

## ON THE MATHEMATICAL THEORY OF TIDAL WAVE PROPAGATION

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### ARSTRACT

The vertical structure of the tidal-wave-propagation is expressed in terms of the solutions to a second-order linear inhomogeneous differential equation, with variable coefficient.

In the present paper, analytical expressions for these solutions are obtained, for the first time, through the simulation of the inhomogeneous term, responsible for exciting the observed tides.

### 1. INTRODUCTION

The fundamental equation that governs the vertical structure of the tidal-wave propagation [1] is:

$$(1.1) \quad d^2y_n/dx^2 + \mu^2_n(x) y_n = Q_n(x);$$

subject to the boundary conditions:

$$(1.2) \quad y'_n(0) = K_n y_n(0); K_n = (H(0)/h_n - \frac{1}{2})$$

and

$$(1.3) \quad y_n(x^*) \text{ is bounded; } x^* \text{ is the upper bound.}$$

$y_n(x)$  is the wave function, defined as:

$$(1.4) \quad y_n = (X_n - k_j n/gH) e^{-x/2}$$

where  $X_n(x)$  is the velocity divergence,  $J_n(x)$  is the non-adiabatic heating rate per unit mass, and  $x$  is the reduced height;

$$(1.5) \quad x = \int dz/H(z), H(z) = RT(z)/g$$

The forcing function  $Q_n(x)$  is defined as:

$$(1.6) \quad Q_n(x) = (k/\gamma gh_n) J_n e^{-x/2}$$

The subscript  $n$  indicates the mode number,  $h_n$  is the equivalent depth of the mode of oscillation that characterizes its propagation, and may have negative values for certain kind of modes.

In the existing tidal theory [1], the real difficulty lies in specifying  $Q_n$  with sufficient accuracy from our knowledge of the radiating processes and temperature change. Moreover, previous investigators [2,3] have adopted simplified models for  $Q_n$  in order to render the mathematical treatment more tractable. In comparing these theoretical predictions with the observed tides, Groves [4] has found that changes as large as 300 %, in the upward energy flux of a particular mode, can result for various distributions of  $Q_n$ .

For direct comparison between observations and theory, simulation based on the theory is often powerful. This called the attention for the inverse problem of deriving the forcing function from the observed tides. With such an approach, numerical solutions to Eq. (1.1) have been recently obtained [5]. In the present paper, the deduced empirical formulae for the forcing function are utilized in deriving analytical expressions for the solutions to (1.1).

## 2. A model for the Variable Coefficient

The variable coefficient  $\mu_n^2(x)$ , in (1.1), is defined as:

$$(2.1) \quad \mu_n^2(x) = -\frac{1}{4} + (kH + dH/dx)/h_n$$

For a reasonable choice of  $H(x)$ , Eq. (1.1) is a well-behaved, non-singular differential equation. When  $H$ ,  $(kH + dH/dx)$  or  $(dH/dx)$  is constant, 1.1 has homogeneous solutions which are exponential, sinusoidal or Bessel functions [1,2]. For problems of any complexity, no closed-form solution exists and it has to be approached numerically.

Table 1. *The Model*

Region	1	2	3	4	5
$x$ $x_0$	$x_1$	$x_2$	$x_3$	$x_4$	$x_5$
0	5.3	7.0	11.9	15.6	16.8
$z$ (km) 0	36.53	49.15	81.45	100.09	109.22
$H$ (km) 8.47	7.22	7.51	5.16	6.44	8.70
$p$ 1.33	0.00	-0.12	0.00	0.25	0.25

With a realistic distribution of  $H(x)$ , it was found [5] that the domain is divided into five distinct regions, with respect to the characteristics of the tidal modes propagation, as in table 1.

The range  $x_0, < x < x_4$  is further divided into 78 subregions of spacing  $\Delta x = 0,2$ , for each of which  $(kH + dH/dx)$  satisfies a linear form, thus

$$(2.2) \mu_n^2(x) = p_n x + q_n; x_0 \leq x \leq x_4$$

$p_n$  changes sign at  $x_1$  and  $x_3$ .

In the upper-most region,  $x_4 \leq x \leq x_5$ , the existing model suggests that  $(kH + dH/dx)$  meets smoothly an exponential profile, thus

$$(2.3) \mu_n^2(x) = -\frac{1}{4} + \tau_n e^{x/4}; x_4 < x < x_5.$$

The parameter  $\rho$  is defined by:

$$(2.4) \mu_n^2 + \frac{1}{2} = \partial_n e^{\rho x}$$

$p_n$  and  $\partial_n$  are defined for each mode, but  $\rho$  is the same for all modes.

Thereafter, the subscript  $n$  is dropped, for simplicity in writing, and modes are treated independently.

### 3. Simulation of the Solution

In this section, the solutions to the D. Eq. (1.1) is simulated, using the observational evidences, in the five regions of the domain (table 1), and maintaining the continuity at the separation levels in the solutions and their derivatives.

(i) Theoretically, the vertical dependence terms,  $V(x)$ , in the velocity fields are usually expressed in terms of the solutions,  $y(x)$ , as:

$$(3.1) V(x) = (dy/dx - y/2) e^{x/2}$$

Based on the analysis, of the observed tides,  $V(x)$  have been previously computed [6] at  $x = 0$  (0.1) 8.4, and they have been found to be represented fairly accurately in complex exponential forms, in each of the first two regions;  $0 \leq x \leq x_1$  and  $x_1 \leq x \leq x_2$  as:

$$(3.2) V(x) = \sum_{v=0}^3 a_v e^{i \alpha v x}; 0 \leq x \leq x_1$$

and

$$(3.3) V(x) = \sum_{v=0}^3 b_v e^{i \beta v x}; x_1 < x < x_2$$

Representations in (3.2) } and (3.3) are justified by the fact that  $Q(x)$  on the right-hand side of (1.1) is a periodic force of excitation.

On equating (3.2), and (3.3) independently, to (3.1), the complex coefficients  $a_v$  (and  $b_v$ ) and arguments  $\alpha_v$  (and  $\beta_v$ ) have been evaluated, by applying the Complex Fast Fourier Transform Technique [5] to the observed values of  $V(x)$ ; thus

$$(3.4) \quad (dy/dx - y/2) e^{x/2} = \sum_v a_v e^{i \alpha_v x}; \quad x_0 \leq x \leq x_1$$

and similar expression for the region  $x_1 \leq x \leq x_2$ .

Differentiating (3.4) we find that the solution  $y(x)$  satisfies the linear second order differential equation:

$$(3.5) \quad d^2y/dx^2 - y/4 = r(x)$$

where

$$(3.6) \quad r(x) = e^{-x/2} \sum_v i \alpha_v a_v e^{i \alpha_v x}$$

Hence the general solution is:

$$(3.7) \quad y(x) = A e^{x/2} + B e^{-x/2} + e^{x/2} \int_0^x e^{-x/2} r dx - e^{-x/2} \int_0^x e^{x/2} r dx$$

Substituting from (3.6), for the evaluation of the integrals, we find:

$$(3.8) \quad y(x) = e^{x/2} \left[ A - \sum_v \frac{i \alpha_v a_v}{(i \alpha_v - 1)} \right] \\ + e^{-x/2} \left[ B + \sum_v \frac{a_v}{(i \alpha_v - 1)} e^{i \alpha_v x} + \sum_v a_v \right]$$

On differentiation:

$$(3.9) \quad y'(x) = e^{x/2} \left[ A - \sum_v \frac{i \alpha_v a_v}{(i \alpha_v - 1)} \right] / 2 - e^{-x/2}$$

$$\left[ B + \sum_v \frac{(1 - 2 i \alpha_v)}{(i \alpha_v - 1)} a_v e^{i \alpha_v x} + \sum_v a_v \right] / 2$$

The two constants of integration  $A$  and  $B$  are determined through using the initial values of  $y(0)$  and the lower boundary condition (1.2), which can be rewritten in the form:

$$(3.10) \quad y'(0) = K y(0) = \sum_v a_v + y(0)/2$$

Thus we must have

$$A + B = y(0) \text{ and } A - B = 2 \sum_{\nu} a_{\nu} + y(0)$$

i.e.

$$(3.11) \quad A = \sum_{\nu} a_{\nu} + y(0) \text{ and } B = - \sum_{\nu} a_{\nu}$$

The general solution is, therefore,

$$(3.12) \quad y(x) = e^{x/2} \left[ y(0) - \sum_{\nu} \frac{a_{\nu}}{(i\alpha_{\nu} - 1)} \right] + e^{-x/2} \sum_{\nu} \frac{a_{\nu}}{(i\alpha_{\nu} - 1)} e^{i\alpha_{\nu} x}; \quad \underline{0 \leq x \leq x_1}$$

It should be noted that the numerical values for the solution (3.12) are found to be comparable, within  $\pm 0.5 \%$ , on the average, with those obtained by direct integration of (3.1), reflecting the validity of the approximation (3.4) and also the numerical stability of the solution.

(ii) In the region  $x_1 \leq x \leq x_2$ , the solution  $y$  satisfies also (3.5), but with  $r(x)$  given in the form:

$$(3.13) \quad r(x) = e^{-x/2} \sum_{\nu=0}^3 i\beta_{\nu} b_{\nu} e^{i\beta_{\nu} x}$$

Hence, the general solution is:

$$(3.14) \quad y(x) = e^{x/2} \left[ A - \sum_{\nu} \frac{i\beta_{\nu} b_{\nu} e^{(i\beta_{\nu}-1)x_1}}{(i\beta_{\nu} - 1)} \right] + e^{-x/2} \left[ B + \sum_{\nu} \frac{b_{\nu} e^{i\beta_{\nu} x}}{(i\beta_{\nu} - 1)} + \sum_{\nu} b_{\nu} e^{i\beta_{\nu} x_1} \right]$$

The linearized tidal theory requires that contact should be maintained at the boundaries between the regions, i.e. it requires continuity in  $y(x)$  and  $y'(x)$ . Thus the constants  $A$  and  $B$  are determined as:

$$(3.15) \quad A = y(1) e^{-x_1/2} + \sum_{\nu} b_{\nu} e^{(i\beta_{\nu}-1)x_1} \text{ and } B = \sum_{\nu} b_{\nu} e^{i\beta_{\nu} x_1}$$

Therefore, the general solution assumes the form:

$$(3.16) \quad y(x) = e^{x/2} \left[ y(1) e^{-x_1/2} - \sum_{\nu} \frac{b_{\nu} e^{(i\beta_{\nu}-1)x_1}}{(i\beta_{\nu} - 1)} \right]$$

$$+ e^{-x/2} \sum_v \frac{b_v e^{i\beta_v x}}{(i\beta_v - 1)} ; \underline{x_1 \leq x \leq x_2}$$

(iii) In the region  $x_2 \leq x \leq x_1$ , the type of data, similar to those utilized in (i) and (ii) for the evaluation of  $V(x)$ , is scarce. However, inferences on the existence of the tidal patterns are provided by other techniques-observation [4]. By inspection,  $V(x)$  is speculated to be expressed as:

$$(3.17) V(x) = (c_1 e^{i\gamma_1 x} + c_2 e^{i\gamma_2 x}) e^{x/2}$$

The harmonic coefficients are determined to meet the requirements for  $Q(x)$ , namely:

- a) maximum heating rate occurs in the 50 - 60 km range [4], and
- b) heating rate  $Q$  vanishes at and above 80 km [2].

An expression for  $Q(x)$  is obtained by differentiation of (3.1) and substitution into (1.1), this gives:

$$(3.18) (x) = (\mu^2(x) + \frac{1}{4})y + e^{-x/2}V'$$

By further differentiation, we find

$$(3.19) Q'(x) = Q(\rho + \frac{1}{2}) + e^{-x/2}(V'' - V'(1 + \rho) + (\mu^2 + \frac{1}{4})V)$$

In the present model, it is assumed that  $Q$  (and identically  $Q'$ )  $\rightarrow 0$  at  $x = x_3$ , corresponding to height around 82 km; this level is characterized by  $\rho = 0$ . In this case,  $V$  satisfies:

$$(3.20) V'' - V' + (\mu_3^2 + \frac{1}{4})V = 0; \mu_3^2 = \mu^2(x_3)$$

whose solution is:

$$(3.21) V(x) = (c_1 e^{i3x} + C_2 e^{-i3x}) e^{x/2}$$

On the other hand, the level at which maximum heating occurs (i.e.  $Q' = 0$ ) corresponds, in the present model, to  $x = x_2$ , and is characterized by the minimum value of  $\rho = \rho_2$ . Therefore, (3.19) reduces to:

$$(3.22) V'' - V'(1 + \rho_2) + (\mu^2 + \frac{1}{4})V = Q_2(\rho_2 + \frac{1}{2}) e^{x_2/2}, \text{ at } x = x_2$$

Substituting for  $V$  as given by (3.21), together with the requirement of continuity in  $V_2$  at  $x = x_2$ , the coefficients  $c_1$  and  $c_2$  are determined.

$$(3.23) c_1 = e^{-i\mu_3 x_2} (q_2 + V_2 e^{-x_2/2} / 2) \text{ and } c_2 = -e^{i\mu_3 x_2} (q_2 - V_2 e^{-x_2/2} / 2)$$

where

$$(3.24) q_2 = (V_2 e^{-x_2/2} (\mu_2^2 - \mu_2^2 - \rho_2/2) + Q_2(\rho_2 + \frac{1}{2})) / 2 \mu_3 \rho_2$$

Therefore, the vertical dependence terms  $V(x)$  are obtained in the range  $x_2 \leq x \leq x_3$ , by substituting for  $c_1$  and  $c_2$  (3.23) in (3.21). Following similar procedures, as for the previous two regions, the general solution to (3.5) is:

$$(3.25) \quad y(x) = Ae^{x/2} + Be^{-x/2} + e^{x/2} \int_{x_2}^x e^{-x/2} \{ (V_2 + i\mu_3) c_1 e^{i\mu_3 x} + (\frac{1}{2} - i\mu_1) c_2 e^{-i\mu_3 x} \} dx - e^{-x/2} \int_{x_1}^x e^{x/2} \{ (\frac{1}{2} + i\mu_3) c_1 e^{i\mu_3 x} + (1/2 - i\mu_3) c_2 e^{-i\mu_3 x} \} dx$$

The constants of integration A and B satisfy the initial values of  $y(x_2)$  and  $y'(x_2)$ , thus:

$$A = y(2) e^{-x_2/2} + V(2) e^{-x_2} \text{ and } B = -V(2)$$

Hence the general solution is:

$$(3.26) \quad y(x) = e^{(x - x_2)/2} \left\{ y(2) - \frac{c_1 e^{i\mu_3 x_2}}{(i\mu_1 - 1/2)} + \frac{c_2 e^{-i\mu_3 x_2}}{(i\mu_1 + 1/2)} \right\} + \left\{ \frac{c_1 e^{i\mu_3 x}}{(i\mu_1 - 1/2)} - \frac{c_2 e^{-i\mu_3 x}}{(i\mu_1 + 1/2)} \right\}; \quad x_2 \leq x \leq x_1$$

(iv) In the region  $x_3 \leq x \leq x_4$  and above, the forcing function  $Q(x)$  vanishes and, therefore, (1.1) reduces to the homogeneous form, with the variable coefficient as approximated in (2.2).

On using the transformation:

$$(3.27) \quad s(x) = (2/3p) \mu^3(x), \mu^2 < 0$$

the homogeneous equation  $d^2 y/dx^2 + \mu^2(x) y = 0$  reduces to

$$(3.28) \quad d^2 y/ds^2 + (1/3s) dy/ds + y = 0$$

Writing

$$(3.29) \quad s = (2i/3) t^{3/2}$$

eq. (3.28) assumes the form:

$$(3.30) \quad d^2 y/dt^2 - ty = 0.$$

This equation is Airy's equation [7], whose general solution is given in terms of Bessel functions of the first kind  $J_{\pm 1/3}$  in the form:

$$(3.31) \quad y = t^{1/2} [a J_{1/3}(2it^{3/2}/3) + bj - 1/3(2it^{3/2}/3)],$$

or in terms of  $s$ , the solution is:

$$(3.32) \quad y = \mu [A J_{1/3}(s) + B J_{-1/3}(s)]; \quad \underline{x_1 \leq x \leq x_1}$$

In case of  $\mu^2 < 0$  ( $= -\lambda^2$ ), the transformation is:

$$(3.33) \quad \sigma(x) = (2/3p) \lambda^3(x),$$

and the solutions are expressed in terms of the modified Bessel functions of the first kind as

$$(3.34) \quad y = \lambda [-A I_{1/3}(\sigma) + B I_{-1/3}(\sigma)]; \quad \underline{x_3 \leq x \leq x_4}$$

The constants of integration A and B are determined to satisfy the requirement of continuity in y and y' at  $x = x_1$ .

(v) In the uppermost region  $x_4 \leq x \leq x_5$ , the variable coefficient  $\mu^2(x)$ , in the homogeneous-form equation of (1.1), has been adjusted to meet smoothly the model given by (2.3).

Writing

$$(3.35) \quad s(x) = 8 \sqrt{\tau} e^{x/8}, \quad \mu^2 > 0$$

the homogeneous equation reduces to Bessel's differential equation:

$$(3.36) \quad d^2y/ds^2 + (1/s)dy/ds + (1 - 16/s^2)y = 0,$$

whose solutions are Bessel functions  $J_4$  and  $Y_4$  of the the first and second kinds, respectively, of order 4. Hence the general solution is:

$$(3.37) \quad y(x) = A J_4(s) + B Y_4(s); \quad \underline{x_4 \leq x \leq x_5}$$

If  $\mu^2 < 0$  ( $= -\lambda^2$ ), ( $i\sigma = s$ ), we get the modified Bessel equation whose solutions are the modified Bessel functions  $I_4$  and  $K_4$ :

$$(3.38) \quad y(x) = A I_4(\sigma) + B K_4(\sigma); \quad \underline{x_4 \leq x \leq x_5}$$

In this case,

$$(3.39) \quad A = 0,$$

in order to comply with the upper boundary condition of bounded y(x) at  $x^* = x_5$ . Therefore,

$$(3.40) \quad y(x) = B K_4(\sigma); \quad \underline{x_4 \leq x \leq x_5}$$

The constants A and B are determined to satisfy the requirements of continuity in the solution at  $x = x_4$ .

This completes the method of obtaining the solutions of the linear second order equation (1.1) in the five regions of the model as given in table 1.



## REFERENCES:

- S. CHAPMAN R. LINDZEN, *Atmospheric Tides*, D. Reidel, Amsterdam (1970)
- S.T. BUTLER K. A. SMALL, Proc. Roy. Soc. A274, 91 (1963)
- M. SIEBERT, "Atmospheric Tides", *Adv. Geophys.* 7, Acad. Press, N.Y. (1961)
- G. V. GROVES, J. Birt. Interp. Space, 30, 32, (1977)
- S. H. MAKARIOUS, Comm. Fac. Sci. Univ. Ankara, Math. 31, 95, (1982)
- S. H. MAKARIOUS, Archiv. Mechanics, 31 (1), 125, (1979)
- C. J. TRANTER, "Bessel Functions Applications", English Univ. Press, London (1968)