



## Aqueous Extracts of *Aaronsohnia pubescens* subsp. *pubescens* Aerial Parts as Green Corrosion Inhibitor for Mild Steel in Hydrochloric Acid Solution

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**Abstract:** In this study, two aqueous extracts from the aerial parts of *Aaronsohnia pubescens* subsp. *pubescens* (Odorized aqueous extract (OE) and Deodorized aqueous extract (DE)) were used as some novel ecological corrosion inhibitors for mild steel (MS) in 1 M HCl medium. For this reason, the inhibition behavior of the OE and DE were investigated using weight loss measurements, electrochemical assays, kinetics, and thermodynamic parameters, and electrochemical methods, both stationary (Potentiodynamic polarization (PDP)) and transient (Electrochemical impedance spectroscopy (EIS)). The obtained results showed that EO and DE act as effective corrosion inhibitors and the inhibition efficiency of inhibitors increases for the concentration of 1.5 g/L; reaching some high values of 93.11 and 87.88% in 1 M HCl solution at 308 K for OE and DE, respectively. Furthermore, PDP measurements exhibited that the studied of each inhibitor performs as a mixed-type inhibitor. The results of the thermodynamic kinetic parameters indicate the adsorption of OE and DE on the MS surface sites obeying the Langmuir adsorption isotherm.

**Keywords:** *Aaronsohnia pubescens* subsp. *pubescens*; aqueous extracts; mild Steel; ecological corrosion inhibitors; 1 M HCl.

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### INTRODUCTION

Mild Steel (MS) is extensively used in many industries such as tanks and water utilities, power production, heat exchangers, oil, chemical, and electrochemical technologies due to good mechanical strength and relatively low price, but it is susceptible to several forms of corrosion in some environments especially in the acidic environment (1, 2). This phenomenon can be minimized or

delayed by various means such as coatings, cathodic protection, and corrosion inhibitors (3). Corrosion inhibitors, classified as inorganic and organic types, are one of the most cost-effective methods for controlling corrosion. The most well-known acid corrosion inhibitors are organic compounds that adsorb on the MS surface and protects it from corrosion by blocking the active sites. These inhibitors are rich in electrons and can share their electrons with unoccupied d-orbitals of

steel (4). Nowadays, the researchers' interests are directed towards environmental-friendly inhibitors (i.e., biodegradable molecules). The essential oils (EOs) and extracts components from a variety of plants origins as eco-friendly sources of sustainable corrosion inhibitors (5-9). These types of inhibitors, which are readily available through a simple extraction process, are able and effective to protect the metal from corrosion (10).

In our laboratory, a great deal of research has been carried out to study inhibitive effect several plant extract on the corrosion of steel in 1 M HCl (11-16). In this context, recently, *Aaronsohnia pubescens subsp. pubescens* essential oil has been established, as an eco-friendly corrosion inhibitor of acid corrosion of MS in 1 M HCl. The inhibition efficiency IE (%) was found to increase with naturally substance content to attain 82.11% at 1.50 g/L (17).

The main objective of current research is to study for the first time the potency of the power of extracts from the aerial parts of *Aaronsohnia pubescens subsp. pubescens* Figure 1 (Odorized aqueous extract (OE) and Deodorized aqueous extract (DE)) to protect mild steel in 1M HCl medium were assessed by WL measurement, PDP, and EIS examinations.

## EXPERIMENTAL PART

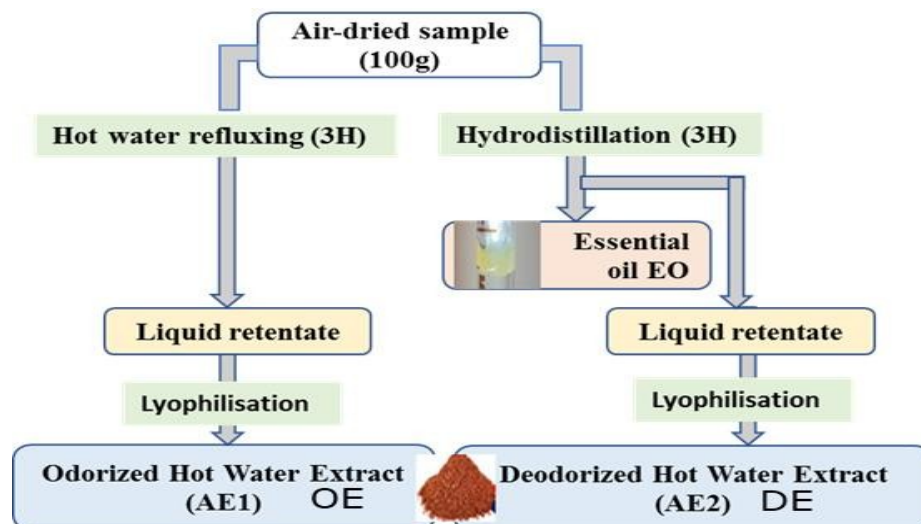
### Inhibitors

The experimental phase followed in the current study such as preparations of the aqueous extract

(OE and DE) have been mentioned according to a previously described experimental procedure in our work (18). A portion (100 g) of dried plant material was extracted with 1 L of water under refluxing for 3 h. The liquid retentate was collected, filtered, and centrifuged at 5000 rpm for 30 min. The supernatant was also filtered to eliminate any residues and lyophilized to give finally odorized aqueous extract (OE) in a yield of 11.37 % (w/w). However, the liquid retentate obtained after completion of hydrodistillation of 100 g dried plant material in 1 L of water for 3 h, using a Clevenger-type apparatus to isolate volatile compounds, was collected, filtered, centrifuged and lyophilized to give finally deodorized aqueous extract (DE) in a yield of 10.82 % (w/w) (19).



**Figure 1:** *Aaronsohnia pubescens subsp. pubescens* in its native habitat in south-eastern Morocco.



**Figure 2:** Scheme of the extraction methods of aqueous extracts from aerial parts of *Aaronsohnia pubescens subsp. Pubescens*.

### Corrosion test

Corrosion inhibition on MS in 1 M HCl by OE and DE was performed by using WL, PDP and EIS methods according to the methodology described previously in our work (13,17). A very low concentration range (0.25-1.5 g/L) of inhibitors were prepared in 1M HCl media for its corrosion

inhibition potential at different temperatures (308-343 K).

### Preparation of MS segments, corrosive solutions and inhibitors

Corrosion tests were conducted on the MS segments with dimension of 2 cm×2 cm×0.05 cm; the MS metal presents the subsequent composition

with mass percentage (%): P 0.09, Si 0.38, Al 0.01, Mn 0.05, C 0.21, S 0.05 and Fe 99.21. Before each corrosion test, the MS segments were mechanically ground with sequential grades of emery papers (400, 600 and 1200 grit), and ensuing rinsed and degreased with distilled water and acetone, then dried and weighed. The corrosive acid solution was a molar hydrochloric acid (1 M of HCl), was prepared from concentrated commercial acid of HCl (37%) by dilution with distilled water.

### Electrochemical (PDP and EIS) measurements

Before conducting each electrochemical corrosion test, the sample was immersed in the test solution during 30 min at the open circuit potential ( $E_{OC}$ ) to find a steady state. Both PDP and EIS tests were performed from utilizing an assembly of electrochemical cell containing three electrodes: a disc cut from the MS as working electrode ( $1\text{ cm}^2$ ), a saturated calomel electrode as a reference electrode, and a platinum electrode as counter electrode. All electrochemical measurements were carried out using a potentiostat/galvanostat (Model PAR 263A) and the electrochemical parameter values were determined using the Volta Master 4 software. We note that all potentials measurement in this study were obtained with respect to the potential value of the reference electrode.

## RESULTS AND DISCUSSION

### Effect of both concentration and temperature

The effect of different concentrations of OE and DE on MS corrosion in 1 M HCl at 308 K was investigated using the gravimetric method. The inhibition efficiency (IEW (%)) was calculated on the basis of the Equation 1:

$$IE \% = \frac{W_{corr} - W_{corr(inh)}}{W_{corr}} \times 100 \quad (\text{Eq. 1})$$

where  $W_{corr}$  and  $W_{corr(inh)}$  are the values of corrosion rate of MS in 1 M HCl medium without and with the addition of the aqueous extracts tested.

The obtained results of the study are summarized in Table 1. It shows that the corrosion rate reduces and the IE (%) increase with concentrations and reach a maximum value of 93.46 and 80.48 % at 1.5 g/L of OE and DE, respectively. These results suggesting that the aqueous extracts inhibited the corrosion of MS in a dose-dependent manner. This behavior can be attributed to the strong interaction

of the compounds forming these extracts with the metal surface. In other words, we observed that the inhibition efficiency of OE is slightly increased when the temperature media increases, which results probably to the chemisorption behavior of OE onto MS surface.

### PDP investigation

The effect of EO and DE at 308 K on anodic and cathodic reactions was demonstrated by PDP plots in 1 M HCl medium and the embodiments obtained are displayed in Figures 3 and 4. The outputted parameters of PDP analysis including the potential of corrosion ( $E_{corr}$ ), the current density of corrosion ( $I_{corr}$ ) and cathodic and anodic Tafel slopes ( $\beta_a$  and  $\beta_c$ ) are given in Table 2. The corrosion inhibition efficiency  $IE_{PDP}$  (%) was derived as given below:

$$IE_{PDP} \% = \left( \frac{I_{corr} - I_{corr, inh}}{I_{corr}} \right) \times 100 \quad (\text{Eq. 2})$$

Where  $I_{corr}$  and  $I_{corr, inh}$  are the corrosion current densities in the absence and the presence of inhibitor, respectively.

According to Figures 3 and 4, we have noticed that the use of OE and DE at 308 K are suppressed both the cathodic hydrogen development and anodic metal dissolution reactions. Moreover, the PDP curves in the inhibited solutions were translated into lower current densities. The polarization diagrams noted that the addition of different concentrations of the two aqueous extracts that both the cathodic and anodic reactions did not affect, as well as the corresponding  $E_{corr}$  appeared to be approximately constant significant. Therefore, EO and DE can be classified as mixed-type inhibitors (20). In addition, the results of Table 2 indicate that the rate of the  $I_{corr}$  values of MS is decreased with an increase in the concentrations of the two inhibitors; reaching some high values of 517 and 862  $\mu\text{A}/\text{cm}^2$  in 1 M HCl solution at 308 K for OE and DE, respectively at 1.5 g/L. These results suggest that the addition of EO and DE loading more compounds of both adsorbed on the MS surface, and thus the corrosion-resistant film can be generated on the metal surface (21). As shown in Table 2, the  $IE_{PDP}$  (%) of EO and DE in the 1 M HCl solution is about 91.02% and 85.05% respectively. It can be concluded from these findings that both aqueous extracts provided the good anti-corrosion performance, with a clear preference for OE.

**Table 1:** Weight loss results for MS in 1 M HCl with and without different concentrations of aqueous extracts (OE and DE) at different temperatures.

C (g/L)	308 K		313 K		323 K		333 K		343 K	
	W (mg/cm <sup>2</sup> .h)	IE% (%)	W (mg/cm <sup>2</sup> .h)	IE% (%)	W (mg/cm <sup>2</sup> .h)	IE% (%)	W (mg/cm <sup>2</sup> .h)	IE% (%)	W (mg/cm <sup>2</sup> .h)	IE% (%)
<b>OE 1M HCl</b>	<b>0.942</b>	.....	<b>1.751</b>	.....	<b>2.836</b>	.....	<b>3.641</b>	.....	<b>6.301</b>	.....
0.25	0.186	80.25	0.344	80.37	0.532	81.24	0.682	81.28	1.115	82.30
0.50	0.116	87.66	0.214	87.78	0.320	88.70	0.409	88.78	0.638	89.88
1.00	0.108	88.58	0.197	88.74	0.315	88.88	0.404	88.90	0.633	89.96
1.50	0.065	93.11	0.119	93.22	0.189	93.33	0.241	93.39	0.412	93.46
<b>DE</b>	0.224	76.21	0.470	73.15	0.824	70.95	1.064	70.77	1.872	70.29
0.50	0.193	79.50	0.378	78.44	0.622	78.08	0.822	77.42	1.426	77.37
1.00	0.152	83.89	0.309	82.38	0.507	82.12	0.667	81.68	1.170	81.43
1.50	0.114	87.88	0.276	84.23	0.473	83.33	0.621	82.95	1.230	80.48

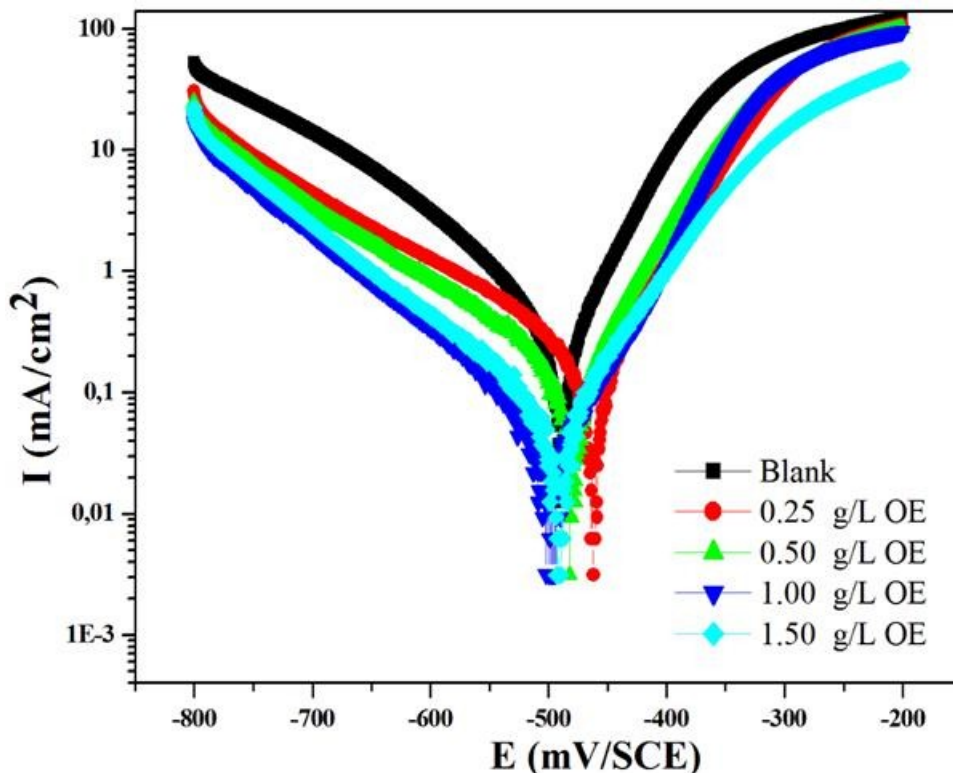


Figure 3: Anodic and cathodic polarization curves of MS in solutions of 1 M HCl without and with different concentrations of odorized extract.

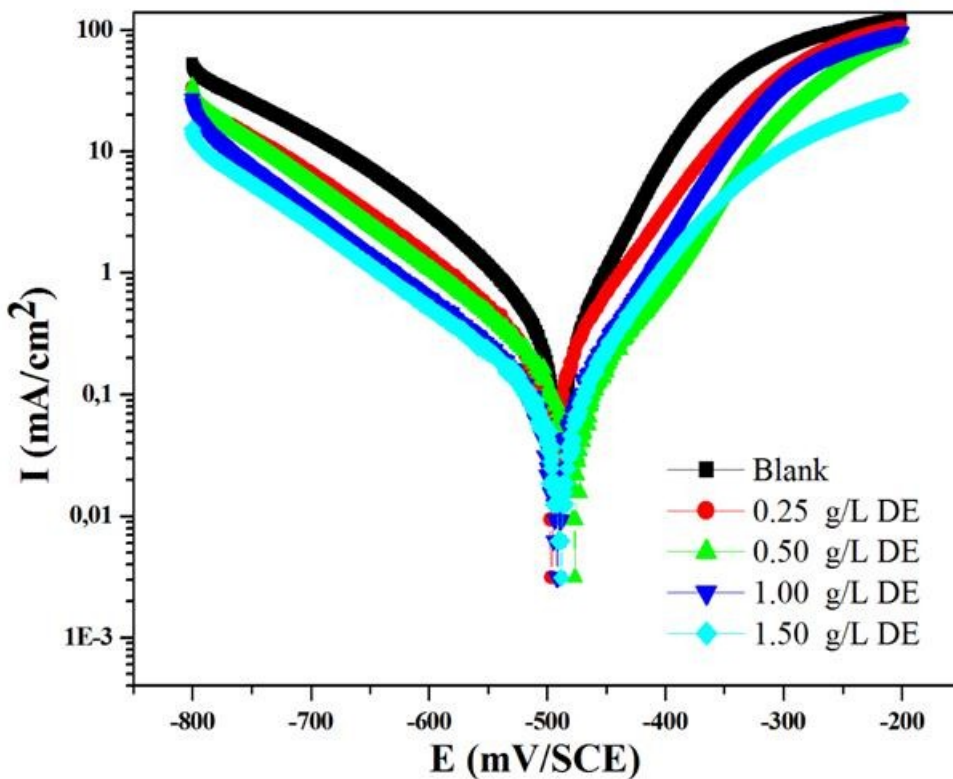


Figure 4: Anodic and cathodic polarization curves of MS in solutions of 1 M HCl without and with different concentrations of deodorized extract.

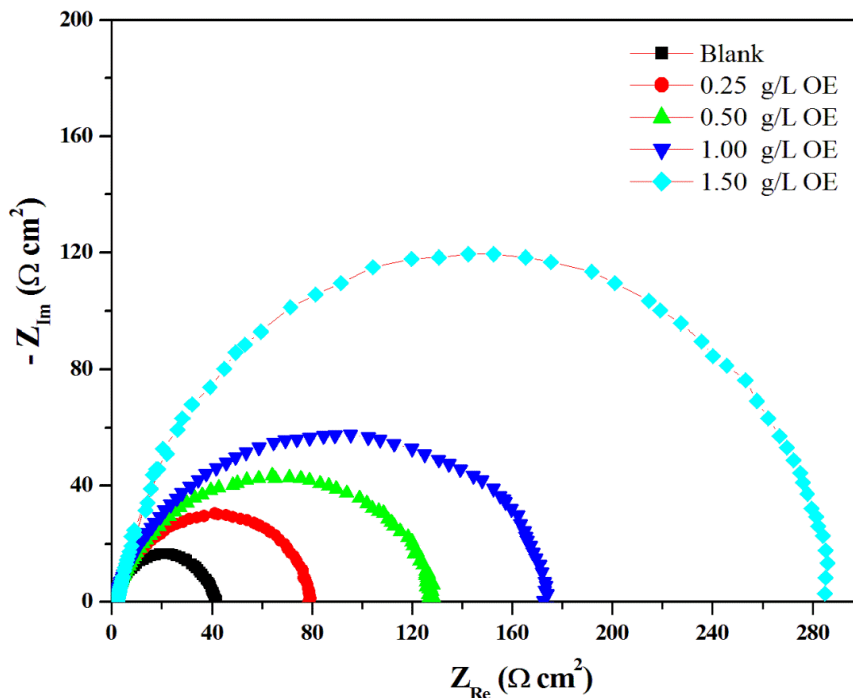
**Table 2:** Electrochemical parameters for the MS in 1 M HCl with and without various concentrations of aqueous extracts from *Aaronsohnia pubescens* aerial parts (OE and DE) at 308 K.

	C (g/L)	- E <sub>corr</sub> (mV/SCE)	I <sub>corr</sub> (mA cm <sup>-2</sup> )	-β <sub>c</sub> (mV dec <sup>-1</sup> )	β <sub>a</sub> (mV dec <sup>-1</sup> )	IE <sub>PDP</sub> (%)
<b>1 M HCl</b>		490.0	0.5779	147.4	74.8	.....
<b>OE</b>	0.25	462.9	0.1145	110.2	60.8	80.18
	0.50	460.1	0.0857	100.1	67.1	85.17
	1.00	498.9	0.0701	109.2	62.9	87.86
	1.50	497.0	0.0517	100.7	65.0	<b>91.02</b>
<b>DE</b>	0.25	497.8	0.1651	110.6	74.3	71.43
	0.50	480.8	0.0997	104.8	73.5	82.74
	1.00	495.3	0.0897	110.7	72.1	84.47
	1.50	494.0	0.0862	106.5	74.4	85.05

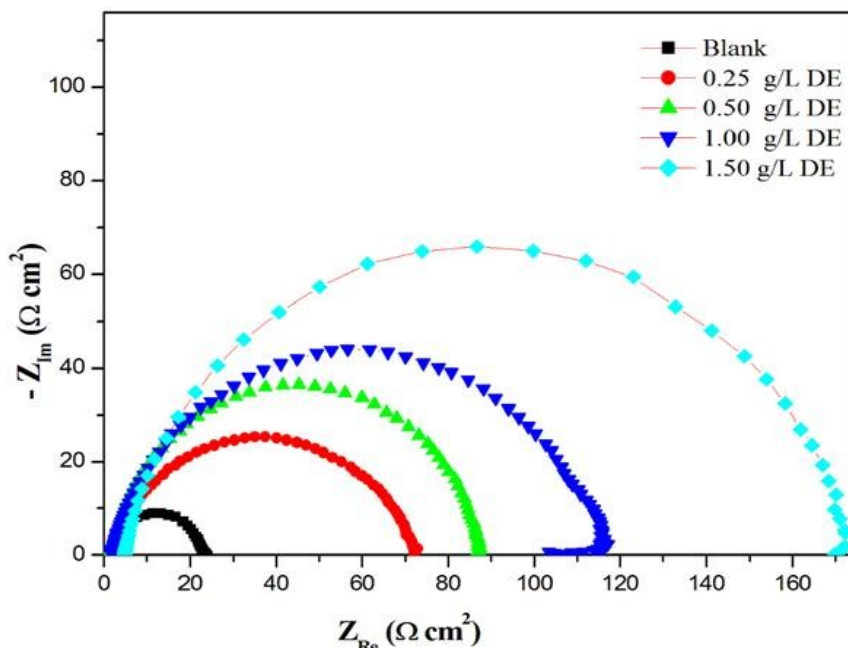
**EIS investigation**

The EIS is a convenient and rapid approach for examining the protective properties of inhibitors onto metal surfaces in different corrosive environments (22). Thus, it was used to evaluate

the effectiveness of the two aqueous extracts tested. The EIS measurements of the immersed MS in 1 M HCl medium protected with various concentrations of EO and DE at 308 K are depicted in Figures 5 and 6 sequentially.



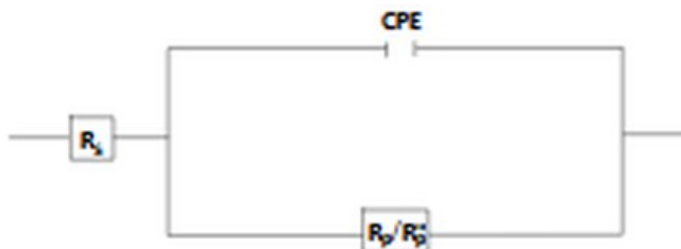
**Figure 5:** The Nyquist plots of the immersed MS in 1 M HCl without and with different concentrations of OE at 308 K.



**Figure 6:** The Nyquist plots of the immersed MS in 1 M HCl without and with different concentrations of DE at 308 K.

In the present investigation, the Nyquist plots of EO and DE (Figures 5 and 6) showed a single capacitive loop whose size increases with increased concentrations of both aqueous extracts employed (23,24). However, these capacitive loops are not the perfect semicircles because of a frequent

dispersion effect attributing to roughness because of heterogeneous solid surface (25-27). In addition, the diameter of the Nyquist plots increases as a function of the concentration of each inhibitor, which affirms the adsorption of the EO and DE molecules on the MS surface.



**Figure 7:** Equivalent circuit used to fit the experimental EIS data of the immersed MS in 1 M HCl without and with different concentrations of OE and DE.

Furthermore, the impedance curves were fitted by using EC-LAB software, and an equivalent electrical circuits (EEC) diagram corresponds to the metal/solution interface (the double layer between the MS / EO / HCl and MS / DE / HCl) was proposed in Figure 7 (28-30). As reported in Figure 7, the equivalent circuit elements consisting of solution resistance ( $R_s$ ) connected in ( $CPE_{dl}$ ) represent the constant phase element coupled with the polarization resistance ( $R_p$ ). In this circuit,  $R_p$  corresponds to the sum of charge transfer resistance ( $R_{ct}$ ) and diffuse layer resistance ( $R_d$ ) at the metal/solution interface in the absence of OE and DE ( $R_p = R_{ct} + R_d$ ). While that ( $R''_p$ ) corresponds to the sum of  $R_p$ ,  $R_a$  (accumulated species) and  $R_f$  (film resistance) in the presence of

the two studied extracts ( $R''_p = R_p + R_a + R_f$ ) (31,32). The  $CPE_{dl}$  is defined as follows:

$$Z_{CPE} = \frac{1}{Y_2(j\omega)^2} \tag{Eq. 3}$$

Where  $Y_0$  benefits from the possibility of a non-ideal capacitance of ( $CPE_{dl}$ ), ( $\omega$ ) is the angular frequency and ( $j$ ) is the imaginary unit, and  $n$  is the phase shift, which gives details about the degree of surface inhomogeneity for whole numbers ( $0 < n < 1$ ) (29,33).

The inhibition efficiency  $E_{EIS}$  (%) is designed according to (Equation 4), where  $R''_p$  and  $R_p$  are the

polarization resistance in the presence and absence of inhibitors, respectively.

$$IE_{EIS}(\%) = \left( R_{p_{inh}} - \frac{R_p}{R} \right) \times 100 \quad (\text{Eq. 4})$$

The impedance data that were fitted according to the equivalent circuit and inhibition efficiency ( $IE_{EIS}$  %) are listed in Table 3. According to the fitted results, that the double layer capacitance ( $C_{dl}$ ) values were reduced for the inhibited samples, evidencing the enhancement of the OE and DE molecules adsorption onto the surface. The reduction of the ( $CPE_{dl}$ ) values for the protected samples is attributed to the replacement of water molecules adsorbed on the metal surface with the

compounds of OE and DE at the metal /solution interface (34). In addition, we noticed that the values of  $R_p$  increases with the increase of different concentrations of two aqueous extracts to reaches its maximum values 288.10 and 174.05 ( $\Omega.cm^2$ ) at 1.5 g/L for the OE and DE respectively. Consequently, the inhibition efficiencies ( $IE_{EIS}$ %) of OE and DE showed the maximum  $IE_{EIS}$  is approximate 92.09% and 86.91% respectively. Thus, it reveals that the OE and DE molecules have considered as a useful green inhibitors to protect MS against corrosion and to reduce the reactive sites which could be created during corrosion phenomenon (35). These results are in good agreement with the results obtained by PDP investigation and show that OE has the best inhibitory performance compared to DE.

**Table 3:** The electrochemical data obtained from the fitting of EIS curves for MS immersed in 1 M HCl without and with various concentrations of OE and DE at 308 K.

C (g/L)	$R_s$ ( $\Omega.cm^2$ )	$R_p$ ( $\Omega.cm^2$ )	$CPE_{dl}$ $Y_o$ ( $\times 10^6 S^n \Omega^{-1}cm^{-2}$ )	n	$C_{dl}$ ( $\times 10^6 S \Omega^{-1}cm^{-2}$ )	$IE_{EIS}$ (%)
Blank						
0.00	1.699	22.78	327.88	0.902	92.88	-
<b>EO</b>						
0.25	1.731	80.08	223.09	0.891	58.27	71.55
0.50	1.772	133.02	118.18	0.866	45.72	82.87
1.00	1.821	174.72	94.08	0.925	42.02	86.96
1.50	1.891	288.10	84.80	0.851	37.88	<b>92.09</b>
<b>DE</b>						
0.25	1.701	76.08	258.01	0.888	64.07	70.05
0.50	1.752	87.98	175.11	0.849	54.00	74.10
1.00	1.791	117.67	107.18	0.981	42.52	80.64
1.50	1.823	174.05	93.22	0.893	39.75	<b>86.91</b>

**Kinetics/Activation parameters**

Inhibitory performance as a function of temperature (T) has been discussed in this part. It is understood that the variation of the corrosion rate as a function of temperature gives results that make it possible to thermodynamically demonstrate the mechanism of OE and DE adsorption onto an MS surface. According to the Arrhenius plot  $\ln(W/T)$  versus  $10^3/T$ , we calculated the enthalpy  $\Delta H^{\circ}_a$  and entropy  $\Delta S^{\circ}_a$  energies; then the standard activation  $E^{\circ}_a$  was calculated from the plot of  $\ln(W)$  against  $10^3/T$ . These parameters are associated for MS without and with inhibitors basing on the following equations: Equation 5 for  $\Delta H^{\circ}_a$  and  $\Delta S^{\circ}_a$  energies (36) and Equation 6 for  $E^{\circ}_a$  energy (37).

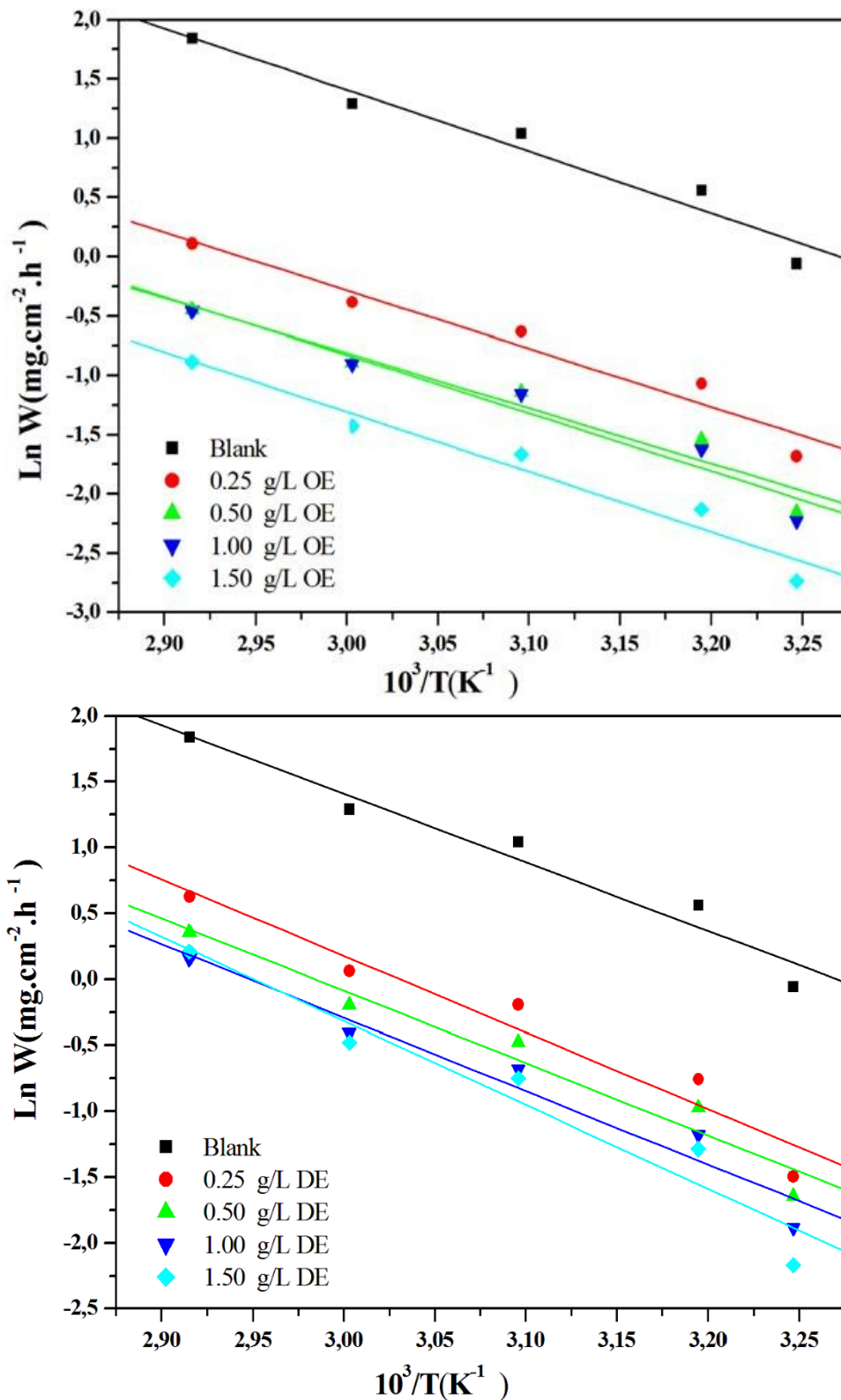
$$\ln \left[ \frac{W}{T} \right] = \ln \left[ \left( \frac{R}{N_a h} \right) + \frac{\Delta S^{\circ}_a}{R} \right] + \left[ \frac{-\Delta H^{\circ}_a}{R T} \right] \quad (\text{Eq. 5})$$

The outputted parameters from the Arrhenius plot (Figures 8 and 9) are listed in Table 4.

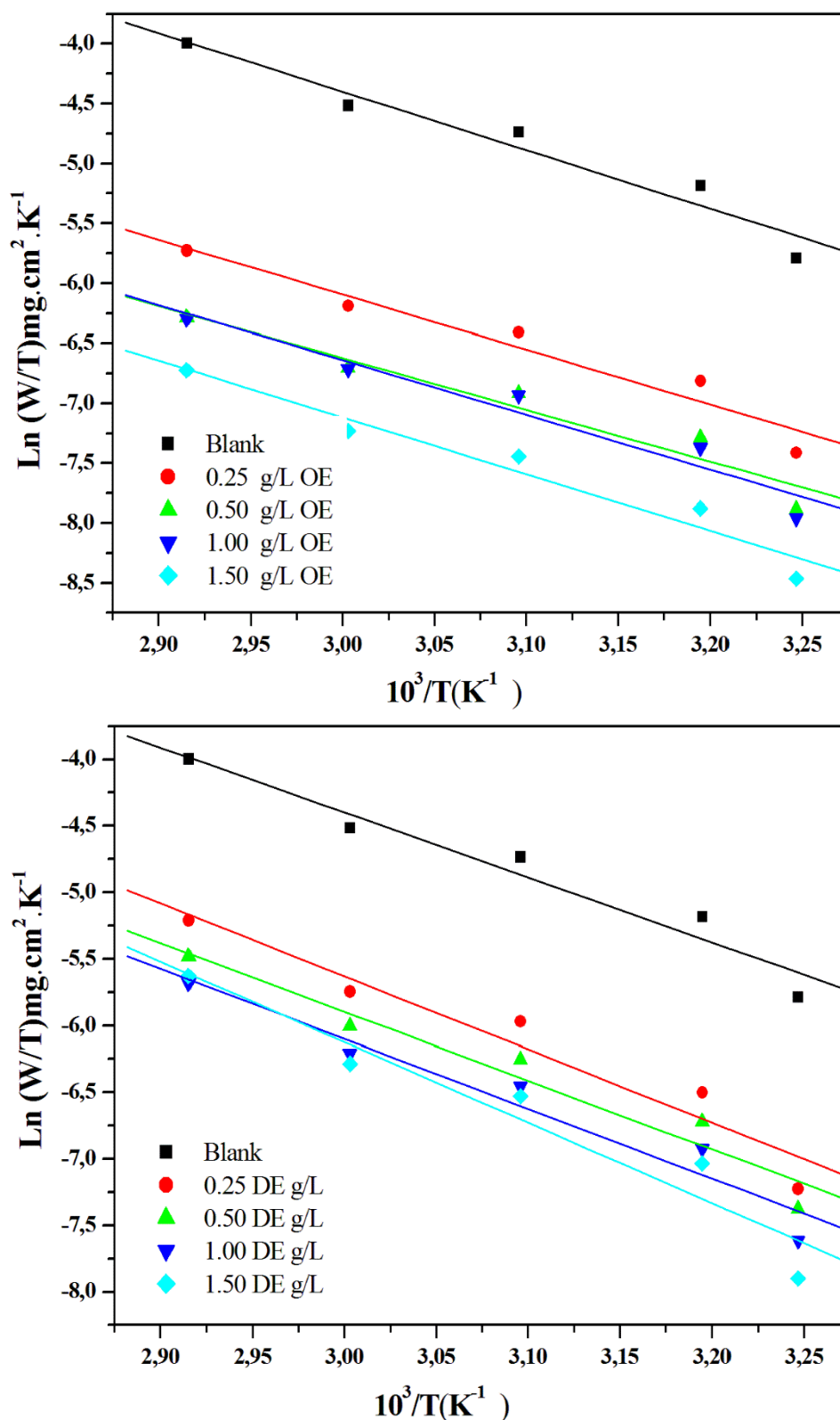
$$\ln W = \ln A + \left[ \frac{-E^{\circ}_a}{R T} \right] \quad (\text{Eq. 6})$$

Where W, R, T, h and  $N_a$  signify the corrosion rate, the universal constant of the ideal gas, the absolute temperature, the Planck’s constant and universal Avogadro number, respectively.





**Figure 8:** Arrhenius plots for MS corrosion rates (W) in 1 M HCl in the absence and presence of different concentrations of each inhibitor.



**Figure 9:** Transition-state plots for MS corrosion rates (W) in 1 M HCl in the absence and presence of various concentrations of each inhibitor.

**Table 4:** Enthalpy  $\Delta H^\circ_a$  and entropy  $\Delta S^\circ_a$  energies for MS without and with various concentrations of OE and DE.

	C (g/L)	$E^\circ_a$ (kJ. mol <sup>-1</sup> )	$\Delta H^\circ_a$ (kJ. mol <sup>-1</sup> )	$E_a - \Delta H^\circ_a$ (kJ. mol <sup>-1</sup> )	$\Delta S^\circ_a$ (J. mol <sup>-1</sup> . K <sup>-1</sup> )
OE	1 M HCl	43.35	40.65	2.70	-112.32
	0.25	40.74	38.04	2.70	-134.24
	0.50	38.62	35.92	2.70	-145.00
	1.00	40.69	38.00	2.70	-138.91
	1.50	42.11	39.42	2.70	-138.61
DE	0.25	48.29	45.59	2.71	-122.13
	0.50	45.66	42.96	2.70	-117.86
	1.00	46.35	43.65	2.70	-117.45
	1.50	52.96	50.26	2.71	-97.82

It is crystal clear from the data in Table 4 that the increase of  $E_w$  (%) with temperature and the lower value of  $E^\circ_a$  are in favor of chemisorption for OE, but are in favor of physical electrostatic nature for DE.

Additionally, the positive value of standard activation enthalpy reveals the endothermic process of corrosion phenomenon of MS (38). However, in other words, the positive value of the standard activation entropy showed a high disorder of the inhibitors molecules during adsorption. (39).

**Adsorption isotherm and thermodynamic parameters**

To get information more about the adsorption and the surface behavior of OE and DE molecules, different models of adsorption isotherms including Langmuir, Temkin and Frumkin were considered with the range of temperature of 308 to 348 K at the different concentrations of OE and DE. The equations related to these isotherms are use these formulas (40):

$$\text{Langmuir : } \frac{C}{\theta} = \frac{1}{K_{ads}} + C \quad (\text{Eq. 7})$$

$$\text{Temkin : } \ln \left[ \frac{C}{\theta} \right] = \ln K_{ads} - g \cdot \theta \quad (\text{Eq. 8})$$

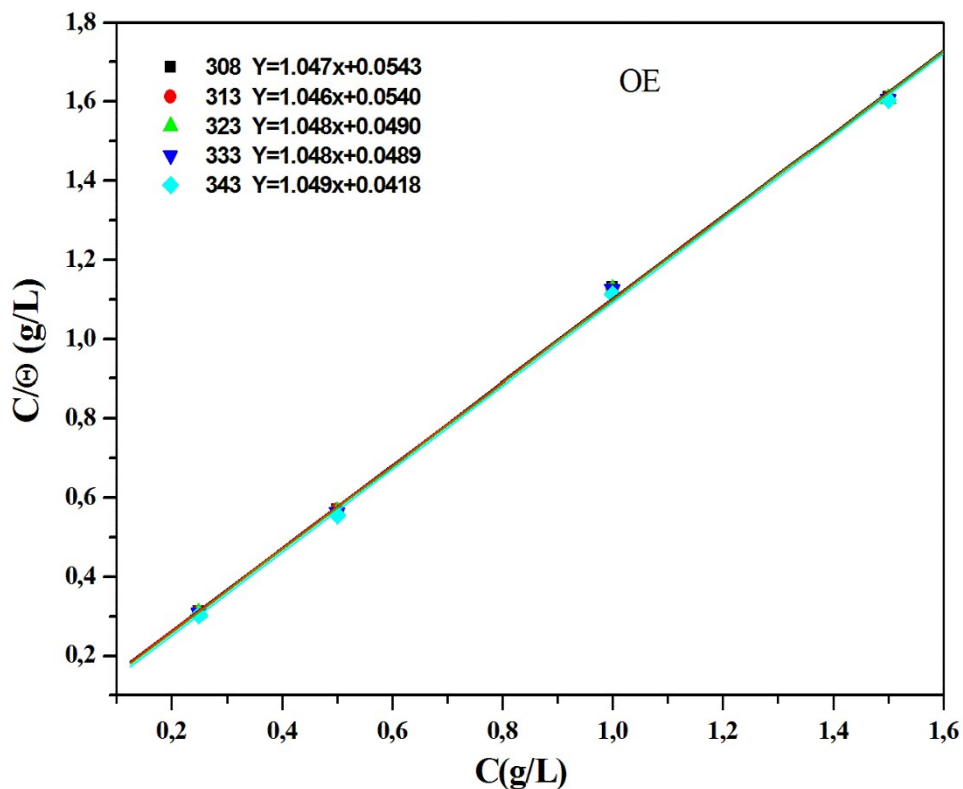
$$\text{Frumkin : } \ln \left[ C \cdot \left( \frac{\theta}{1-\theta} \right) \right] = \ln K_{ads} + g \cdot \theta \quad (\text{Eq. 9})$$

where  $K_{ads}$  is adsorption coefficient,  $\theta$  is the surface coverage and  $C_{inh}$  is the concentrations of the OE and DE.

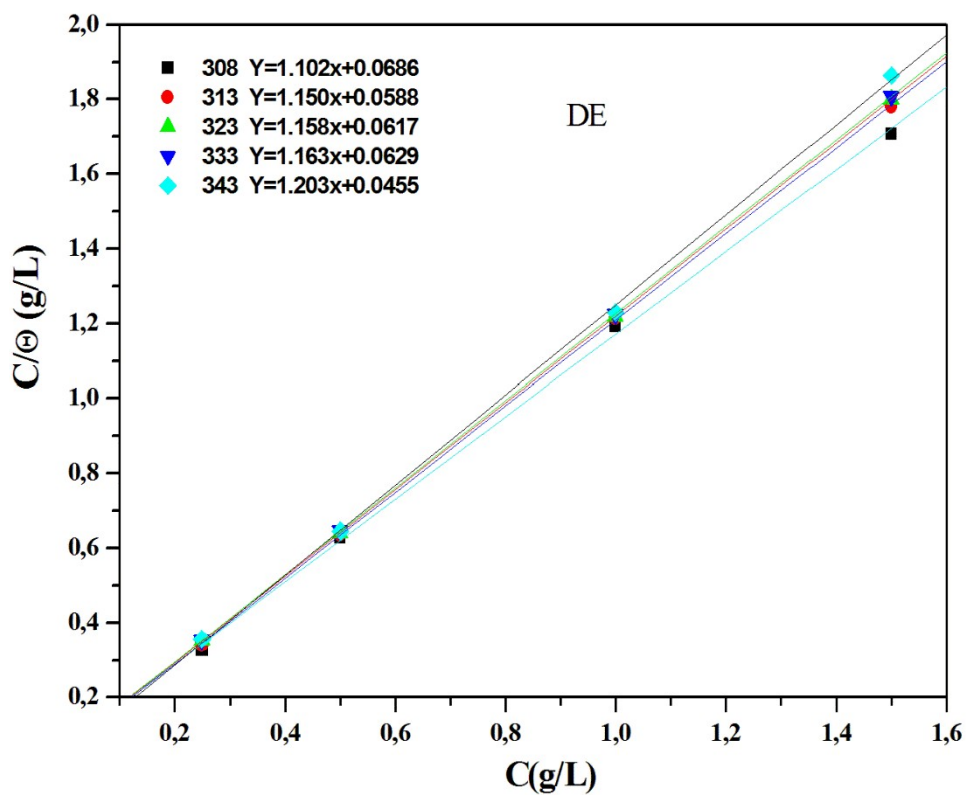
The  $K_{ads}$  values can be calculated from the intercept lines on the  $C_{inh}/\theta$  axis. As shown in the results Figures 10 and 11 and Table 5, the linear regression factor of this isotherm model appears close to 1 for the both aqueous extracts. it is understood that the OE and DE adsorption onto the metal followed the Langmuir isotherm. Using the following equation (Eq. 10) the standard free energy of adsorption  $\Delta G^\circ_{ads}$  for OE and DE was calculated:

$$K_{ads} = \frac{1}{55.5} \exp \left( \frac{-\Delta G^\circ_{ads}}{RT} \right) \quad (\text{Eq. 10})$$

where R, T, 55.5 are gas constant, absolute temperature of experiment the molar concentration of water in solution in respectively.



**Figure 10:** The Langmuir adsorption isotherm of OE on the MS surface in 1 M HCl at different temperatures.



**Figure 11:** The Langmuir adsorption isotherm of DE on the MS surface in 1 M HCl at different temperatures.

**Table 5:** Langmuir isotherm adsorption parameters for 1 M HCl/OE and DE/MS interface at various temperatures.

	T(K)	R <sup>2</sup>	K <sub>ads</sub> (L. g <sup>-1</sup> )	ΔG° <sub>ads</sub> (KJ. mol <sup>-1</sup> )
OE	308	0.999	18.41	-25.66
	313	0.999	18.51	-25.58
	323	0.999	20.40	-26.66
	333	0.999	20.49	-27.50
	343	0.999	24.39	-28.82
DE	308	0.999	14.70	-24.58
	313	0.999	17.24	-25.40
	323	0.998	16.39	-26.07
	333	0.999	16.12	-26.84
	343	0.999	22.02	-28.56

We can conclude from Table 5, OE has a greater value indicating its ability to be absorbed easily and strongly (41). Also, it is clear that, the negative values of ΔG°<sub>ads</sub> suggest that the adsorption of inhibitor molecules onto MS surface is a spontaneous phenomenon. The predominant adsorption mode of OE and DE depends upon factors such as the nature of the extract molecules, type of acid anion, as well as chemical changes in the extracts. Molecular adsorption of the OE and DE at the metal surface can be attributed to the presence of electronegative elements such as oxygen and nitrogen atoms and also to the presence of n-electrons. The high inhibitive performance of OE is due probably to the synergic effect of their volatile especially, E-anethole (15.4%), (E)-heptadeca-10,16-dien-7-one (11.1 %), and Z-β-ocimene (8.6%) were identified as major constituents of the essential oil from *Aaronsohnia pubescens subsp. pubescens* and non-volatile compounds. These results are coherent those of the studies previously reported in our group (12).

## CONCLUSION

The experimental results showed that the odorized aqueous extract (OE) and deodorized aqueous extract (DE) of *Aaronsohnia pubescens subsp. pubescens* proved significant corrosion inhibition activity. PDP curves demonstrate that inhibitors acts as a mixed type inhibitor in 1 M HCl. The inhibition is accomplished by a mixture physical and chemical adsorption of the extract components on the MS surface. The aqueous extracts obeys a Lagmuir adsorption isotherm. The Nyquist diagram showed that adsorption mechanism of OE and DE are governed by a charge transfer process. The high protective efficiency of OE is due to the synergic effect of their volatile and non-volatile molecules.

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