# Optimization of laser doping process in crystalline silicon solar cells

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**Abstract-** A large area selective emitter patterning scheme is developed and reported in the present study that features a single additional step compared to the standard process. Initially, trials are conducted to achieve a uniform base sheet resistance of  $100\pm10$  Ω/sq in p-type c-Si wafers using POCl3 diffusion on a large area 156 x 156 mm silicon wafers. Thereafter, employing a nanosecond, Q-switched, green laser and phosphosilicate glass layer (PSG) as a dopant source, areas below the front contact fingers are heavily doped while areas between them are kept lowly doped, thus realizing a selective emitter. This study refers to optimization of diffusion parameters to achieve uniform diffusion of base sheet resistance of 100±10 Ω/sq and optimization of laser parameters for achieving localized regions of high doping to attain selective emitter structure.

**Keywords-** Laser, Doping, Diffusion, Crystalline silicon solar cell, sheet resistance.

#### **1. Introduction**

Low Ohmic contacts to the front side of p-n junction Si solar cells require high doping in the ''emitter'' (usually the ntype) part of the cell. Unfortunately, high doping goes hand-inhand with increased Auger recombination and decreased quantum efficiency for short wavelength radiation. The ''selective'' emitter (SE) concept uses laterally different emitter doping: (i) high doping under the front side metallization for low contact resistance between contact metal and semiconductor interface, (ii) low doping between the contact fingers for a better short wavelength response owing to reduced Auger recombination [1] as well as improved emitter passivation [2,3]. Unfortunately, most SE concepts developed so far in research imply a high process complexity due to the required steps for masking of selective diffusion [4] or emitter

etch back [5]. In essence, these concepts are difficult to implement into industrial production of solar cells. Several different SE approaches for industrial production are currently under development [6,7] or are being transferred to the industry [8].

The present paper refers to optimization of laser parameters for achieving high doping in regions below the front metal contacts employing furnace diffused silicon wafers as the base material. The add-on laser doping increases the doping concentration as well as the emitter depth underneath the contact fingers, thus yielding good Ohmic contacts. The silver metallization is then put exactly over the laser doped regions using high precision screen printer. The laser doping has several advantages over the chemical etching process, conventionally used for achieving selective emitter. These include a dry process, having a high accuracy and fast speed. In the present paper, we have discussed tuning of laser parameters

# INTERNATIONAL JOURNAL of RENEWABLE ENERGY RESEARCH Abhishek Sharan *et al. ,Vol.3, No. 3*

for laser diffusion of furnace diffused emitter for achieving selectively doped emitter.

# **2. Experimental**

Figure 1 below describes the process sequence for Laser Doped selective emitter solar cell structure for which the starting material is  $156$  mm x  $156$  mm in size,  $200 \mu m$  thick, ptype Czochralski grown wafers. Step 1 textures the wafer surface by a standard, alkaline etching process that produces random pyramids and reduces the optical reflectivity of the surface. Step 2 creates the n-type phosphorus doped emitter together with a phosphosilicate glass (PSG) layer on top by conventional POCl3 diffusion process. The PSG layer mainly consists of SiO2:P2O5 with the ratio of SiO2 and P2O5 depending on the processing time, gas composition, gas flow and diffusion temperature [9]. The sheet resistivity of the wafer is adjusted to lie in the range of  $100\pm10$   $\Omega$ /sq. by experimenting with several combinations of the flat zone temperature, pre-diffusion time and the drive-in time.



**Fig.1.** Process flow for laser doped selective emitter solar cells.

In Step 3, laser doping is carried out to create heavily diffused, deep emitter over closely spaced localized regions. The PSG layer serves as the doping precursor. The laser that is used for laser doping is a nanosecond, green (532 nm), Nd:VO4 laser with a spot size of approximately  $25 \mu m$ . The laser frequency used is either 50 or 55 kHz at which frequency the laser shows the maximum stability. The laser parameters varied for process optimization of laser doping include laser power  $(0.2 - 1.2 \text{ W})$ , scan speed  $(500 - 1200 \text{ mm/sec})$ , laser shift in transverse direction and number of cycles  $(1 - 6)$ . To determine the effect of laser doping and its dependence on various factors, the sheet resistance of wafers before and after laser doping are measured and the ratio of the sheet resistances (Rsheet after laser doping/Rsheet before laser doping) used as the parameter for determining the effectiveness of laser doping.

In Step 4, Hydrofluoric acid is used to remove the PSG layer and a SiNx anti reflection coating (ARC) is deposited over the emitter. Before putting the ARC, the wafers are mapped with respect to their sheet resistance using a four probe measurement set up. The cell fabrication process is completed in Step 5 by applying the front and back metal contacts with screen printing and firing. The last process step, however, is beyond the scope of this study.

#### **3. Results and discussions**

#### *3.1. Shallow emitter diffusion*

Figure 2 depicts the contour plots of resistivity measurements for six different experiments on emitter diffusion as described above. The summary of the results with the process parameters is shown in Table 1. From the figure and the table, it is clear that at the diffusion temperature of 780  ${}^{0}C$ , a pre-deposition time of 45 min and a drive-in time of 25 min yield a mean sheet resistance of  $106.1\Omega$ /sq with a standard deviation of 5.37 $\Omega$ /sq. This is the base wafer that is used in our subsequent study of optimization of laser parameters to achieve a target sheet resistance of  $40\pm10$   $\Omega$ /sq after laser diffusion.



# INTERNATIONAL JOURNAL of RENEWABLE ENERGY RESEARCH Abhishek Sharan *et al. ,Vol.3, No. 3*





**Fig.2.** Contour plots of Sheet Resistance for different experiments on emitter diffusion

S1.	Diffu	Pre	Drive	Mean	<b>Std Dev</b>
No.	sion Temp	Dep Time	In Time	Rshee t	$(\Omega/Sq.)$
	$({}^{\circ}C)$	(minute)	(minu te)	$(\Omega/Sq)$ . )	
A	770	45	30	145.3	12.7
B	785	45	20	139.3	19.4
$\mathcal{C}$	780	45	25	106.1	5.37
D	800	45	20	92.3	3.56
E	795	45	30	73.3	3.15
$\mathbf{f}$	800	45	30	72.8	3.21

**Table 1.** Variation of Rsheet with diffusion parameters

# *3.2. Laser Power Optimization*

The variation of laser power has a significant effect on emitter doping. This is seen from Fig. 3 where the ratio of sheet resistance of the laser doped region to that of the base wafer is plotted against the laser power. The plot shows that efficiency of laser doping, shown by a reduction in the ratio of sheet resistances, increases with an increase in the laser power applied. While keeping the other laser parameters constant, this ratio reaches the minimum value at a laser power of 0.3 and 0.4 W and then begins to increase. This suggests that the laser doping is most optimal at 0.3 and 0.4 W.



**Fig.3.** Variation of the ratio of sheet resistances of laser doped region to that of the base wafer vs. laser power

# INTERNATIONAL JOURNAL of RENEWABLE ENERGY RESEARCH Abhishek Sharan *et al. ,Vol.3, No. 3*

The increase in the ratio of sheet resistances beyond 0.4 W of laser power suggests that phosphorous doping decreases at higher laser powers. At a laser power close to 1.0 W, the sheet resistance of the laser doped region even exceeds that of the base wafer suggesting ablation of silicon atoms along with phosphorus atoms. This is very well depicted in the SEM images of the samples in Fig.4.



**Fig.4.** SEM images of silicon wafer after laser doping with laser power of (a) 0.4 W, (b) 0.9 W

#### *3.3. Laser Scan Speed Optimization*

The laser in use is a pulsed laser with a spot size of approximately 25 µm. However, as depicted in Fig. 5, the spot size varies a little with the laser power. It is desired that for uniform doping, the consecutive laser pulses sufficiently overlap each other.



**Fig.5.** Variation of laser spot size with laser

The overlapping of consecutive laser pulses is dependent on the scan speed of the laser spot and the effect is clearly visible from the SEM images of Fig. 6 where a good overlap of laser pulses at a speed of 800 mm/sec is compared with a nooverlap case at a scan speed of 1200 mm/sec.

This is suggestive of the fact that lower scan speeds are preferred for doping uniformity. However, appearance of visual uniformity alone does not ascertain effective doping. For this, ratio of sheet resistance is plotted against scan speed (Fig 7). It is seen from this plot that lower scan speeds (500-600 mm/sec) are preferred for optimum laser doping.



**Fig.7.** Variation of ratio of sheet resistance of laser doped region to that of base wafer with laser scan speed (laser power of 0.4 W, laser shift of 22 µm in transverse direction & no. of cycles as 1)



 $Speed = 800 \text{ mm/sec}$  Speed = 1200 mm/sec **Fig.6.** SEM images showing laser pulse overlap at different laser scan speeds

#### *3.4. Laser Shift in transverse direction and no. of cycles:*

While optimization of laser scan speed is required to maintain pulse overlap in the horizontal direction, optimization of laser shift in transverse direction is required to maintain pulse overlap in the vertical direction. The plot of the mean of the ratio of sheet resistances obtained from laser doping at

various set of laser parameters at a specific laser shift versus laser shift (in  $\mu$ m) in transverse direction is shown in Fig. 8(a). It is evident from the plot that at 20 µm laser shift the ratio of sheet resistance is higher when compared to laser shifts at 16  $\mu$ m and 18  $\mu$ m.



Fig. 8 The effect of laser shift in transverse direction and no. of cycles on laser doping

Fig 8(b) above plots the mean of the ratio of sheet resistance obtained from laser doping at various set of laser parameters repeated a number of times (cycle) Vs the number of repetition of laser doping (cycle). 6 cycles shows a significant reduction in sheet resistance of the samples. However, for industrial processes 6 cycles is not feasible since it a long time and leads to low throughput. Therefore, for industrial processes comprising 1 and 2 cycles are preferred over a 6-cycle process.

Having obtained the optimized ranges of laser power, scan speed, laser shift in transverse direction and no. of cycles, from the above described experiments, studies are carried out on a number of combinations of these laser parameters. From the measurement of sheet resistances, the following four sets of laser parameters show the optimal results with the minimum ratio of sheet resistances, which are feasible to be incorporated into production, as shown in Table 2.

Table 2. Laser Parameters corresponding to the desired value the ratio of sheet resistances in the Laser Doped region to laser undoped region

Sl.No.	Laser Power	Laser	Scan	Laser	shift	1n	No. of cycles	Rsh(Laser
	W)	Speed		transverse		direction		Doped)/Rsh(Base)
		(mm/sec)		(um)				
	0.4	500		18				0.32
	0.4	500		20				0.32
	0.3	500		16				0.33
	0.4	600		16				0.33

#### **4. Conclusion**

The study described above, optimizes the POCl3 diffusion process for shallow emitter, of sheet resistance value  $100\pm10$   $\Omega$ /sq, to be used for making laser doped selective emitter solar cells. Diffusion temperature of  $780^{\circ}$ C, pre deposition time of 45 min and drive in time of 25 min have been found to give emitters of sheet resistance value of 106  $\Omega$ /sq with a standard deviation of 5.37  $\Omega$ /sq.

The study also includes scanning of various laser parameters involved in laser doping and reveals the set of laser parameters giving minimum ratio of sheet resistances in the laser doped and laser undoped region. A minimum ratio of sheet resistance in laser doped and laser undoped region of 0.32-0.35 have been obtained on a base wafer of sheet resistance ~106  $\Omega$ /sq, which is much below the target ratio of 0.40. Such selectively doped emitter is expected to give a high efficiency solar cell.

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