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# Investigation of Potential Prevailing Wind Impact on Land Surface Temperature at Gas Flaring Sites in the Niger Delta, Nigeria

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### Abstract

This research examines the effects of South prevailing wind on Land Surface Temperature (LST) retrieved from Earth Observation (EO) Satellites at 11 gas flaring sites in Rivers State, Niger Delta region, Nigeria. 7 Landsat 5 Thematic Mapper (TM) and 18 Landsat 7 Enhanced Thematic Mapper Plus (ETM+) from 17/01/1986 to 08/03/2013 with < 5 % cloud contamination were considered. All sites are located within a single Landsat scene (Path 188, Row 057). The atmospherically corrected reflectance was used for the classification of 4 land cover (LC) types at each site. The emissivity ( $\varepsilon$ ) for each site is estimated by using standard values for determined LC from Look Up Table (LUT). The surface-leaving radiance ( $L_{\lambda}$ ) is computed from the atmospherically corrected thermal band 6 (High gain) and the emissivity ( $\varepsilon$ ) values. The Planck equation was inverted using Landsat calibration constants to derive LST. Geospatial analysis of LST results using ArcGIS show 6 ranges of LST values for all sites. For both sensors LST retrieved for the flare stack sources are the highest values compared to other locations within the sites. Wind directions and wind speeds for Landsat data acquisitions dates and the South prevailing wind were applied to the LST for assessing their effects on it. The results show that for Eleme I and II, and Onne, the p-values results showed that no statistically significant relationships between  $\delta$ LST values in different directions ( $\delta$ LST<sub>NE</sub>,  $\delta$ LST<sub>NS</sub> and  $\delta$ LST<sub>NW</sub>) existed. For Obigbo site, the wind direction (South) for data acquisition date combined with the South prevailing wind to generate a noticeable impact on the LST towards the North-East and the North-West directions. For Alua, Bonny, Chokocho, Rukpokwu, Umurolu and Sara sites, the p-value obtained is statistically significant for all the 3 ( $\delta$ LST<sub>NE</sub>,  $\delta$ LST<sub>NE</sub> and  $\delta$ LST<sub>NW</sub>) relationships; therefore, producing a circle flare  $\delta$ LST footprint. For Umudioga site, only  $\delta LST_N$  versus  $\delta LST_N$  is statistically significant, causing a noticeable effect on the flare  $\delta LST$  in the North-West direction. Based on these results, it can be concluded that the volume and rate of burning gas, and the speed of the South wind at the time of satellite overpass are major factors that determine the influence of the South prevailing wind on the LST retrieved at the flaring sites in the Niger Delta.

Keywords: Investigation, prevailing, wind, land surface temperature, gas flaring, Niger Delta.

### Introduction

Gas flaring (GF) is part of the upstream oil and gas industry processes as a means of disposing of unwanted natural gas or as a measure for pressure relief through high temperature oxidation at the tip of a stack (Caseiro et al., 2018). GF are a globally, regionally and locally significant source of atmospheric pollutants (Nwaogu and Onyeze, 2020; Caseiro, et al., 2019). They can be detected by satellite remote sensing technology (Morakinyo, et al., 2020b). Several negative impacts of GF on the immediate surrounding (Nwaogu and Onyeze, 2020; Akinola, 2018) among others include increase in surface temperature (Lu et al., 2020; Dung et al., 2008), noise (Nwoye et al., 2014; Ismail and Umukoro, 2012), light pollution (Morakinyo, 2015), air pollution (Sekyi, 2017; Edino et al., 2010), visual pollution (Aromolaran, 2012; Ajao and Anurigwo, 2002) and heat stress (Aromolaran, 2012; Julius, 2011).

Most of the satellite techniques currently applied for detecting gas flaring platforms and for assessing their spatio-temporal variations (Liu et al., 2018; Zhang et al., 2015; Anejionu et al., 2015; Elvidge et al., 2013; Anejionu et al., 2014; Casadio et al., 2012; Ülker et al. 2020) are based on measurements acquired by different sensors e.g., Operational Linescan System (OLS), Moderate Resolution Imaging Spectroradiometer (MODIS), Visible Infrared Imaging Radiometer Suite (VIIRS), Along-Track Scanning Radiometer (ATSR), Land Remote Sensing Satellite (Landsat) in different portions of the electromagnetic spectrum (visible (VIS), near-infrared (NIR), shortwave infrared (SWIR), middle infrared (MIR), thermal infrared (TIR) (Faruolo et al., 2018). The combustion of natural gas in the air at the flaring sites typically results in radiant temperatures usually within the range of (1450-2200) K (Elvidge et al., 2015; Zhang et al., 2015; Faruolo et al., 2014; Elvidge et al., 2013; Reed, 1986) with a mean of around 1750 K (Elvidge et al., 2015; Zhang et al., 2015; Faruolo et al., 2014). The climate assessments for the study

environment highlight the atmospheric pattern of the study area. The assessments of climatic parameters such as wind directions and wind speeds among others are important baseline variables for any continuing project activity in any place. Wind is created when air moves from areas of high pressure toward areas of low pressure. Factors that affect wind direction (Table 3) and wind speed (Table 4) are seasonal temperature changes, centripetal acceleration, air pressure and Earth's rotation (Barber, 2021). The climate of the Niger Delta is affected by ocean and atmospheric interactions both within and outside its environment, in which the Inter-Tropical Convergence Zone (ITCZ) plays a controlling factor. The movement of the ITCZ is associated with the warm humid maritime tropical air mass with its South-Western winds and the hot and dry continental air mass with its dry North-Eastern winds (Antai, et al., 2020; Tokuşlu et al., 2020; Edokpa and Nwagbara, 2017). The prevailing wind direction is the South-Western winds (Antai, et al., 2020; Edokpa and Nwagbara, 2017). This implies that the wind blew from the South towards the North, North-East and North-West directions of the study environment (Antai, et al., 2020). Furthermore, average wind speeds in Nigeria range from about 2 m/s to about 4 m/s with highest average speeds of about 3.5 m/s and 7.5 m/s in the South and North areas, respectively (Oyewole and Aro, 2018; Fagbenle and Karayiannis, 1994).



Fig. 1: Recent Nigeria's gas flaring scene in the Niger Delta; A) Onshore, Source: (Micheal, 2019); B) Offshore, Source: (Nwabughiogu, 2021).

The gaps before this study is that in the Niger Delta, limited research into investigating the effects of the prevailing wind on the Land Surface Temperature (LST) retrieved from Earth Observation Satellites (Landsat 5 TM and Landsat 7 ETM+) at the flaring sites has been published to date, and no research applied the methodology discussed in this paper. The basis for this research is the concept that combining remote sensing data with field survey data would result in significantly better analyses that give 2 dimensional spatio-temporal results. The 3 basic research questions for this study are: (1) What are different classes of LST retrieved from satellite data at the study sites in the Niger Delta? (2) Is there a detectable impact of wind direction on the spatial gradients in LST around the flares?

(3) What is the impact of the South prevailing wind on the LST retrieved at flaring sites in the Niger Delta? Based on these questions, the primary aim of this study is to examine the effects of the South prevailing wind on the LST retrieved from Landsat 5 TM and Landsat 7 ETM+ at the flaring sites in the Niger Delta. The specific objectives set for these research questions are: (1) Retrieval of LST from Landsat 5 TM and Landsat 7 ETM+ data at the flaring sites; (2) Parameterization of flare-related change in LST as  $\delta$ LST; (3) Integration of wind directions and wind speeds data into the LST retrieved at the flaring sites; (4) Statistical analysis for the effects of the South prevailing wind on the LST. In this paper, we present a spatial variation of LST at flare sites using ArcGIS for investigating the impacts of the South prevailing wind on the LST retrieved at flaring sites in the Niger Delta. Section 2 presents the study area and dataset used. Section 3 describes the developed methods; section 4 presents the results and finally, in section 5 we present summary and our conclusions.

### Study Area and Dataset Used *Study Area*

All 11 flaring sites studied for this research are located in Rivers State of the Niger Delta region. The selection of the sites were based on the availability of Landsat data in the United State Geological Survey (USGS)/National Aeronautic and Space Administration (NASA) archive; function of the facility e.g. refineries, liquefied natural gas (LNG) plant, flow stations, terminals and oil wells; spatial dimensions of the facility; accessibility and location i.e. both coastal and inland facilities. The geographical coordinates of the sites limit lies approximately within Latitude 4 ° 40 <sup>1</sup> and 5 ° 01 <sup>1</sup> N and Longitude 6  $^{\circ}$  50  $^{1}$  and 7  $^{\circ}$  01  $^{1}$  E (Morakinyo, 2015). The name, size of the facility, height of the flare stack and the geographical coordinate of the flare stack position within each site are presented in Table 1. The size of the area examined around the flare stacks with Landsat satellite data is  $12 \times 12$  km, in order to include sufficient data for detailed mapping of each site so that processes not related to flaring could also be resolved.

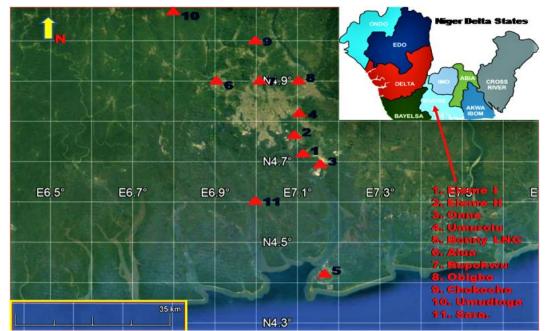


Fig. 2. Case study sites, Rivers States, Niger Delta Region of Nigeria; (Source: Google Earth, 2021; Nigerian Infopedia, 2021) Table 1: Name and size of the facility, their height of flare stack with their geographical coordinates.

S/N	Name of the facility	Size of the facility	Height of the flare stack (m)	Geographical coordinates of the flare stack position		
			Stuck (III)	Latitude ( $\theta$ )	Longitude ( $\lambda$ )	
1.	Eleme Refinery I Petroleum	1.6 × 1.1 km	50	4.729	7.119	
	Company			,		
2.	Eleme Refinery II Petroleum	$2.2 \times 1.3$ km	65	4.762	7.111	
	Company				,	
3.	Onne Flow Station	175 × 130 m	3.5	4.712	7.141	
4.	Umurolu Flow Station	$4.2 \times 2.4$ km	60	4.830	7.109	
5.	Bonny Liquefied Natural Gas	$4.2 \times 2.8$ km	25	4.425	7.153	
5.	(LNG) Plant	1.2 × 2.0 km	20	11125	1.155	
6.	Alua Flow Station	$170 \times 90 \text{ m}$	20	4.933	6.977	
7.	Rukpokwu Flow Station	$350 \times 350 \text{ m}$	25	4.930	7.016	
8.	Obigbo Flow Station	$650 \times 650 \text{ m}$	23	4.892	7.120	
9.	Chokocho Flow Station	$350 \times 050$ m	22	5.008	7.019	
9. 10.	Umudioga Flow Station	$100 \times 100 \text{ m}$	21 22	5.193	6.762	
	Sara Flow Station	$350 \times 250 \text{ m}$	22 22	4.657	7.060	
11. Tabla	2: List of Landsat 5 TM and Landsa			4.037	/.000	
	2: List of Landsat 5 TM and Landsa Scene Identity No.		acquisition UTC Tin	D-41-/	D	
S/N 1.	LT51880571986017AAA04	17-01-1		ne Path/ row 188/057	Processing level L1T	
1. 2.	LT51880571986065XXX01	06-03-1		188/057	L1T	
2. 3.	LT51880571986353XXX10	19-12-1		188/057	L1T	
4.	LT51880571987004XXX04	04-01-1		188/057	LIT	
5.	LT51880571987084XXX02	25-03-1		188/057	L1T	
6.	LT51880571990356XXX03	22-12-1	990 09:10	188/057	L1T	
7.	LT51880571991007XXX03	07-01-1		188/057	L1T	
8.	LE71880571999317EDC00	13-11-1		188/057	L1T	
9.	LE71880572000352EDC00	17-12-2		188/057	L1T	
10.	LE71880572004331ASN00	26-11-2		188/057	L1T	
11.	LE71880572005029ASN00	29-01-2		188/057	L1T	
12. 13.	LE71880572005365ASN00	31-12-2 18-12-2		188/057 188/057	L1T L1T	
15. 14.	LE71880572006352ASN00 LE71880572007003ASN00	03-01-2		188/057	LIT LIT	
14.	LE71880572007355ASN00	21-12-2		188/057	L1T L1T	
16.	LE71880572008006ASN00	06-01-2		188/057	L1T	
17.	LE71880572008326ASN00	21-11-2		188/057	LIT	
18.	LE71880572009344ASN00	10-12-2		188/057	L1T	
19.	LE71880572010043ASN00	12-02-2	010 09:37	188/057	L1T	
20.	LE71880572010347ASN00	13-12-2		188/057	L1T	
21.	LE71880572011334ASN00	30-11-2		188/057	L1T	
22.	LE71880572011350ASN00	16-12-2	011 09:39	188/057	L1T	
23.	LE71880572012017ASN00	17-01-2	012 09:39	188/057	L1T	
				100/057	I. 100	
24.	LE71880572013003ASN00	03-01-2	013 09:41	188/057	L1T	

Landsat 5 Thematic Mapper (TM) and 18 data of Landsat 7 Enhanced Thematic Mapper Plus (ETM+) dated 17/01/1986 to 08/03/2013 used were downloaded from the USGS Earth Resources Observation and Science (EROS) Data Centre website (http://earthexplorer.usgs.gov/) using the Glovis/Earth Explorer interface. The scenes with < 5 %contamination were selected for the research (Table 2); and all sites are located within a single Landsat scene (Path 188, Row 057). Landsat 5 TM images are acquired in 7 spectral bands while Landsat 7 ETM+ is acquired in 8 spectral bands; and both have similar spatial resolution of 30 m for bands 1-5 and 7. Band 8 for Landsat 7 ETM+ is panchromatic with a spatial resolution of 15 m. The spatial resolution for Landsat 5 TM band 6 (Thermal infrared) is 120 m while for Landsat 7 ETM+ is 60 m but both are resampled to 30 m pixels (Morakinyo, 2015; Chander and Markham, 2003). L1T is the processing level for all the imagery, which means systematic radiometric and geometric correction using ground control points (GCPs), and digital elevation model (DEM) has been applied. The problem of Scan Line

Correction (SLC-off mode) with Landsat 7 sensor that started in 2004 which lead to loss of part of data in the imagery (Chen et al., 2012) was reduced to a minimum by setting one of the criteria for the selection of flare sites as the availability of data covering each facility.

### Meteorological Data

Port Harcourt International Airport meteorological station which is about 50 km away from Eleme Refinery I Petroleum Company flaring site is the closest meteorological station available in Rivers State and its data is used in this research. The monthly wind directions and wind speeds data observed at 10 m height from 2000 to 2020 (21 years), collected from the Nigeria Meteorological Agency (NMA), Lagos, Nigeria were used in this study. South is the dominant wind origin directions, followed by the West direction with a few instances of South-West, North-West and North-East directions. Tables 3 and 4 shows the monthly wind directions and wind speeds measured at Port Harcourt International Airport meteorological station from 2000 to 2020.

	11	1			
Table 3: Wind	directions at Port	Harcourt In	ternational Airpor	rt, Rivers State	(2000-2020).

	wind unec	tions at 10			ulonal Al	<b>.</b> ·	CIS State	2000-20	120).				
Stn	Yr	J	F	М	A	М	J	J	A	S	0	N	D
PH	2000	S	S	S	S	S	S	SW	SW	SW	S	S	NW
PH	2001	NW	S	S	S	S	S	S	SW	W	S	S	NW
PH	2002	NW	S	S	S	S	S	S	SW	SW	S	S	SW
PH	2003	S	S	S	S	S	S	S	S	W	W	S	S
PH	2004	S	Ν	S	S	S	S	S	W	W	S	S	W
PH	2005	W	W	S	S	S	S	S	W	S	S	S	W
PH	2006	W	SW	S	S	S	S	S	S	SW	S	SW	W
PH	2007	W	W	W	W	W	W	W	W	W	W	W	NE
PH	2008	S	Ν	S	S	S	S	S	W	W	S	S	W
PH	2009	W	W	S	S	S	S	S	W	S	S	S	W
PH	2010	W	SW	S	S	S	S	S	S	SW	S	SW	W
PH	2011	W	S	S	W	S	S	S	W	W	S	S	W
PH	2012	S	S	S	S	S	S	S	S	W	S	W	S
PH	2013	S	S	S	S	S	S	S	S	W	S	S	W
PH	2014	S	S	S	W	S	S	SW	SW	SW	S	S	W
PH	2015	S	SW	S	S	S	S	S	S	W	S	S	S
PH	2016	W	S	S	S	S	S	S	S	W	W	S	S
PH	2017	W	S	S	S	S	S	S	S	S	S	W	W
PH	2018	S	S	S	S	W	S	S	SW	S	S	S	W
PH	2019	NW	S	S	S	S	S	S	W	S	S	S	SW
PH	2020	S	NW	S	S	S	S	W	S	SW	S	SW	S

Source: NMA, Lagos.

Table 4: Wind speed (m/s) at Port Harcourt International Airport, Rivers State (2000-2020).

Stn	Yr	J	F	М	А	М	J	J	A	S	0	Ν	D
PH	2000	3.6	4.4	3.3	3.5	3.4	3.9	3.3	4.5	3.3	2.9	3.5	2.5
PH	2001	4.1	4.5	4.3	3.6	3.7	2.9	2.2	3.3	2.3	1.0	1.7	2.2
PH	2002	4.1	3.8	3.9	4.0	3.3	3.0	3.2	3.5	2.5	1.7	1.7	2.6
PH	2003	2.8	2.6	3.1	2.7	2.8	3.5	3.9	2.7	3.0	2.0	2.0	2.4
PH	2004	3.0	3.3	3.2	2.9	3.9	4.5	4.7	2.9	3.2	2.6	2.5	2.4
PH	2005	3.8	4.4	5.5	4.6	4.1	4.3	4.7	5.5	4.5	3.8	2.8	3.3
PH	2006	3.3	4.1	4.2	4.3	4.8	4.7	5.4	5.6	4.7	2.5	1.9	2.2
PH	2007	2.4	3.9	4.1	4.6	4.1	4.7	4.5	4.7	3.7	3.3	2.7	2.8
PH	2008	3.3	3.8	3.2	2.4	2.3	2.2	2.2	2.4	1.9	2.1	1.6	1.5
PH	2009	5.3	2.3	2.3	2.6	2.3	2.6	3.5	2.1	2.3	2.8	2.2	1.8
PH	2010	3.2	3.5	3.5	2.9	3.7	4.2	4.5	3.1	2.3	4.5	4.0	3.3
PH	2011	3.1	3.4	3.3	3.0	4.0	4.6	4.7	3.0	3.3	2.7	2.6	2.5
PH	2012	3.4	3.9	3.3	2.5	2.4	2.3	2.3	2.5	2.0	2.2	1.7	1.6
PH	2013	3.2	4.0	4.1	4.2	4.7	4.6	5.3	5.5	4.6	2.4	1.8	2.1
PH	2014	4.0	4.4	4.2	3.5	3.6	2.8	2.1	3.2	2.2	1.0	1.6	2.2
PH	2015	3.2	3.4	3.5	3.0	3.6	4.1	4.4	3.1	2.4	4.4	3.9	3.3
PH	2016	3.5	4.4	3.4	3.6	3.4	3.8	3.4	4.3	3.4	2.8	3.4	2.5
PH	2017	2.9	2.7	3.2	2.8	2.9	3.4	3.8	2.8	3.1	2.2	2.2	2.5
PH	2018	2.5	3.8	4.0	4.5	4.0	4.5	4.4	4.5	3.7	3.3	2.8	2.9
PH	2019	5.2	2.4	2.5	2.6	2.4	2.6	3.4	2.2	2.4	2.9	2.3	2.1
PH	2020	4.2	3.9	4.0	4.1	3.5	3.1	3.3	3.6	2.7	1.9	1.9	2.8

Source: NMA, Lagos.

### Methods

Processing Steps for Landsat 5 TM and Landsat 7 ETM+Data

The methods adopted are:

(1). Verification of geo-location points using Google Earth. 5 ground control points each were selected over all the 11 sites and measured with GPS on site during ground validation exercise. 14 imagery (7 each from Landsat 5 TM and Landsat 7 ETM+) were uploaded into ArcGIS and the selected ground control points (GCPs) were identified.

(2) MATLAB code was used for data processing and for removal of zero or out of range values from the data and their replacement with not a number (nan) to avoid divide by zero errors in calculations.

(3) Radiometric calibration of the thermal band (6) of the data by converting the Digital Number (DN) values recorded into top of atmosphere (TOA) radiance or temperature values based on sensor calibration parameters provided within the metadata files from USGS (Chander and Markham, 2003; NASA, 2002) using equation 1

 $L_{\lambda} = ((LMAX_{\lambda} - LMIN_{\lambda})/(QCALMAX - QCALMIN)) \times (QCAL-QCALMIN) + LMIN_{\lambda} \quad (Eq.1)$ 

Where:

 $L_{\lambda}$ = Spectral Radiance at the sensor's aperture (Wm<sup>-2</sup>sr<sup>-1</sup> $\mu$ m<sup>-1</sup>);

QCAL = The quantized calibrated pixel value in DN;

LMIN<sub> $\lambda$ </sub>= The spectral radiance that is scaled to QCALMIN (Wm<sup>-2</sup>sr<sup>-1</sup> $\mu$ m<sup>-1</sup>);

LMAX<sub> $\lambda$ </sub> = The spectral radiance that is scaled to QCALMAX (Wm<sup>-2</sup>sr<sup>-1</sup> $\mu$ m<sup>-1</sup>);

QCALMIN = The minimum quantized calibrated pixel value (corresponding to LMIN<sub> $\lambda$ </sub>) in DN = 1 for LPGS (a processing software version) products;

QCALMAX = The maximum quantized calibrated pixel value (corresponding to LMAX<sub> $\lambda$ </sub>) in DN = 255.

(4) Removing atmospheric effects from multispectral bands (1-4) and thermal band (6). The atmospheric correction parameters (upwelling radiance (L<sub>u</sub>), downwelling radiance (L<sub>d</sub>), and transmittance ( $\tau$ )) obtained from Atmospheric Correction Parameters (ATMCORR) Calculator, a National Aeronautics and Space Administration (NASA) web tool developed by Barsi et al. (2005), were applied to thermal band 6 to obtain atmospherically corrected data. Dark Object Subtraction (DOS) method (Kaufman et al., 2000) was employed for removing atmospheric effects from the multispectral bands (1-4).

# Land Use Land Cover (LULC) Classification and Estimation of Emissivity ( $\epsilon$ ) Values

4 land cover (LC) types (vegetation, soil, built up and water) (Maaharjan, 2018) with their % identified at study sites during ground validation from 04/08/2012-21/09/2012 and 05/08/2020- 21/09/2020 was derived when MATLAB code and cluster analysis method (Şatır and Berberoğlu, 2012) were applied to the

atmospherically corrected reflectance (bands 1-4) produced by Landsat 5 TM and Landsat 7 ETM+ (Alvarez, 2009). The 4 LC types was clarified using images held within Google Earth and Digital Global (http://browse.digitalglobe.com/imagefinder/public.do) such as WorldView-1 and 2, IKONOS pseudo-true colour images, Landsat imagery (bands 1-4 and 6), and Red, Green, Blue (RGB) pseudo-true colour composite images.

The method adopted to estimate emissivity  $(\varepsilon)$  value for LC types at the sites is based on the  $\varepsilon$  value of 4 LC types present at each site. Each pixel LC types were considered for the entire site and their  $\varepsilon$  values (both minimum (min) and maximum (max)) were taken from the literature. Mean of  $\varepsilon$  values for LC types for each single pixel obtained from using their (min) and (max) values from the literature were calculated. Average of both (min) and (max)  $\varepsilon$  values results were obtained for each pixel and the same procedure was repeated for all pixels in the selected  $12 \times 12$  km area (Morakinyo, et al., 2019). Therefore, the  $\varepsilon$  value for each Landsat pixel's LC is a combination of the  $\varepsilon$  value of background features present within the pixel. The authors adopted an independent method of using LC types at each site for the correction of  $\boldsymbol{\epsilon}$  value rather than Global Land Cover (GLC) data from USGS in order to ensure quality control primarily.

# Retrieval of LST from atmospherically corrected Landsat 5 TM and Landsat 7 ETM+ datasets.

The theoretical basis for the LST measurement is Plank's radiation function, formulated as:

$$B(\lambda, T) = \frac{C_1 \lambda^{-5}}{\pi (\exp (C_2 / \lambda T) - 1)}$$
(Eq. 2)

Where:

B(λ, T) = Spectral radiance of a blackbody (Wm<sup>-2</sup>sr <sup>-1</sup>μm<sup>-2</sup>);  $\lambda$  = Wavelength (m);

T = Temperature (K); C<sub>1</sub> = The first spectral constant =  $3.741775 \times 10^{-22}$  Wm<sup>2</sup>;

 $C_2$  = The second spectral constant 1.4388 × 10<sup>-2</sup> mK; PI ( $\pi$ ) = constant = 3.142 (Qin et al., 2011).

When  $B(\lambda,T)$  is measured generally by a thermal sensor, the surface-leaving radiance  $(L_{\lambda})$  can be computed by inverting the Planck's radiance function as follows (Figure 3):

$$L_{\lambda} = \frac{C_2}{\lambda \ln[(C_1/\lambda^5 B(\lambda, T)) + 1]}$$
 (Eq. 3)

The approach for the calculation of LST, by first calculating  $L_{\lambda}$  and substituting it into the Planck function and inverting the function to get the LST was adopted for the study (Figure 3) (Morakinyo, 2020a; Coll et al., 2010). The formula for computing  $L_{\lambda}$  is:

$$\begin{split} L_{\lambda} &= ((L_s - L_u)/\epsilon\tau) - ((1-\epsilon)/\epsilon) \times L_d \ (Wm^{\text{-}2} sr^{\text{-}1} \mu m^{\text{-}1}) \\ (Eq. \ 4) \end{split}$$

The  $L_u$ ,  $L_d$ , and  $\tau$  were applied to the calibrated at-sensor radiance band 6 (High gain) data to compute the  $L_{\lambda}$ .

LST was derived using equation 5.

 $L_s$  = Radiometrically corrected Landsat thermal band 6 radiance (High gain);

 $L_u$  = Upwelling radiance;  $L_d$  = Downwelling radiance;

 $\tau$  = Atmospheric transmission;  $\epsilon$  = emissivity.

 $L_u,\,L_d,\,and\,\tau$  are atmospheric correction parameters for the Landsat thermal band.

$$LST = \frac{K_2}{\ln((K_1/L_\lambda) + 1)}$$
(Eq.5)

Where,  $K_1$  and  $K_2$  are thermal band calibration constants calculated for the Landsat sensor characteristics.

For Landsat 5 TM,  $K_1 = 607.76 \text{ (Wm}^{-2}\text{sr}^{-1}\mu\text{m}^{-1})$  and  $K_2 = 1260.56 \text{ (K)}$ ; and

For Landsat 7 ETM+,  $K_1 = 666.09$  (W m<sup>-2</sup> sr<sup>-1</sup> $\mu$ m<sup>-1</sup>) and  $K_2 = 1282.71$  (K).

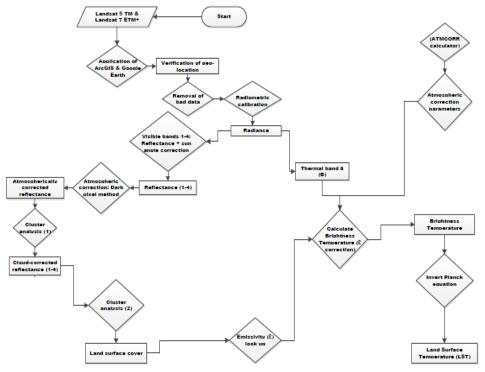


Fig. 3: Flowchart presentation of the methods employed for the processing of Landsat 5 TM and Landsat 7 ETM+ data for LULC classification, estimation of emissivity and LST retrieval.

### Linear regression analysis of $\delta LST_{N, S, E, W}$

Linear regression helps to model the relationship between two variables by fitting a linear equation to observed data. Linear regression analysis is the most widely used of all statistical techniques: it is the study of linear, additive relationships between variables (Eze et al., 2005). One variable is considered to be an independent variable, and the other is considered to be a dependent variable. A scatter plot (Figure 8) is a helpful tool in determining the strength of the relationship between two variables. If there appears to be no relationship between the proposed independent and dependent variables (i.e., the scatter plot does not indicate any increasing or decreasing trends), then fitting a linear regression model to the data probably will not provide a useful model. A valuable numerical measure of relationship between two variables is the correlation coefficient, which is a value between -1 and 1 indicating the strength of the relationship of the observed data for the two variables. A linear regression line has an equation of the form Y = a + bX, where X =Independent variable and Y = Dependent variable, b =Slope of the line and a = Intercept (the value of Y when X = 0) (Eze et al., 2005).

A new parameter  $\delta LST$  was defined to facilitate quantitative verification of the heat sources at the flare locations.  $\delta LST$  is the difference between the LST at the flare stack and the LST at 450 m (maximum distance) from the flare stack. Figure 4 shows the schematic diagram for the definition of  $\delta LST$ .

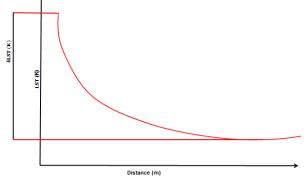


Fig. 4: Change in LST with distance, and the definition of  $\delta$ LST

Both linear and non-linear relationships were tested, but non-linear give no better results. Hence, linear regression analysis was used to compare  $\delta LST$  in different directions at the flaring sites. Specifically, it was assumed that a consistent relationship should exist between  $\delta$ LST in pairs of directions at any site where a strong prevailing wind does not influence the impact of the flare on LST values near the flare; i.e. heat from the flare radiates equally in all directions and the resulting heated air mass does not flow in a dominant direction. Pairwise linear regression analysis was applied to the

 $\delta$ LST values in each direction, site by site. The significance level was set a priori to  $\alpha = 0.01$ .

In addition, in order to summarize the spatial geographical shape of  $\delta$ LST around the study sites, figures were created based on facilities with statistically significant p-value from any of the three relationships ( $\delta$ LST<sub>NE</sub>,  $\delta$ LST<sub>NS</sub>, and  $\delta$ LST<sub>NW</sub>). 3 different cases are presented (Figure 9).

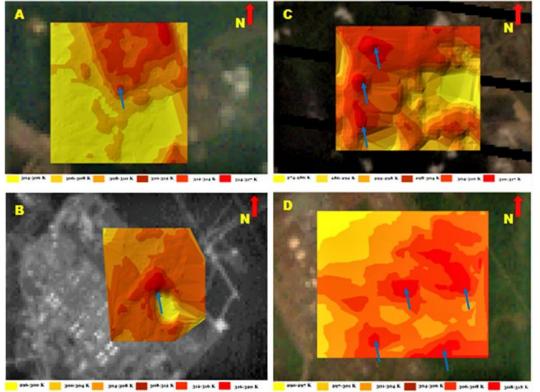


Fig. 5: A) Eleme Refinery I; B) Eleme Refinery II; C) Onne Flow Station; D) Umurolu Flow Station.

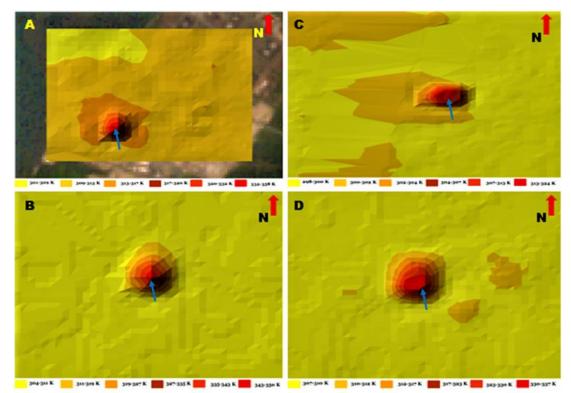


Fig. 6: A) Bonny LNG; B) Alua Flow Station; C) Rukpokwu Flow Station; D) Obigbo Flow Station.

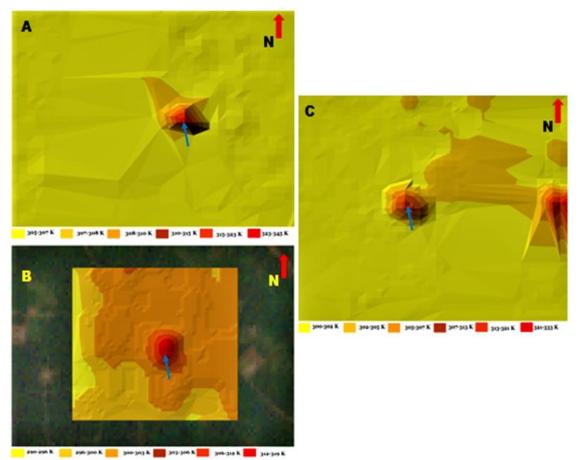


Fig. 7: A) Chokocho Flow Station; B) Umudioga Flow Station; C) Sara Flow Station.

### **Results and Discussion**

# Retrieval of LST from atmospherically corrected Landsat 5 TM and Landsat 7 ETM+ datasets.

For the Figures 5-7, the pseudo-true colour images from the combination of Landsat bands 3, 2 and 1 as Red, Green and Blue (RGB) were used as the background map for the sites instead of the Google Earth images in order to avoid geo-referencing errors that are associated with Google Earth images. The Red arrow and letter N at the upper corner of the right side shows the direction of the North, the Blue arrow show the flare flack and Kelvin (K) in the legend is the International System Unit for temperature. Figures 5-7 show the 2D ArcGIS plots of each facility with LST overlaid and classified in 6 different range group layers with a colour to represent each group. Pure red colour is for highest range of values, followed by light red, light brown, deep orange, light orange and yellow colours respectively. This is to help in determining the best direction of the minimum and maximum LST slope for each site. Generally, for all sites, the spatial analysis of LST with ArcGIS shows that the flare sources give the highest LST, followed by the next adjoining pixels surrounding the flare and continue in that order.

For Eleme I and II refineries (Figures 5A and 5B), Onne and Umurolu Flow Stations (Figures 5C and 5D), their data acquisition dates, wind directions and wind speeds are 17/12/2000, North-West, 2.5 m/s; 29/01/2005, South,

3.8 m/s; 08/03/2013, South, 4.1 m/s; and 12/02/2010, South, 3.5 m/s respectively. Similarly, for Bonny LNG (Figure 6A), Alua, Rukpokwu and Obigbo Flow Stations (Figures 6B-6D), their acquisition dates, wind directions and wind speeds are 06/01/2008, South, 3.3 m/s; 16/12/2011, South, 3.6 m/s; 10/12/2009, West, 1.8 m/s; and 12/02/2010, South, 3.5 m/s respectively. Also, the acquired dates, wind directions and wind speeds for Chokocho, Umudioga and Sara Flow Stations (Figures (7A-7C) are 03/01/2013, North-East, 3.2 m/s; 26/11/2004, South, 2.5 m/s; and 21/12/2007, West, 2.8 m/s respectively.

Generally, it is observed that the size and shape of the plume, and LST differ from one oil facility to another. Therefore, the result suggests that the LST retrieved is dependent on the size of the facility, volume and rate of the burning gas at the time of satellite overpass.

### Linear regression analysis of $\delta LST_{N, S, E, W}$

All relationships with significant impact for each site are shown in bold in Table 5. Figure 8 summarize these results.

 $\delta LST_{NE}$  = relationship between  $\delta LST_N$  and  $\delta LST_E$ ;  $\delta LST_{NS}$  = relationship between  $\delta LST_N$  and  $\delta LST_S$ ;  $\delta LST_{NW}$  = relationship between  $\delta LST_N$  and  $\delta LST_W$ . Table 5 show a -correlation for  $\delta LST_N$  compared to  $\delta LST_E$ , and a +correlation for both the  $\delta LST_{NS}$  and  $\delta LST_{NW}$  directions for Eleme Refinery I. Both Eleme II and Onne were characterized by +correlations for both the  $\delta LST_{NE}$  and  $\delta LST_{NS}$  directions, and a –correlation for the  $\delta LST_{NW}$  direction. However, the p-values for both Eleme I and II, and Onne showed that no statistically significant relationships between  $\delta LST$ values in different directions existed. Umurolu, Bonny LNG, Alua, Rukpokwu, Chokocho and Sara were characterized by correlations amongst the 4 directions and their p-values showed that these were statistically significant. Obigbo and Umudioga had +correlations with 3 of the relationships; Obigbo had significant pvalues for both  $\delta LST_{NE}$  and  $\delta LST_{NW}$  while Umudioga had significant p-values for  $\delta LST_{NW}$  only.

Table 6 presents another set of correlation coefficients (r<sup>2</sup>-value and p-value) for the 11 facilities with a condition that any  $\delta$ LST with a p-value (computed from ANOVA) greater than  $\alpha = 0.01$  should not be used. The results in Table 6 suggests that the influence of South wind demonstrated in Table 5 is the same as recorded in Table 6 despite a further statistical condition imposed on the Table 5 results.

Table 5: Computed values of,  $r^2$  and p-value with  $\alpha = 0.01$  from  $\delta$ LST<sub>N</sub>,  $\delta$ LST<sub>S</sub>,  $\delta$ LST<sub>E</sub>,  $\delta$ LST<sub>W</sub> for each facility (using linear regression analysis and p-value)

S/N	Facility		$\delta LST_{NE}$		$\delta LST_{NS}$	$\delta LST_{NW}$		
		$r^2$	p-value	$r^2$	p-value	$r^2$	p-value	
1.	Eleme I	-0.0001	0.965	0.017	0.594	0.023	0.539	
2.	Eleme II	0.0024	0.811	0.019	0.499	$-3.611 \times 10^{-4}$	0.937	
3.	Onne	0.074	0.080	0.046	0.172	$-6.241 \times 10^{-3}$	0.619	
4.	Umurolu	0.538	$7.000 imes10^{-8}$	0.206	0.003	0.642	$5.470  imes 10^{-10}$	
5.	Bonny	0.501	<b>4.140</b> × 10 <sup>-6</sup>	0.377	$1.465 \times 10^{-4}$	0.584	$2.227 \times 10^{-7}$	
6.	Alua	0.898	$6.774  imes 10^{-15}$	0.753	$1.123  imes 10^{-9}$	0.662	$8.035  imes 10^{-8}$	
7.	Rukpokwu	0.527	$1.138  imes 10^{-7}$	0.753	$1.123  imes 10^{-5}$	0.266	$6.657  imes 10^{-4}$	
8.	Obigbo	0.778	$5.700  imes 10^{-10}$	0.200	0.017	0.272	0.004	
9.	Chokocho	0.540	$5.587  imes 10^{-6}$	0.221	0.010	0.805	$4.444  imes 10^{-11}$	
10.	Umudioga	0.261	0.015	0.125	0.106	0.343	0.004	
11.	Sara	0.707	$1.121  imes 10^{-11}$	0.196	0.004	0.461	$1.448  imes 10^{-6}$	

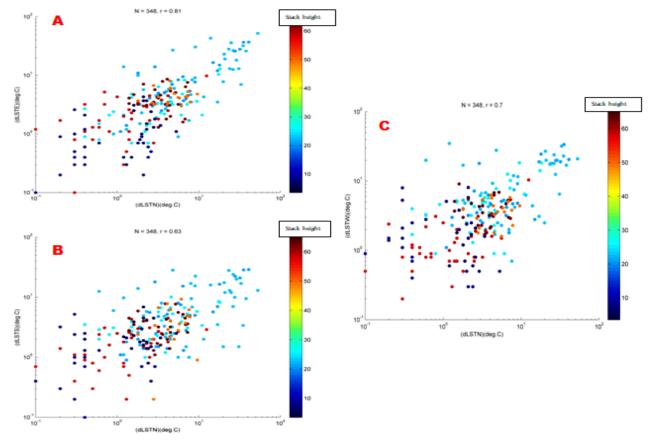


Fig. 8: A)  $\delta$ LST<sub>N</sub> against  $\delta$ LST<sub>E</sub>; B)  $\delta$ LST<sub>N</sub> against  $\delta$ LST<sub>S</sub>; C)  $\delta$ LST<sub>N</sub> against  $\delta$ LST<sub>W</sub>

S/N	Facility		$\delta \mathrm{LST}_{\mathrm{NE}}$		$\delta LST_{NS}$		$\delta LST_{NW}$
		$r^2$	p-value	$r^2$	p-value	$\mathbf{r}^2$	p-value
1.	Eleme I	0.104	0.682	0.020	0.945	-0.010	0.972
2.	Eleme II	0.043	0.860	0.268	0.298	0.119	0.649
3.	Onne	0.291	0.158	0.099	0.618	-0.022	0.920
4.	Umurolu	0.804	8.789 ×10 <sup>-8</sup>	0.474	0.010	0.811	2.976 ×10 <sup>-7</sup>
5.	Bonny	0.760	1.584 ×10 <sup>-4</sup>	0.635	0.003	0.796	2.725 ×10 <sup>-5</sup>
6.	Alua	0.962	5.620 ×10 <sup>-11</sup>	0.908	8.008 ×10 <sup>-8</sup>	0.814	7.048 ×10 <sup>-6</sup>
7.	Rukpokwu	0.809	1.817 ×10 <sup>-7</sup>	0.605	3.142 ×10 <sup>-4</sup>	0.461	0.002
8.	Obigbo	0.886	9.233 ×10 <sup>-8</sup>	0.474	0.035	0.423	0.007
9.	Chokocho	0.794	1.019 ×10 <sup>-5</sup>	0.380	0.008	0.934	$2.600 \times 10^{-11}$
10.	Umudioga	0.333	0.290	0.488	0.055	0.662	0.010
11.	Sara	0.910	$1.123 \times 10^{-10}$	0.368	0.004	0.746	2.885 ×10 <sup>-5</sup>
			•		٨		

Table 6: Computed values of  $r^2$  and p-value for  $\alpha = 0.01$  from  $\delta LST_N$ ,  $\delta LST_E$ ,  $\delta LST_S$ ,  $\delta LST_W$  and each facility (using linear regression analysis, p-value computed from ANOVA)

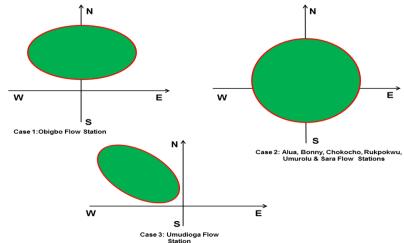


Fig. 9: Geographical symmetry of LST in relation to the flare

Furthermore, Figure 9 is the graphical representation of Table 6 in which 3 different cases are presented to summarize the spatial geographical shape of  $\delta$ LST around the study sites. The figure for each case was created based on the facilities with statistically significant p-value from any of the 3 relationships ( $\delta$ LST<sub>NE</sub>,  $\delta$ LST<sub>NS</sub>, and  $\delta$ LST<sub>NW</sub>). For case 1, Obigbo Flow Station only, the p-value for the pairwise linear regression of  $\delta LST_N$  against  $\delta LST_E$ , and  $\delta LST_N$  against  $\delta LST_W$  are statistically significant. This shows that the wind direction (South) for data acquisition date used to plot Obigbo site, combined with the South prevailing wind to generate a noticeable impact on the LST towards the North-East and the North-West directions. Case 2 is for Alua, Bonny, Chokocho, Rukpokwu, Umurolu and Sara Flow Stations where there is no evidence of the influence of their respective wind directions for data acquisition dates, and that of the South prevailing wind on the flare because  $\delta LST$  is directionally uniform; therefore, the flare  $\delta LST$  footprint is a circle. The pvalue obtained is statistically significant for all the 3 ( $\delta$ LST<sub>NE</sub>,  $\delta$ LST<sub>NS</sub> and  $\delta$ LST<sub>NW</sub>) relationships. For case 3, which is for Umudioga site, only  $\delta LST_N$  versus  $\delta LST_W$  is statistically significant. The influence of the combination of the wind direction (South) for data acquisition date used for plotting of Umudioga site and that of the South prevailing wind on the flare was strong; while from the West it was mild causing a noticeable effect on the LST to be felt in the North-West direction.

#### **Summary and Conclusions**

The satellite data made available for the research work spanned a length of 27 years and that of meteorological data is 21 years, making an appreciably conclusive results to be safely drawn. Wind directions and wind speeds for data acquisitions dates were applied to the South prevailing for the 11 sites. The results show that for Eleme I and II, and Onne the p-values results showed that no statistically significant relationships between  $\delta$ LST values in different directions existed. For Obigbo site, the wind direction (South) for data acquisition date combined with the South prevailing wind to generate a noticeable impact on the LST towards the North-East and the North-West directions. For Alua, Bonny, Chokocho, Rukpokwu, Umurolu and Sara sites, the pvalue obtained is statistically significant for all the 3  $(\delta LST_{NE}, \delta LST_{NS} \text{ and } \delta LST_{NW})$  relationships; therefore, producing a circle flare  $\delta$ LST footprint. For Umudioga site, only  $\delta LST_N$  versus  $\delta LST_W$  is statistically significant, causing a noticeable effect on the flare  $\delta$ LST in the North-West direction. The research showed that wind directions and wind speeds contribute to the spatiotemporal variation of the LST at the flaring sites in the Niger Delta. Based on these results, it can be concluded

that the volume and rate of burning gas, and the speed of the South wind at the time of satellite overpass are major factors that determine the influence of the South prevailing wind on the LST retrieved at the flaring sites in the Niger Delta.

As seen, there are limitations encountered in this study for example, the available Landsat data covers only dry season in Nigeria, hence a further research is required to investigate and compare for the wet season data too. In addition, the meteorological data gathered was collated on a monthly basis, thereby making diurnal wind pattern difficult; this calls for further studies because the nonanalysis of the diurnal wind patterns could lead to underestimation of the impacts of the wind on the LST retrieved at the study sites. The following recommendations are made: Curbing gas flaring in Nigeria is a veritable factor for enforcing standard of living and sustainable development. The problem of gathering gas to a central location can be solved by building mini and micro gas power plants in remote areas where the gas flaring occurs. Also, adequate geographical coverage of natural gas pipeline distribution network as it is done for oil products can help curb flaring. Strict adherence to the suggested applications of flared gas would serve as the way forward for Nigeria in conservation of gas and her ecosystem. Contradictorily, companies undertaking oil activities in Nigeria are the same ones handling similar activities in Europe and America, where flaring have been reduced to a minimal level. Therefore, the technologies to re-inject and add value to the associated gas are known all over the world; Nigeria's case should not be treated otherwise.

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