



Optimization of extraction parameters of cationic dye using emulsified liquid membrane process. Application of Box-Behnken design

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ABSTRACT

Cationic dye (Methylene blue) was extracted from wastewater by using emulsified liquid membrane process. The membrane is composed of two phases: organic and aqueous. D2EHPA, SPAN 80, and acid are the composition of the aqueous phase, however, the fuel oil represents the organic phase. The effect of different parameters such as the initial concentration of cationic dye (MB), the addition of salt (KCl/ NaCl/ Na₂SO₄), acid (HCl/ H₂SO₄/H₃PO₄) and the extractant concentration (10, 30 and 50 ppm) was examined using Box-Behnken design. The optimization of the extraction has been shown that the extraction efficiency reach 100% for the following optimum operating conditions: 30 ppm for the initial concentration of [BM]₀, 10% w for the extracting (D2EHPA) with the presence of Na₂SO₄ and H₂SO₄. It can be said that the ELM method is efficient for the removal of methylene blue.

Keywords: Emulsified liquid membrane, extraction, methylene blue, modelling, optimization.

1. INTRODUCTION

Basic dye family represent the most important class of commercial dyes and are mainly used in textile, leather, paper, plastics, etc.¹⁻³ Among these dyes, methylene blue (MB) is a harmful pollutant and has been long been known for its detrimental effects on human health and the presence of low concentration improves water pollution.

Emülsifiye sıvı membran prosesi kullanılarak katyonik boyanın ekstraksiyon parametrelerinin optimizasyonu. Box-Behnken tasarımının uygulanması

ÖZ

Emülsifiye sıvı membran prosesi kullanılarak atık sudan Katyonik boya (Metilen mavisi) ekstrakte edilmiştir. Membran organik ve sulu olmak üzere iki fazdan oluşmaktadır. Sulu fazın bileşiminde D2EHPA, SPAN 80 ve asit bulunur, ancak fuel oil organik fazı temsil eder. Katyonik boyanın başlangıç konsantrasyonu (MB), tuz ilavesi (KCl/ NaCl/ Na₂SO₄), asit (HCl/ H₂SO₄/H₃PO₄) ve ekstraktan konsantrasyonu (10, 30 ve 50 ppm) gibi farklı parametrelerin etkisi Box-Behnken tasarımı kullanılarak incelenmiştir. Ekstraksiyonun optimizasyonu aşağıdaki optimum çalışma koşulları için ekstraksiyon verimliliğinin %100'e ulaştığını göstermiştir: 30 ppm [BM]₀ başlangıç konsantrasyonu, Na₂SO₄ ve H₂SO₄ varlığında yapılan ekstraksiyonun %10'u (D2EHPA). Metilen mavisinin giderilmesinde ELM yönteminin etkili olduğu söylenebilir.

Anahtar Kelimeler: Emülsifiye sıvı membran, ekstraksiyon, metilen blue, modelleme, optimizasyon.

The treatment and elimination of dyes from contaminated waters have been the subject of great attention in the last few years.⁴ There are several methods for dyes removal such as adsorption,^{5,6} extraction,⁷ biological treatment, coagulation/flocculation, chemical oxidation and photocatalytic process etc.⁸ Emulsion liquid membrane (ELM) has achieved a lot of attention seen in their advantages.⁹

The main objective of this work was to model and optimize the influence of various factors affecting the emulsion liquid membrane formation and its stability for removing MB. To achieve total elimination of dye, four factors such as the initial concentration of cationic dye (MB), the addition of salt (KCl/ NaCl/ Na₂SO₄), acid (HCl/ H₂SO₄/H₃PO₄) and the extractant concentration (10, 30 and 50 ppm) were followed applying a Box-Behnken design

The four parameters take each three levels according to the Box-Behnken design. The experiment matrix consists of 27 experiments. The Box-Behnken design makes it possible to minimize the number of experiences,¹⁰⁻¹³ save time, money.

2. MATERIALS AND METHODS

2.1. Materials and compounds

Methylene bleu (MB) (C₁₆H₁₈N₃ClS) is a cationic dye supplied by Sigma Aldrich. The emulsified liquid membrane used for the extraction of MB consisted of monooleate of sorbitan (SPAN 80), an anionic commercial surfactant, di-2-ethylhexylphosphoric acid (D2EHPA) as the extractant, the fuel oil as the thinner. Sulfuric acid (95-97%, Fluka), phosphoric acid H₃PO₄ (85%, Merck), and hydrochloric acid HCl (37.25%, Merck) are the internal phase tested. The fuel oil used in this study is a fraction of Algerian petroleum. Demineralized water (pH=5.0–6.5) was used to prepare the external aqueous phase.

The addition of salt in the external aqueous phase was carried out. The salts used are sodium sulfate (Na₂SO₄) (99%, Merck), KCl (99%, Sigma-Aldrich), NaCl (99%, Sigma-Aldrich).

The homogenizer Moulinex active flow technology, with a capacity of 700 Whats was used to generate a stable emulsion for the extraction. Then, to ensure the dispersion of the emulsified membrane into a beaker containing the external aqueous phase, a mechanical stirrer type RW20 Kjank & Kunkel was used.

2.2. Methods

The ELM method consists to contact the aqueous phase containing the pollutant with an emulsion (W/O) which was formed of an organic phase (membrane) and an internal aqueous solution. Before extraction, a preliminary study of the ELM was essential to deduce the favorable conditions for the emulsion stability. The different parameters affecting the stability of membrane are the concentration of extractant, the concentration of internal phase, the time of emulsification, stirring speed,

the ratio $V_{\text{internal}} / V_{\text{external}}$ and $V_{\text{external}}/V_{\text{emulsion}}$. The stability of the membrane has been verified in an interior study.¹⁴ They found that the membrane is very stable. And the most favorable conditions for the stability of emulsified liquid membranes are: stirring speed = 200 rpm, SPAN 80 = 6%w, D2EHPA= 8 %w ; time of emulsification = 3 mn, ratio $V_{\text{Org}}/V_{\text{int}} = 1$, ratio $V_{\text{internal}} / V_{\text{external}} = 5$ and $[H_2SO_4]_{\text{internal}} = 1M$.

The emulsion (W/O) was prepared by mixing two phases organic and aqueous with the homogenizer for three minutes (a time that is already optimized). The organic phase (membrane) consisted of SPAN 80, D2EHPA, and fuel oil. However, the aqueous phase was the acid. The emulsions are prepared according to the matrix given by the MINITAB 18.

The samples were analyzed using a visible spectrophotometer (PRIM-SECOMAM) (at 664nm) to determine the concentration of the residual MB. The extraction efficiency was calculated by equation (1).

$$R\% = \left[1 - \frac{[MB]_f}{[MB]_0}\right] \times 100 \quad (1)$$

Where:

R : extraction yield (%).

[MB]_f: final concentration of MB in the external phase (ppm).

[MB]₀: initial concentration of MB in the external phase (ppm).

3. RESULTS AND DISCUSSION

3.1. Box-Behnken design

The industrial effluents are released into the aquatic environment loaded with various types of salts. In order to study the effect of the presence of salts in the solution, we have chosen three salts KCl, NaCl and Na₂SO₄ for levels (-1), (0) and (+1) respectively. The other factors studied are the weight percentage of D2EHPA (from 5 to 10% w), the initial concentration of MB dye (10 to 50ppm) and the type of acid in the internal phase (HCl (-1), H₂SO₄ (0) and H₃PO₄ (+1)). For this, an experimental design of second degree was envisaged (Table 1).

3.2. Anova

The ANOVA statistical analysis of experimental results are grouped in Table 2.

From the results of Table 2 it can be seen that the (internal phase) is a highly significant term on MB extraction with a p-value equal to zero. The linear effect and the square effect of the salt are significant terms where the value of the p-value is less than or equal to 0.05 (5%) with the values of p-value respectively equal to 0.05 and 0.03. We also observe that no interaction is significant.

Table.1: Experimental yields of MB extraction according to Box-Behnken design.

Essay	[BM] ₀	Effect of salts	Internal phase	[D2EHPA]	R exp. %	R theo. %
1	30	KCl	H ₂ SO ₄	5	98.98	99.79
2	50	NaCl	HCl	7.5	76.24	79.08
3	10	KCl	H ₂ SO ₄	7.5	99.56	92.43
4	30	KCl	HCl	7.5	76.25	79.61
5	50	NaCl	H ₃ PO ₄	7.5	82.32	77.59
6	30	NaCl	HCl	5	82.66	78.27
7	10	NaCl	HCl	7.5	61.34	70.16
8	30	NaCl	HCl	10	82.50	77.29
9	50	NaCl	H ₂ SO ₄	5	99.07	98.34
10	30	Na ₂ SO ₄	HCl	7.5	92.48	87.05
11	50	KCl	H ₂ SO ₄	7.5	96.75	94.86
12	50	Na ₂ SO ₄	H ₂ SO ₄	7.5	99.81	102.00
13	30	NaCl	H ₂ SO ₄	7.5	96.26	93.54
14	10	Na ₂ SO ₄	H ₂ SO ₄	7.5	100.00	98.56
15	10	NaCl	H ₂ SO ₄	10	91.25	92.11
16	30	KCl	H ₂ SO ₄	10	94.55	93.81
17	30	Na ₂ SO ₄	H ₂ SO ₄	5	98.90	103.00
18	50	NaCl	H ₂ SO ₄	10	86.43	88.07
19	30	Na ₂ SO ₄	H ₃ PO ₄	7.5	93.99	90.75
20	30	KCl	H ₃ PO ₄	7.5	78.67	84.24
21	30	NaCl	H ₃ PO ₄	5	83.43	84.40
22	30	NaCl	H ₂ SO ₄	7.5	94.08	93.54
23	10	NaCl	H ₂ SO ₄	5	89.29	87.77
24	30	NaCl	H ₃ PO ₄	10	79.30	79.46
25	30	Na ₂ SO ₄	H ₂ SO ₄	10	100.00	103.00
26	10	NaCl	H ₃ PO ₄	7.5	78.71	79.97
27	30	NaCl	H ₂ SO ₄	7.5	90.28	93.54

Table.2 : Estimated coefficients for the yield of MB extraction for coded units.

Terms	Coef	SE Coef	T	P
Constant	93.54	3.19	29.29	0.000
[BM] ₀	1.64	1.60	1.02	0.33
Salts	3.49	1.60	2.18	0.05
internal Phase (Acids)	2.08	1.60	1.30	0.22
D2EHPA	-1.48	1.60	-0.93	0.37
[BM] ₀ ²	-2.56	2.40	-1.07	0.31
(Salts) ²	6.15	2.40	2.57	0.03
(internal phase) ²	-14.28	2.40	-5.96	0.000
(D2EHPA) ²	0.59	2.40	0.25	0.81
[BM] ₀ × salts	0.42	2.77	0.15	0.88
[BM] ₀ × internal phase	-2.82	2.77	-1.02	0.33
[BM] ₀ × (D2EHPA)	-3.65	2.77	-1.32	0.21
Salts × internal phase	-0.23	2.77	-0.08	0.94
Salts × (D2EHPA)	1.51	2.77	0.55	0.60
internal Phase × (D2EHPA)	-0.99	2.77	-0.36	0.73

3.3. Mathematical model

The mathematical model is a second degree and relates the extraction yield to the different factors, their squares and their interactions. For coded units the model is represented by equation 2:

$$\begin{aligned} R(\%) = & 93.5420 - 1.6353 \times [\text{BM}]_0 - 3.4873 \times (\text{salt}) \\ & - 2.0793 \times (\text{internal phase}) + 1.4818 \times (\text{Extractant}) \\ & + 2.5611 \times [\text{BM}]_0^2 - 6.1477 \times (\text{salt})^2 + 14.2781 \times (\text{internal phase})^2 \\ & - 0.5935 \times (\text{Extractant})^2 - 0.4216 \times [\text{BM}]_0 \times (\text{salt}) \\ & + 2.8231 \times [\text{BM}]_0 \times (\text{internal phase}) + 3.6508 \times [\text{BM}]_0 \times (\text{Extractant}) \\ & + 0.2315 \times (\text{salt}) \times (\text{internal phase}) - 1.5076 \times (\text{salt}) \times (\text{Extractant}) \\ & - 0.9902 \times (\text{internal Phase}) \times (\text{Extractant}) \end{aligned} \quad (2)$$

3.4. Effects of factors

A factor may be a qualitative or quantitative variable, continuous or discontinuous, controllable or uncontrollable.¹⁵ Figure 1 shows the effect of the factors studied in the chosen domain on the yield of MB extraction.

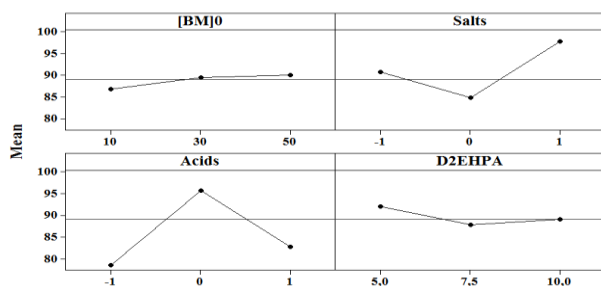


Figure1. Effects of factors.

Two effects are observed; the first is a negative effect of 5 to 7.5% by mass and a second positive effect of 7.5 to 10% by mass (with a weak slope). It can be said that the yield is good at a minimum level of the mass percentage of extractant. This is explained with a high mass percentage extractant (D2EHPA) the membrane becomes a little viscous, which means that the transfer is difficult.¹⁶

It is observed that there are two slopes, a negative one from KCl (-1) to NaCl and a positive slope from NaCl to Na₂SO₄. Therefore, we can say that the presence of Na₂SO₄ promotes the extraction of methylene blue which it has been obtained a yield of 97.76%. It was observed that there is a positive effect from HCl to H₂SO₄ and a negative effect from H₂SO₄ to H₃PO₄. It was also found that the H₂SO₄ acid gives the best removal efficiency (95.77%) of methylene blue dye. So, we can explain this result by the presence of hydrogen ions (2H⁺) which promotes the discoloration of aqueous solutions of MB.¹⁷ It was observed that there is a positive effect of the initial

dye concentration with a moderately high slope (low inclination). It was found that increasing the dye concentration increases the yield of the dye extraction (from 86.83 to 90.10%). Therefore, the concentration of 50 ppm in methylene blue gives the best result.^{18,19}

3.5. Henry's line of residual values

Generally, Henry's line is useful for checking the normality of the model. We see that the points tend to form a line.

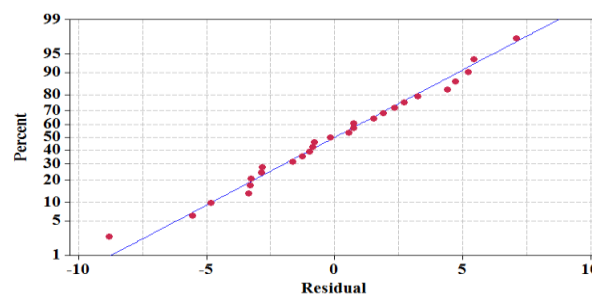


Figure 2. Henry's line of residual values for yield.

3.6. Graphics contour and surface responses

At an initial concentration of [BM]₀ equal to 50 ppm and in the presence of Na₂SO₄, it can be seen that the good yields are of the order of 100% in an average level for the acid (internal phase is sulfuric acid H₂SO₄) and at a concentration of minimum value of D2EHPA (5% m). The response surface is convex, giving the same findings of the contour.

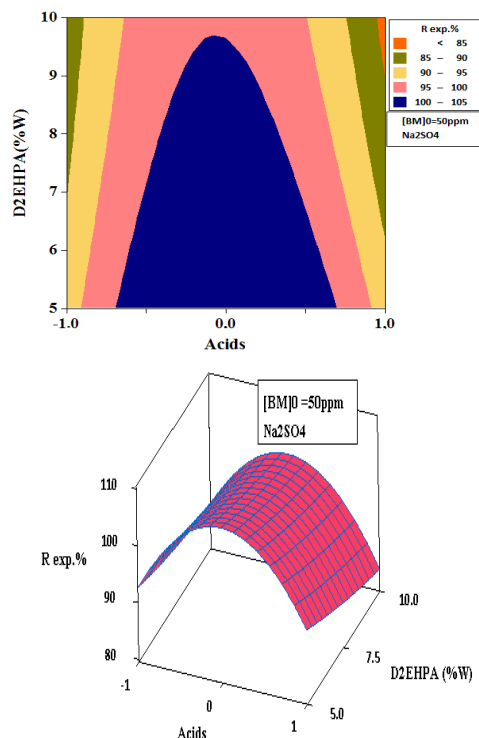


Figure 3. Graphic contour and surface responses as function of acid-D2EHPA with [BM]₀ = 50 ppm and Na₂SO₄ salt.

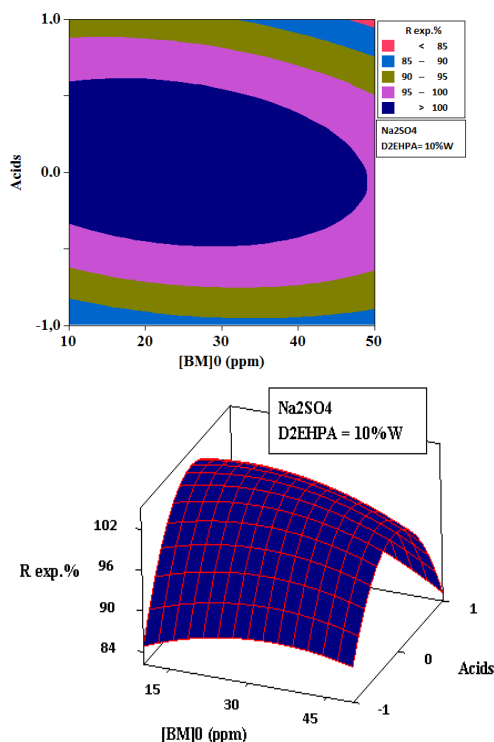


Figure 4. Graphic response contour as a function of $[BM]_0$ - acids with salt Na_2SO_4 and D2EHPA = 10% m.

By fixing the salt Na_2SO_4 and the mass percentage of D2EHPA at 10% m, it is noted that the good yields take a large place in the contour surface under the conditions $[BM]_0$ of (10ppm-50ppm) and in the presence of the phase internal H_2SO_4 . The response surface indicates the same observations

3.7. Experimental yield depending on the theoretical yield

From Figure.5 it can be seen that the experimental and estimated yields are distributed around the regression line ($R^2 = 0.9553$). The fit is very good, especially above 80%.

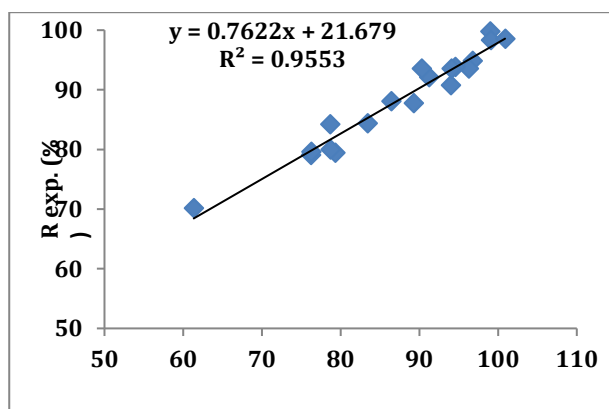


Figure 5. Graphical representation of measured responses as function of theoretical responses for BM extraction.

4. OPTIMISATION

The goal is to maximize the extraction yield. A constraint was imposed on studied factors. The best elimination of MB dye is obtained under optimal conditions: 30 ppm for the initial concentration of $[BM]_0$, 10%w for the extracting (D2EHPA) with the presence of Na_2SO_4 and H_2SO_4 .

Finally, we can say that in total we could extract the entire MB using the emulsified liquid membrane technique.

5. CONCLUSIONS

The elimination of the cationic pollutant "methylene blue" is influenced by several factors that have demonstrated the possibility of using the emulsified liquid membrane extraction process.

A membrane consists of a surfactant (span80), a diluent (fuel oil) and an extractant (D2EHPA) in the organic phase, varying the type of acids as an internal phase. In addition, an external aqueous phase of the MB dye mixture with salt at different concentrations of pollutant (MB) has been studied in order to find the optimal conditions that promote the extraction yield of the cationic dye MB.

From the Box-Behnken design, we obtained several information which increase the experimental yield of MB extraction. Thus, after optimizing the extraction of MB, we found the best optimal conditions, which are: a weight percentage of extractant equal to 10%w, the presence of sulfuric acid as the internal phase, the initial concentration of dye is 30 ppm, the salt that promotes extraction is Na_2SO_4 for total extraction of MB.

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Conflict of interests

I declares that there is no a conflict of interest with any person, institute, company, etc.

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