is "zero" (i.e.}$$
$$E(S_{i}^{*}) = 0) \text{ and the variance is "unity" (i.e. V(S_{i}^{*}) = 1).}$$

Then in the proposed additive model, each respondent selected in the sample is requested to rotate a spinner, as demonstrated in Fig. 2, in which the proportion of the k shaded areas, say  $P_1, P_2, \dots P_k$  such that:

$$\sum_{j=1}^{k} \mathbf{P}_{j} = 1 \tag{2.1}$$

Now if the pointer stops in the j<sup>th</sup> shaded area, then the i<sup>th</sup> respondent with real value of the sensitive variable, say  $Y_i$ , is requested report the scrambled response  $Z_{i \text{ as:}}^*$ 

$$\mathbf{Z}_{i}^{*} = \mathbf{Y}_{i} + \mathbf{S}_{j}^{*} \tag{2.2}$$

Let a sample of size n be drawn from the population using the simple random sampling with replacement (SRSWR). Then we prove the following theorems.

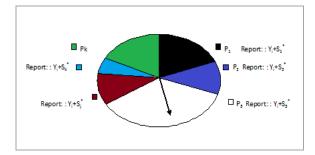


Fig. 2 Spinner for proposed procedure.

Theorem 2.1 An unbiased estimator of the population mean  $\mu_Y$  is given by

$$\hat{\mu}_{ST} = \frac{1}{n} \sum_{i=1}^{n} Z_i^*$$
(2.3)

**Proof.**Let  $E_1$  and  $E_2$  denote the expectation over the sampling design and the randomization device respectively, we have

$$\begin{split} E(\hat{\mu}_{ST}) &= E_1 E_2 \left\lfloor \frac{1}{n} \sum_{i=1}^n Z_i^* \right\rfloor \\ &= E_1 \left[ \frac{1}{n} \sum_{i=1}^n E_2(Z_i^*) \right] \\ &= E_1 \left[ \frac{1}{n} \sum_{i=1}^n \left\{ Y_i \sum_{j=1}^k P_j + \sum_{j=1}^k P_j E_2(S_j^*) \right\} \right] \\ &= E_1 \left[ \frac{1}{n} \sum_{j=1}^n Y_i \right] = \mu_Y \quad , \qquad \text{since} \\ &\sum_{j=1}^k P_j = 1 \text{ and } E_2(S_j^*) = 0, \end{split}$$

Which proves the theorem.

The variance of the proposed estimator  $\hat{\mu}_Y$  is given in the following theorem.

**Theorem 2.2** The variance of the proposed estimator  $\hat{\mu}_{\mathbf{Y}}$  is given by

$$\mathbf{V}(\hat{\boldsymbol{\mu}}_{\mathrm{ST}}) = \frac{1}{n} \left[ \boldsymbol{\sigma}_{\mathrm{y}}^{2} + 1 \right]$$
(2.4)

**Proof.** Let  $V_1$  and  $V_2$  denote the variance over the sampling design and over the proposed randomization device, respectively, then we have

$$V(\hat{\mu}_{Y}) = E_{I}V_{2}(\hat{\mu}_{Y}) + V_{I}E_{2}(\hat{\mu}_{Y})$$
  
=  $E_{I}\left[V_{2}\left(\frac{1}{n}\sum_{i=1}^{n}Z_{i}^{*}\right)\right] + V_{I}\left[E_{2}\left(\frac{1}{n}\sum_{i=1}^{n}Z_{i}^{*}\right)\right]$  (2.5)  
=  $E_{I}\left[\frac{1}{n^{2}}\sum_{i=1}^{n}V_{2}(Z_{i}^{*})\right] + V_{I}\left[\frac{1}{n}\sum_{i=1}^{n}E_{2}(Z_{i}^{*})\right]$ 

$$= \mathbf{E}_{1} \left[ \frac{1}{n^{2}} \sum_{i=1}^{n} (1) \right] + \mathbf{V}_{1} \left[ \frac{1}{n} \sum_{i=1}^{n} \mathbf{Y}_{i} \right]$$
$$= \frac{1}{n} \left( \sigma_{y}^{2} + 1 \right)$$

Note that:

$$\begin{split} \mathbf{V}_{2}(\mathbf{Z}_{i}^{*}) &= \mathbf{E}_{2}\left(\mathbf{Z}_{i}^{*2}\right) - \left(\mathbf{E}_{2}\left(\mathbf{Z}_{i}^{*}\right)\right)^{2} \\ \mathbf{E}_{2}(\mathbf{Z}_{i}^{*2}) &= \mathbf{E}_{2}\left(\mathbf{Y}_{i} + \mathbf{S}_{j}^{*}\right)^{2} = \mathbf{E}_{2}\left[\mathbf{Y}_{i}^{2} + \mathbf{S}_{j}^{*2} + 2\mathbf{Y}_{i}\mathbf{S}_{j}^{*}\right] \\ &= \mathbf{Y}_{i}^{2}\sum_{j=1}^{k}\mathbf{P}_{j} + \sum_{j=1}^{k}\mathbf{P}_{j} \quad , \qquad \text{since} \\ \mathbf{E}_{2}(\mathbf{S}_{j}^{*2}) &= 1 \text{ and } \mathbf{E}_{2}(\mathbf{S}_{j}^{*}) = 0, \\ &= (\mathbf{Y}_{i}^{2} + 1), \end{aligned}$$

and

$$E_2(Z_i^*) = E_2(Y_i + S_j^*) = Y_i \sum_{j=1}^k P_j = Y_i$$
,since  
 $E_2(S_j^*) = 0,$ 

Thus

$$V_2(Z_i^*) = Y_i^2 + 1 - Y_i^2 = 1$$

which proves the theorem.

#### 3. Efficiency Comparison

From (1.3) and (2.4), we have

$$V(\hat{\mu}_{ST}) < V(\hat{\mu}_{GS})_{if}$$

$$\frac{1}{n} \left[ \sigma_y^2 + 1 \right] < \frac{1}{n} \left[ \sigma_y^2 + \alpha \beta (\theta^2 + \gamma^2) \right]$$
i.e. if  $1 < \alpha \beta (\theta^2 + \gamma^2)$ 
i.e. if  $\alpha \beta < \frac{1}{(\theta^2 + \gamma^2)}$ 
(3.1)

Thus the proposed estimator  $\hat{\mu}_{ST}$  is better than Gjestvang and Singh (2009) estimator  $\hat{\mu}_{GS}$  as long as condition (3.1) is satisfied.

Further from (1.8) and (2.4), we have

$$V(\hat{\mu}_{ST}) < V(\hat{\mu}_{Y})$$

if

i.e.if 
$$\frac{1}{n} \left[ \sigma_y^2 + 1 \right] < \frac{1}{n} \left[ \sigma_y^2 + \sum_{j=1}^k P_j \left\{ (\theta_j^2 + \gamma_j^2) \right\} \right]$$

$$1 < \sum_{j=1}^{k} P_{j}(\theta_{j}^{2} + \gamma_{j}^{2})$$
  
i.e if  
$$\sum_{j=1}^{k} P_{j}(\theta_{j}^{2} + \gamma_{j}^{2} - 1) > 0, \quad \text{sin ce} \quad \sum_{j=1}^{k} P_{j} = 1,$$
  
i.e. if  $(\theta_{j}^{2} + \gamma_{j}^{2}) > 1, \forall j$  (3.2)

The condition (3.2) clearly indicates that if one chooses  $(\theta_j, \gamma_j)$  such that  $\{\!\!\{\theta_j^2 + \gamma_j^2\}\!\!>\!1\}\!\!$  then the proposed model is always better than the Singh's (2010) model. The percent relative efficiency (PRE) of the proposed estimator  $\hat{\mu}_{ST}$  with respect to Singh's (2010) estimator  $\hat{\mu}_{Y}$  and Gjestvang and Singh's (2009) estimator  $\hat{\mu}_{GS}$  are respectively given by

$$PRE(\hat{\mu}_{ST}, \hat{\mu}_{Y}) = \frac{\left[\sigma_{y}^{2} + \sum_{j=1}^{k} P_{j}\left\{\left(\theta_{j}^{2} + \gamma_{j}^{2}\right)\right\}\right]}{\left[\sigma_{y}^{2} + 1\right]} \times 100$$
(3.2)

and

$$PRE(\hat{\mu}_{ST}, \hat{\mu}_{GS}) = \frac{\left[\sigma_y^2 + \alpha\beta(\theta^2 + \gamma^2)\right]}{\left[\sigma_y^2 + 1\right]} \times 100$$
(3.3)

By keeping the respondents cooperation in mind, we decided to choose  $\alpha = 0.4$ ,  $\beta = 0.6$  (similarly to Gjestvang and Singh (2009)),  $\gamma=40$ ,  $\gamma_1=30$ ,  $\gamma_2=40$ ,  $\gamma_3=20$ ,  $\gamma_4=10$ ,  $P_1=0.02$ ,  $P_2=0.05$ ,  $P_3=0.06$ ,  $P_4=0.87$  with k=4 (similarly to Singh (2010)). In addition we choose different values  $\sigma_y^2$ ,  $\theta$ ,  $\theta_1$ ,  $\theta_2$ ,  $\theta_3$  and  $\theta_4$  as listed in Tables 1 and 2 respectively.

We have computed the percent relative efficiencies  $PRE(\hat{\mu}_{ST}, \hat{\mu}_{Y})_{and} \quad PRE(\hat{\mu}_{ST}, \hat{\mu}_{GS})_{and} \quad findings \quad are displayed in Tables 1 and 2 respectively.$ 

**Table 1.** The PRE  $(\hat{\mu}_{ST}, \hat{\mu}_{Y})$ 

$\sigma_{\mathbf{v}}^2$	$\theta_1$	$\theta_2$	$\theta_3$	$\theta_4$	PRE
	٩	02	•3	•4	
	300	200	100	-25.20	19948.02
	800	700	600	-100.00	260900.00
	1300	1200	1100	-174.70	789178.76
25	1800	1700	1600	-249.40	1604801.20
	300	200	100	-25.20	4195.62
	800	700	600	-100.00	53915.87
	1300	1200	1100	-174.70	162925.78
125	1800	1700	1600	-249.40	331228.82
	300	200	100	-25.20	2383.40
	800	700	600	-100.00	30103.54
ĺ.	1300	1200	1100	-174.70	90878.97
225	1800	1700	1600	-249.40	184711.64
	300	200	100	-25.20	1682.97
	800	700	600	-100.00	20900.00
	1300	1200	1100	-174.70	63032.66
325	1800	1700	1600	-249.40	128082.30
	300	200	100	-25.20	1311.38
	800	700	600	-100.00	16017.37
	1300	1200	1100	-174.70	48259.74
425	1800	1700	1600	-249.40	98039.51
	300	200	100	-25.20	1081.08
ĺ.	800	700	600	-100.00	12991.25
	1300	1200	1100	-174.70	39103.89
525	1800	1700	1600	-249.40	79419.83
	300	200	100	-25.20	924.36
	800	700	600	-100.00	10931.95
	1300	1200	1100	-174.70	32873.24
625	1800	1700	1600	-249.40	66748.93
	300	200	100	-25.20	810.81
	800	700	600	-100.00	9439.94
	1300	1200	1100	-174.70	28359.02
725	1800	1700	1600	-249.40	57568.64
	300	200	100	-25.20	724.76
1	800	700	600	-100.00	8309.20
1	1300	1200	1100	-174.70	24937.83
825	1800	1700	1600	-249.40	50611.18

# **Table 2.** The PRE $(\hat{\mu}_{ST}, \hat{\mu}_{GS})$

$\sigma_Y^2$	$\theta_1$	$\theta_2$	$\theta_3$	$\theta_4$	θ	PRE
	1	2	5	-		
	300	200	100	-25.20	200.00	38496.154
	800	700	600	-100.00	700.00	453880.77
	1300	1200	1100	-174.70	1200.00	1330803.8
25	1800	1700	1600	-249.40	1700.00	2669265.4
	300	200	100	-25.20	200.00	8023.0159
	800	700	600	-100.00	700.00	93737.302
	1300	1200	1100	-174.70	1200.00	274689.68
125	1800	1700	1600	-249.40	1700.00	550880.16
	300	200	100	-25.20	200.00	4517.2566
	800	700	600	-100.00	700.00	52304.867
	1300	1200	1100	-174.70	1200.00	153189.82
225	1800	1700	1600	-249.40	1700.00	307172.12
	300	200	100	-25.20	200.00	3162.2699
	800	700	600	-100.00	700.00	36291.104
	1300	1200	1100	-174.70	1200.00	106229.75
325	1800	1700	1600	-249.40	1700.00	212978.22
	300	200	100	-25.20	200.00	2443.4272
	800	700	600	-100.00	700.00	27795.54
	1300	1200	1100	-174.70	1200.00	81316.667
425	1800	1700	1600	-249.40	1700.00	163006.81
	300	200	100	-25.20	200.00	1997.9087
	800	700	600	-100.00	700.00	22530.228
	1300	1200	1100	-174.70	1200.00	65876.236
525	1800	1700	1600	-249.40	1700.00	132035.93
	300	200	100	-25.20	200.00	1694.7284
	800	700	600	-100.00	700.00	18947.125
	1300	1200	1100	-174.70	1200.00	55368.85
625	1800	1700	1600	-249.40	1700.00	110959.9
	300	200	100	-25.20	200.00	1475.0689
	800	700	600	-100.00	700.00	16351.102
	1300	1200	1100	-174.70	1200.00	47756.061
725	1800	1700	1600	-249.40	1700.00	95689.945
	300	200	100	-25.20	200.00	1308.5956
	800	700	600	-100.00	700.00	14383.656
	1300	1200	1100	-174.70	1200.00	41986.562
825	1800	1700	1600	-249.40	1700.00	84117.312

It is observed from Tables 1 and 2 that the value of  $PRE(\hat{\mu}_{ST}, \hat{\mu}_Y)$  and  $PRE(\hat{\mu}_{ST}, \hat{\mu}_{GS})$  are greater than 100. It follows that the proposed estimator is more efficient than the estimator  $\hat{\mu}_Y$  due to Singh (2010) and  $\hat{\mu}_{GS}$  due to Gjestvang and Singh (2009) with substantial gain in efficiency. Thus, based on our simulation results, the use of the proposed estimator  $\hat{\mu}_{ST}$  over Singh (2010) estimator  $\hat{\mu}_Y$  and Gjestvang and Singh (2009) estimator  $\hat{\mu}_{GS}$  is recommended for all

situations close to Tables 1 and 2 respectively. It should be mentioned here that the experience is must in real surveys while making a choice of randomization device to be used in practice.

Further we consider a situation where  $\theta = 0$  as well as  $\theta_j = 0$  for j = 1,2,3,4, and rest of the parameters are kept same as in Tables 1 and 2. The percent relative efficiency of the proposed estimator over Gjestvang and Singh (2009) and Singh (2010) estimators has been shown in Tables 3 and 4 respectively.

$\sigma_y^2$	25	125	225	325	425	525	625	725	825
PRE	900.00	256.08	192.04	163.80	148.83	139.54	133.23	128.65	125.18

Table 3. Percent relative efficiencies of the proposed estimator  $\hat{\mu}_{ST}$  over the Singh (2010) estimator  $\hat{\mu}_{Y}$ .

Table 4. Percent relative efficiencies of the proposed estimator  $\hat{\mu}_{ST}$  over the Gjestvang and Singh (2009) estimator  $\hat{\mu}_{GS}$ .

$\sigma_y^2$	25	125	225	325	425	525	625	7 25	825
PRE	1573.07	403.96	269.46	217.48	189.90	172.81	161.18	152.75	146.36

The minimum values of the percent relative efficiencies in Tables 3 and 4 is observed as 125.18 and 146.36 and maximum 900.00 and 1573.07 with a median of 148.83 and 189.90 based on 9 situations investigated in Tables 3 and 4 for different choices of parameters respectively. It is observed from tables 3 and 4 that the percent relative efficiency remains higher if the value of  $\sigma_y^2$  is small. In order to see as the maximum gain we also investigate lower values of  $\sigma_y^2$  given that in practice, for example, the number of abortions by a woman could vary from 0 to 3 or 4, because it may not be practical for a woman to go for more than 3 or 4 abortions. In that case the value of  $\sigma_y^2$  will be around 0.5 to 5.0 [see Singh (2010), p.79]. We observed that the percent relative efficiency value decreases from 13966.67 to 3566.76 (in case of Singh (2010)) and 25633.33 to 6483.34 (in case of Gjestvang and Singh (2009)) as the value of  $\sigma_y^2$  increases from 0.5 to 5.0 when all the means of the scrambling variables are zero level.

We have given the various choices of parameters for k =2 in Tables 5 and 6 such that the suggested estimator  $\hat{\mu}_{ST}$ remains better than the Singh's (2010) estimator  $\hat{\mu}_{Y}$  and Gjestvang and Singh (2009) estimator  $\hat{\mu}_{GS}$ . Thus, based on our findings, the use of the envisaged estimator  $\hat{\mu}_{ST}$  over Singh's (2010) estimator  $\hat{\mu}_{Y}$  and Gjestvang and Singh (2009) estimator  $\hat{\mu}_{GS}$  is recommended for all situations close to Tables 1 to 6 in real practice. **Table 5.** Percent relative efficiencies of the proposed estimator  $\hat{\mu}_{ST}$  over the<br/>Singh (2010) estimator  $\hat{\mu}_Y$  with k =2.Percent relative efficiencies of the proposed estimator  $\hat{\mu}_{ST}$  over the<br/>Gjestvang and Singh (2009) estimator  $\hat{\mu}_{GS}$  with k =2.

$\begin{array}{c c c c c c c c c c c c c c c c c c c $		-	1102
125         336575.40           225         187692.48           325         130148.77           425         99620.89           525         80700.57           625         67825.08           725         58496.56           0.2         1700         1300           -325.0         825         51426.76           25         235942.31         125           125         18909.51         225           425         14494.13           525         11757.60           625         9895.37           725         8546.14           0.4         700         300           -200.0         825         7523.61           25         1646116.67           125         339754.23           225         189464.75           325         131377.40           425         100561.11           525         81462.04           625         68464.91           725         59048.26           0.4         1700         800           -533.3         825         51911.66           125         1388711.54         125			
125         336575.40           225         187692.48           325         130148.77           425         99620.89           525         80700.57           625         67825.08           725         58496.56           0.2         1700         1300         -325.0           825         51426.76           25         235942.31           125         48765.87           225         27232.30           325         18909.51           425         14494.13           525         11757.60           625         9895.37           725         8546.14           0.4         700         300           -200.0         825         7523.61           25         1646116.67           125         339754.23           225         189464.75           325         131377.40           425         100561.11           525         81462.04           625         68464.91           725         59048.26           0.4         1700         800           -533.3         825         51911.66			
0.2         1700         1300         -325.0         825         130148.77           425         99620.89         525         80700.57         625         67825.08           0.2         1700         1300         -325.0         825         51426.76           0.2         1700         1300         -325.0         825         51426.76           0.2         1700         1300         -325.0         825         51426.76           0.2         1700         1300         -325.0         825         51426.76           0.2         1700         300         -200.0         825         14494.13           525         11757.60         625         9895.37         725         8546.14           0.4         700         300         -200.0         825         7523.61           125         14494.13         525         11757.60         625         9895.37           725         8546.14         1105         625         14494.13           525         11757.60         625         11757.60         625           625         1466.116.67         125         339754.23         225         131377.40         425         14051.11         525		25	
0.2         1700         1300         -325         130148.77           425         99620.89         525         80700.57           625         67825.08         725         58496.56           0.2         1700         1300         -325.0         825         51426.76           0.2         1700         1300         -325.0         825         51426.76           0.2         1700         1300         -325.0         825         51426.76           125         48765.87         225         27232.30         325         18909.51           425         14494.13         525         11757.60         625         9895.37           725         8546.14         0.4         700         300         -200.0         825         7523.61           0.4         700         300         -200.0         825         7523.61           125         339754.23         225         189464.75         325         131377.40           425         14051.11         525         81462.04         625         68464.91           525         800         -533.3         825         51911.66           0.4         1700         800         -533.3		125	336575.40
0.2         1700         1300         -325.0         825         80700.57           625         67825.08         725         58496.56           0.2         1700         1300         -325.0         825         51426.76           25         235942.31         125         48765.87         225         27232.30           325         18909.51         425         14494.13         525         11757.60           625         9895.37         725         8546.14         300         -200.0         825         7523.61           0.4         700         300         -200.0         825         7523.61         125         339754.23           0.4         700         300         -200.0         825         7523.61           0.4         700         800         -533.3         825         5191.66           0.4         1700         800         -533.3         825         51911.66           0.4         1700         800         -533.3         825         51911.66           0.4         1700         800         -533.3         825         51911.66           0.4         1700         800         -533.3         825         519		225	187692.48
0.2         1700         1300         -325.0         825         51426.76           0.2         1700         1300         -325.0         825         51426.76           125         48765.87         225         27232.30         325         18909.51           125         48765.87         225         11757.60         625         9895.37           725         8546.14         525         11757.60         625         9895.37           725         8546.14         525         11757.60         625         9895.37           725         8546.14         525         11757.60         625         9895.37           725         8546.14         525         11757.60         625         9895.37           725         8546.14         525         11757.60         625         9895.37           725         8546.14         525         11757.60         625         11757.60           625         1646116.67         125         339754.23         225         131377.40           425         100561.11         525         81462.04         625         68464.91           725         59048.26         51911.66         25         1388711.54 <td< td=""><td></td><td>325</td><td>130148.77</td></td<>		325	130148.77
0.2         1700         1300         -325.0         825         51426.76           0.2         1700         1300         -325.0         825         51426.76           125         48765.87         225         27232.30         325         18909.51           125         14494.13         525         11757.60         625         9895.37           725         8546.14         525         1646116.67         125         339754.23           0.4         700         300         -200.0         825         7523.61           225         189464.75         325         131377.40           425         100561.11         525         81462.04           625         68464.91         725         59048.26           0.4         1700         800         -533.3         825         51911.66           125         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59           625         57773.96         525         57773.96         5773.96		425	99620.89
0.2         1700         1300         -325.0         825         51426.76           25         235942.31         125         48765.87           225         27232.30         325         18909.51           425         14494.13         525         11757.60           625         9895.37         725         8546.14           0.4         700         300         -200.0         825         7523.61           25         1646116.67         125         339754.23         225         189464.75           325         131377.40         425         100561.11         525         81462.04           625         68464.91         725         59048.26         68464.91         725         59048.26           0.4         1700         800         -533.3         825         51911.66         25         1388711.54           125         286638.89         225         159851.77         325         110848.16         425         84850.94         525         68738.59         625         57773.96		525	80700.57
0.2         1700         1300         -325.0         825         51426.76           25         235942.31         125         48765.87           225         27232.30         325         18909.51           425         14494.13         525         11757.60           625         9895.37         725         8546.14           0.4         700         300         -200.0         825         7523.61           25         1646116.67         125         339754.23         225         189464.75           325         131377.40         425         100561.11         525         131377.40           425         100561.11         525         519048.26         625         68464.91           0.4         1700         800         -533.3         825         51911.66           0.4         1700         800         -533.3         825         51911.66           25         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59         625         57773.96		625	67825.08
0.4         700         300         -200.0         825         125         48765.87           225         27232.30         325         18909.51         425         14494.13           525         11757.60         625         9895.37         725         8546.14           0.4         700         300         -200.0         825         7523.61           225         189464.75         325         131377.40           425         100561.11         525         81462.04           625         68464.91         725         59048.26           0.4         1700         800         -533.3         825         51911.66           25         159851.77         325         1388711.54         125         286638.89           225         159851.77         325         110848.16         425         84850.94           525         68738.59         625         57773.96         625         57773.96		725	58496.56
125         48765.87           225         27232.30           325         18909.51           425         14494.13           525         11757.60           625         9895.37           725         8546.14           0.4         700         300         -200.0           825         7523.61           255         1646116.67           125         339754.23           225         189464.75           325         131377.40           425         100561.11           525         51046.204           625         68464.91           725         59048.26           0.4         1700         800           -533.3         825         51911.66           25         1388711.54         125           25         159851.77         325           325         110848.16           425         84850.94           525         68738.59           625         57773.96	0.2 1700 1300 -325.0	825	51426.76
0.4         700         300         -200.0         825         7523.61           0.4         700         300         -200.0         825         7523.61           0.4         700         300         -200.0         825         7523.61           0.4         700         300         -200.0         825         7523.61           0.4         700         300         -200.0         825         7523.61           0.4         700         800         -533.3         225         189464.75           325         131377.40         425         100561.11         525         81462.04           625         68464.91         725         59048.26         51911.66           0.4         1700         800         -533.3         825         51911.64           125         286638.89         225         159851.77         325         110848.16           425         84850.94         525         68738.59         625         57773.96		25	235942.31
0.4         700         300         -200.0         825         14494.13           525         11757.60         625         9895.37           725         8546.14           0.4         700         300         -200.0         825         7523.61           25         1646116.67         125         339754.23         225         189464.75           325         131377.40         425         100561.11         525         81462.04           625         68464.91         725         59048.26         625         68464.91           0.4         1700         800         -533.3         825         51911.66           25         159851.77         325         110848.16         425         84850.94           525         68738.59         625         57773.96         57773.96		125	48765.87
0.4         700         300         -200.0         825         7523.61           0.4         700         300         -200.0         825         7523.61           25         1646116.67         125         339754.23           225         189464.75         325         131377.40           425         100561.11         525         81462.04           625         68464.91         725         59048.26           0.4         1700         800         -533.3         825         51911.66           25         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59           625         57773.96         525         57773.96         57773.96		225	27232.30
0.4         700         300         -200.0         825         7523.61           0.4         700         300         -200.0         825         7523.61           125         13646116.67         125         339754.23           225         189464.75         325         131377.40           425         100561.11         525         81462.04           625         68464.91         725         59048.26           0.4         1700         800         -533.3         825         51911.66           25         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59           625         57773.96         625         57773.96         57773.96		325	18909.51
0.4         700         300         -200.0         825         7523.61           725         8546.14         825         7523.61           25         1646116.67         125         339754.23           225         189464.75         325         131377.40           425         100561.11         525         81462.04           625         68464.91         725         59048.26           0.4         1700         800         -533.3         825         51911.66           225         159851.77         325         110848.16         425         84850.94           525         68738.59         625         57773.96         57773.96		425	14494.13
0.4         700         300         -200.0         725         8546.14           0.4         700         300         -200.0         825         7523.61           25         1646116.67         125         339754.23         225         189464.75           325         131377.40         425         100561.11         525         81462.04           625         68464.91         725         59048.26         68464.91           0.4         1700         800         -533.3         825         51911.66           25         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59           625         57773.96         625         57773.96         57773.96		525	11757.60
0.4         700         300         -200.0         725         8546.14           0.4         700         300         -200.0         825         7523.61           25         1646116.67         125         339754.23         225         189464.75           325         131377.40         425         100561.11         525         81462.04           625         68464.91         725         59048.26         68464.91           0.4         1700         800         -533.3         825         51911.66           25         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59           625         57773.96         625         57773.96         57773.96		625	9895.37
0.4         1700         800         -533.3         825         51911.66           0.4         1700         800         -533.3         825         51911.66           25         138964.75         325         131377.40         425         100561.11           525         81462.04         625         68464.91         725         59048.26           0.4         1700         800         -533.3         825         51911.66           25         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59           625         57773.96         625         57773.96         57773.96		725	8546.14
125         339754.23           225         189464.75           325         131377.40           425         100561.11           525         81462.04           625         68464.91           725         59048.26           0.4         1700         800           -533.3         825         51911.66           25         1388711.54         125           225         159851.77         325           325         110848.16           425         84850.94           525         68738.59           625         57773.96	0.4 700 300 -200.0	825	7523.61
225         189464.75           325         131377.40           425         100561.11           525         81462.04           625         68464.91           725         59048.26           0.4         1700         800           -533.3         825         51911.66           25         1388711.54         125           225         159851.77         325           325         110848.16           425         84850.94           525         68738.59           625         57773.96		25	1646116.67
325         131377.40           425         100561.11           525         81462.04           625         68464.91           725         59048.26           0.4         1700         800           -533.3         825         51911.66           25         1388711.54         125           225         159851.77         325           325         110848.16           425         84850.94           525         68738.59           625         57773.96		125	339754.23
425         100561.11           525         81462.04           625         68464.91           725         59048.26           0.4         1700         800           -533.3         825         51911.66           25         1388711.54         125           225         159851.77           325         110848.16           425         84850.94           525         68738.59           625         57773.96		225	189464.75
0.4         1700         800         -533.3         825         51911.66           0.4         1700         800         -533.3         825         51911.66           25         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59           625         57773.96         57773.96         57773.96         57773.96		325	131377.40
0.4         1700         800         -533.3         825         51911.66           0.4         1700         800         -533.3         825         51911.66           25         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59           625         57773.96         57773.96         57773.96         57773.96		425	100561.11
0.4         1700         800         -533.3         725         59048.26           0.4         1700         800         -533.3         825         51911.66           25         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59           625         57773.96         57773.96         57773.96         57773.96		525	
0.4         1700         800         -533.3         725         59048.26           0.4         1700         800         -533.3         825         51911.66           25         1388711.54         125         286638.89         225         159851.77           325         110848.16         425         84850.94         525         68738.59           625         57773.96         57773.96         57773.96         57773.96		625	68464.91
25         1388711.54           125         286638.89           225         159851.77           325         110848.16           425         84850.94           525         68738.59           625         57773.96			59048.26
25         1388711.54           125         286638.89           225         159851.77           325         110848.16           425         84850.94           525         68738.59           625         57773.96	0.4 1700 800 -533.3	825	51911.66
225         159851.77           325         110848.16           425         84850.94           525         68738.59           625         57773.96		25	1388711.54
225         159851.77           325         110848.16           425         84850.94           525         68738.59           625         57773.96		125	286638.89
325         110848.16           425         84850.94           525         68738.59           625         57773.96			
425         84850.94           525         68738.59           625         57773.96			
525 68738.59 625 57773.96			
625 57773.96		525	
725 49829.89		725	49829.89
	0.8 1700 300 -1200.0		43809.32

P1	θ	$\theta_1$	$\theta_2$	$\sigma_{Y}^{2}$	PRE
				25	2669265.4
				125	550880.16
		•		225	307172.12
				325	212978.22
		•		425	163006.81
		•		525	132035.93
		•		625	110959.9
		•		725	95689.945
0.2	1700	1300	-325.0	825	84117.312
				25	453880.77
		•		125	93737.302
		•		225	52304.867
		•		325	36291.104
		•		425	27795.54
				525	22530.228
		•		625	18947.125
				725	16351.102
0.4	700	300	-200.0	825	14383.656
				25	2669265.4
				125	550880.16
				225	307172.12
				325	212978.22
				425	163006.81
				525	132035.93
				625	110959.9
				725	95689.945
0.4	1700	800	-533.3	825	84117.312
				25	2669265.4
				125	550880.16
				225	307172.12
				325	212978.22
				425	163006.81
				525	132035.93
				625	110959.9
				725	95689.945
0.8	1700	300	-1200.0	825	84117.312

## 4. CONCLUSIONS AND RECOMMENDATIONS

This paper illustrates enrichment over the Gjestvang and Singh's (2009) randomized response model and Singh (2010). We have suggested the new additive randomized response model which is to be more efficient both theoretically as well as numerically than the additive randomized response model studied by Gjestvang and Singh (2009) and the additive model due to Singh (2010). Thus the proposed randomized response procedure is therefore recommended for its use in practice as an alternative to Gjestvang and Singh's (2009) and Singh (2010) model.

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## CONFLICT OF INTEREST

No conflict of interest was declared by the authors.

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