



Research Paper

Engineering Integrated Computational Materials with Non-Segregating Concrete for Sustainable Construction

Mohankumar N. BAJAD

Department of Civil Engineering, Sinhgad College of Engineering, Pune, Maharashtra, India
mnbajad@rediffmail.com

Received: 09.12.2022

Accepted: 15.05.2023

Abstract: Non-segregating concrete (NSC) is measured as an inventive structure substantial in erection manufacturing, aimed at the reason for its superb new and toughened features. As a consequence of the exhaustion of normal granular substantial stores, man-made granular substantial (MGM) is being exploited in place of fine aggregate (F.A.) instead of granular substantial. Keeping in view the fundamental nature of the degree of F.A., this examination is done to inspect the impact of various estimations of the mean dimensions (M.S) of MGM (2.3, 2.5, 2.7, 2.9, and 3.1) on the crisp features of NSC. The trial strategies that were directed are V-funnel, slump flow, L-box, and T50cm. Consequences indicated that NSC with MS estimation of 2.7 gave favor over other MS esteems. It is understood that from 2.3 to 2.7 MS esteems, the expansion in MS worth expanded the NSC's new features as a consequence of the reduction in the better division. It is additionally noticed that from 2.7 to 3.1 MS esteems, the expansion in MS worth diminished the NSC's crisp features due to an increase in the coarser division. Consequently, it is uncovered that a legitimate degree of better and coarser divisions of MGM must be reserved to acquire satisfactory NSC new features.

Keywords: aggregate, man-made granular substantial, non-segregating concrete.

1. Introduction

Non-segregating concrete (NSC) is a special type of flowable concrete that does not need any external vibration and can eat away at housings, and plug forms with reinforcements heavily obstructed under its weight [1]. In NSC, the aggregate contribution is approximately 60-70% of the total volume. The legal classification of totals requires urgent work with the apparent characteristics of concrete [2]. It is important to note that the properties of the outline and exterior of F.A. are significantly more significant than the impact rating, easy placement, pump ability, drainage, and insulation of brittle concrete. [4]. When all is said and done, the interest of normal MGM is highest in creating nations to fulfill the quick foundation development, in this circumstance, creating nations like India confront a lack of great excellence in granular and substantial development [5].

1.1 Aim and Objectives

It aims to find out the fresh properties of self-compacting concrete containing fly ash and artificial sand. The aim of this research was achieved through the following objectives:

- To find the workability of self-compacting concrete containing fly ash and artificial sand by slump flow
- To find fresh properties of self-compacting concrete containing fly ash and artificial sand by T50 cm slump flow
- To find the flowability of self-compacting concrete containing fly ash and artificial sand by V-funnel

How to cite this article

Bajad M. N., "Engineering Integrated Computational Materials with Non-Segregating Concrete for Sustainable Construction," *El-Cezeri Journal of Science and Engineering*, 2023, 10 (2), 349-355.

ORCID ID: *0000-0003-1056-0178

- d) To find the rheology of self-compacting concrete containing fly ash and artificial sand by L-box

2. Literature Survey

Especially in India, characteristic granular substantial stores are being exhausted and creating genuine danger just by the reserved ways of the general public. This has encouraged a few ecological issues in this mode of government by forcing a limit on the unlimited utilization of granular substantial [6]. This has made the shortage and huge ascent in the expense of natural granular substances substantial. Subsequently, an option in contrast to MGM has developed the necessity of countless reputations. A rare option for substantial material, viz. fly ash and limestone dust, has just been set aside in favour of a halfway standby of regular granular substantial concrete blends. In any circumstance, a shortage of mandatory excellence is a significant impediment to a slice of the substantial overhead. Presently, maintainable development requests the elective substantial that ought to fulfil the specialized necessities of F.A. Impartial by way of being accessible inexhaustibly. The special utilization of man-made granular substantial (MGM), which is reason-made FA created by squashing and screening, will ration the normal assets intended for the maintainable advancement of the concrete in the development industry. By utilizing proper effect pulverizing innovation, it is conceivable to create cubical molecule forms with unchanging reliability under measured circumstances [7]. Man caused granular substantiality to contain more fine content [8]. By and large, the fines are made out of shaky dust instead of the sediments and mud that result from granular substantial. By way of an effect of the nearness of more fine content, the MGM distresses the water request and the ease of placement of the mortar [9].

It is emphasized that man-made granular size is always superior to waterway granular size. The molecule shape is cubical, which is practically closer to adjusted MGM. Another issue related to MGM is that of mandatory evaluation with a mean dimension (MS) of 2.4 to 3.1. By and large, an mean dimensions (MS) of 2.2 to 2.6, 2.6 to 2.9, and 2.9 to 3.2 demonstrate that the granular substantially is fine, average, and coarse, affirming to evaluating sectors extending from IV to I (IS 383) [10]. It has been confirmed and appears to originate in dissimilar areas crosswise over south India that it has gotten progressively harder to get MGM of steady excellence regarding reviewing prerequisites and constrained sediment/mud content. If there should arise an occurrence of man-made granular substantiality with a well-structured screening framework, the needed evaluation and mean dimensions (2.4 to 3.1) can be reliably accomplished [11671]. It must be noted that appropriately assessed totals can improve both the new and toughened features of concrete. Inferable from the significance of reviewing F.A.s, this examination is done to assess the NSC crisp features utilizing MGM with various estimations of MS [11].

2.1 Literature Gap

As a result, in-depth research is required to address these issues in the present studies. Despite several studies being conducted in this area, the concerns listed below have not been addressed or resolved in earlier studies published as books, journal papers, or reports. For instance, research on the novel features of concrete, including fly ash and the substitution of natural sand with synthetic sand by V-funnel, L-box, and T50 cm, is still lacking. As a result, in-depth research is required to address these issues in the present studies.

2.2 Statement of Novelty

Support for hypotheses, information on individual efforts, procedures that have been approved, a fresh perspective, and expansion of the non-segregating concrete research area. The focus of the current study is on the workability of concrete containing fly ash when natural sand is replaced with synthetic sand.

When this study was compared to previous research on the subject or work done by others, it was discovered that the work or technique described in this publication had never been done or used previously.

Therefore, it can be said that investigations into the workability of concrete containing fly ash with natural sand replaced with artificial sand by slump flow are comparable to work previously reported in the literature, but that investigations into the rheological properties of concrete containing fly ash with natural sand replaced with artificial sand by V-funnel, L-box, and T50 cm are completely different from work previously reported in the literature.

3. Methodology and Investigational Study

Our goal was to decide the impact of various estimations of the mean dimensions (2.3, 2.5, 2.7, 2.9, and 3.1) of MGM on the crisp features of NSC. The trial strategies that were led are slump flow, T50cm slump flow, V-funnel, and L-box [12].

3.1. Substantial

OPC 53 evaluation compared to IS 12269:1987 and class F fly ash as indicated by ASTM C 618 [13] were utilized in this examination. The composition and physical properties of cement and fly ash are displayed in Table 1. Squash rock stones of size 12.5 millimeters were utilized as coarse aggregate (C.A.). The bulk specific gravity of the C.A. in the stove dry state and water assimilation were 2.6 and 0.3%, respectively. Man-made granular substantial (MGM) was used as fine aggregate (F.A.). The bulk specific gravity in the broiler dry state and water retention of MGM were, respectively, 2.61 and 1%. The degree of C.A. and F.A. were controlled by sifter examination according to IS 383:1970 [10] and introduced in Tables 2 and 3. Polycarboxylate ether-based synthetic water-soluble organic substances (SP) were utilized in non-segregating concrete (NSC). The level of dry substance in SP was 40.

Table 1. Chemical and physical features of cementitious substantial

Particulars	Cement	Class F fly ash
Chemical Composition		
% Sulphur Trioxide (SO ₃)	2.47	0.2
% Silica (SiO ₂)	19.80	66.6
% Alumina (Al ₂ O ₃)	5.66	27.0
% Iron Oxide (Fe ₂ O ₃)	4.69	3.0
% Lime (CaO)	61.82	1.0
% Magnesia (MgO)	0.85	1.0
Physical Features		
Specific Gravity	3.15	2.13
Fineness m ² /kg	311.6	361

Table 2. Gradation trial of 12.5-millimetre C.A.

Sieve size	Cumulative % Passing	IS 383:1970 limits
12.5 millimetre	99.65	85-100
10 millimetres	43.37	0-45
4.75 millimetre	6.68	0-10
2.36 millimetre	1.5	N/A

Table 3. Gradation trial of MGM with dissimilar MS

Sieve Size (millimetre)	Cumulative % Passing				
	MS - 2.3	MS - 2.5	MS - 2.7	MS - 2.9	MS - 3.1
4.75	95.00	94.00	92.90	91.70	91.40
2.36	91.40	87.00	87.00	84.00	82.00
1.18	83.00	74.00	68.00	66.00	65.70
0.6	74.00	55.00	50.00	42.00	38.00
0.3	15.00	27.00	20.00	19.81	20.00
0.15	12.00	11.00	10.00	7.85	6.00

3.2. Blend Proportions

NSC blends were set up with MGM having a diverse fineness of modulus (2.3, 2.5, 2.7, 2.9, 3.1) to assess the NSC's new features [opt]. rendering to EFNARC [14], the least C.A. substance of 28% was held in reserve for all the blends. Keeping in mind the reserve funds in charge and land-dwelling fill, ozone-reducing ingredient outflows, and crisp, mechanical, and durability features of NSC, the standby level of class F fly ash was saved at 35% according to IS 456:2000 [15] for all blends. Keeping in mind the moderate fineness and all NSC features, the water-cementitious proportion (w/cm) by weight was reserved at 0.36 for all blends. NSC blends have been assigned NSC-MS 2.3, NSC-MS 2.5, NSC-MS 2.7, NSC-MS 2.9, and NSC-MS 3.1 individually for dissimilar MS estimations of 2.3, 2.5, 2.7, 2.9, and 3.1. The blend proportion of all NSC blends stays the same and is exhibited in Table 4.

Table 4. NSC blend proportions

Blend	w/cm	Binder kg/m ³	Cement kg/m ³	Fly ash kg/m ³	Water l/m ³	12 millimetres kg/m ³	MGM kg/m ³	SP l/m ³
NSC	0.35	496	322	173	178	721	862	4.45

3.3 Trailing of NSC

According to EFNARC [16], trial techniques, e.g., slump flow, T50cm slump flow, V-funnel, and L-box [Figure 1], were completed to assess the crisp features of SCGC. A flow trial is conducted to decide the blowout of the NSC. T50 cm is estimated to show the thickness of the NSC. V-funnel time is estimated to demonstrate the reliability of the NSC, and the L-box trial is directed to assess the passing capacity of the NSC.



Figure 1. Experimental set up

4. Outcomes and Discussion

The NSC new features, i.e., slump flow, t50 cm, v-funnel time, and L-box proportion (h2/h1), are

introduced in Table 5 for all the proportions. Since Table 5, it is perceived that the blend NSC-MS - 2.3 got the slump flow blowout (T50 cm) and V-funnel time estimations of 595 mm, 5.69 sec, and 15.23 sec, separately; this blend got bombed in the L-box trial. This blend can be categorized as a disappointment blend as the new features of this proportion did not meet NSC acknowledgment standards. It is designed for the great trial portion owing to the expanded better portion of MGM at the inferior mean dimensions [17]. This better portion of MGM has a bigger explicit region, which requests more water and glue. The precise state of better particles additionally expands the plastic consistency which affects the ease of placement of NSC. It is observed that the new features of the blends NSC-MS-2.5, NSC-MS-2.7, and NSC-MS-2.9 have met the NSC acknowledgment standards and can be arranged as fruitful NSC blends. Out of these three fruitful blends, the presentation of NSC-MS-2.7 was seen to be superior to the next two blends, NSC-MS-2.5 and NSC-MS-2.9. It is likewise noticed that while the blend NSC-MS-3.1 got the slump flow blowout at T50 cm and V-funnel time estimations of 605 millimeters, 5.76 sec, and 14.38 sec, individually, this blend flopped in the L-box trial. This blend can also be arranged as a disappointment blend, as the crisp features of this blend did not meet NSC acknowledgment standards. It is meant for the great trial fragment owing to the expanded coarse portion of MGM at the higher MS (3.1). This coarser division holds progressively precise outlines and causes expanded yield pressure that impacts the ease of placement of NSC. From the outcomes, it is seen that from 2.3 to 2.7 MS esteems, the expansion in MS worth expanded the NSC crisp features as a consequence of the decrease in the better division. It is likewise noticed that from 2.7 to 3.1 MS esteems, the expansion in MS worth diminished the NSC's crisp features as a consequence of an increase in the coarser part. Henceforth, it is revealed that the appropriate degree of better and coarser divisions of MGM must be saved up to acquire sufficient NSC crisp features.

Table 5. New features of NSC blends

Blend type	L-box Ratio (h_2/h_1)	V- Funnel Time (Sec)	T _{50cm} (Sec)	Slump flow (millimetre)
NSC-MS - 2.3	Blocked	15.21	5.60	596
NSC-MS - 2.5	0.85	8.15	4.21	667
NSC-MS - 2.7	1.00	6.22	3.10	682
NSC-MS - 2.9	0.88	7.27	4.19	677
NSC-MS - 3.1	Blocked	14.33	5.79	601
Acceptance standards as per EFNARA	0.80-1.00	6-12	3-5	650-800

5. Concluding Remark

- 1) The NSC-MS-2.3 blend fizzled at mean dimensions of 2.3 by way of holding progressively better parts, which expanded the plastic thickness.
- 2) The blend NSC-MS-3.1 fizzled at mean dimensions of 3.1 by way of holding progressively coarser portions, which expanded the yield pressure.
- 3) Three blends, NSC-MS -2.5, NSC-MS -2.7, and NSC-MS -2.9, are arranged by effective NSC blend as they meet NSC acknowledgment standards.
- 4) Out of these three fruitful blends, the presentation of NSC-MS-2.7 was seen to be far superior to the next two blends, NSC-MS-2.5 and NSC-MS-2.9.
- 5) From the outcomes, it is seen that from 2.3 to 2.7 MS esteems, the expansion in MS worth expanded the NSC's new features due to a lessening in the better part.
- 6) It is likewise noticed that from 2.7 to 3.1 MS esteems, the expansion in MS worth diminished the NSC new features by way of an increment in coarser parts.
- 7) Thus, it is uncovered that a legitimate degree of better and coarser portions of MGM must be held in reserve to get sufficient NSC new features.

Acknowledgements

The author appreciates the enthusiastic cooperation of S. T. E. S. Pune administration. Any helpful suggestions, initiatives, and prompt assistance from individuals within a given discipline are much valued. We are grateful to all the authors whose works have, over time, given us directional knowledge. This paper would not have been possible without the technical and scientific staff of the Laboratory of Advanced Materials and Library's assistance.

Authors' Contributions

Author is a post Ph.D. researcher, did the investigations and wrote the manuscript. Author read and approved the final manuscript.

Competing Interests

The author declares that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

References

- [1]. ASTM C 618 Standard Specification for Coal Fly Ash and Raw or Calcined Natural Pozzolan for Use in Concrete, 100 Barr Harbor Drive, PO Box C700, West Conshohocken, PA 19428-2959. United States, ASTM International 2003.
- [2]. Indian standard 383 Specification for coarse and fine aggregates from natural sources for concrete, 9 bahadur shah zafar marg New Delhi 110002, Bureau of Indian standards manak bhavan,1970.
- [3]. Indian standard 456 plain and reinforced concrete - code of practice, 9 bahadur shah zafar marg New Delhi 110002, Bureau of Indian standards manak bhavan 2000.
- [4]. C. Alexandra, H. Bogdan, N. Camelia, K. Zoltan, "Mix design of self-compacting concrete with limestone filler versus fly ash addition," *Procedia Manufacturing*, vol. 22, pp. 301-308, 2018.
- [5]. EFNARC, Specification and guidelines for non-segregating concrete, European Federation of Producers and Applicators of Specialist Products for Structures. EFNARC, Association House, 99 West Street, Farnham, Surrey GU9 7EN, UK,2002.
- [6]. EFNARC, The NSC European Project Group. The European guidelines for non-segregating concrete: specification, production and use. EFNARC, Association House, 99 West Street, Farnham, Surrey GU9 7EN, UK. 2005.
- [7]. J. A. Sainz-Aja, I. A. Carrascal, J. A. Polanco, C. Thomas, "Effect of temperature on fatigue behaviour of self-compacting recycled aggregate concrete," *Cement and Concrete*, vol. 125, 2021.
- [8]. K. A. Ostrowski and K. Furtak, "The influence of concrete surface preparation on the effectiveness of reinforcement using carbon fibre-reinforced polymer in high-performance, self-compacting, fibre-reinforced concrete," *Composite Structures*, vol. 276, 2021.
- [9]. N. Gowripalan, P. Shakor, and P. Rocker, "Pressure exerted on formwork by self-compacting concrete at early ages: A review," *Case Studies in Construction*, vol. 15, e00642, 2021.
- [10]. N. Bheel, P. Awoyera, I. A. Shar, S. A. Abbasi, S. H. Khahro, K. Prakash A, "Synergic effect of millet husk ash and wheat straw ash on the fresh and hardened properties of Metakaolin-based self-compacting geopolymer concrete," *Case Studies in Construction Materials*, vol. 15, e00729, 2021.
- [11]. N. Garcia-Troncoso, Lufan Li, Q. Cheng, K. H. Mo, and T. Ling, "Comparative study on the properties and high temperature resistance of self-compacting concrete with various types of recycled aggregates," *Case Studies in Construction Materials*, vol. 15, e00678, 2021.

- [12]. O. M. Ofuyatan, F. Olutoge, D. Omole, A. Babafemi, "Influence of palm ash on properties of light weight self-compacting concrete," *Cleaner Engineering and Technology*, vol. 4, 100233, 2021.
- [13]. P. Niewiadomski, J. Hoła, "Failure process of compressed self-compacting concrete modified with nanoparticles assessed by acoustic emission method," *Automation in Construction*, vol. 112, 103111, 2020.
- [14]. S. C. Gnanaraj, R. B. Chokkalingam, G. L. Thankam, and S. K. M. Pothinathan, "Durability properties of self-compacting concrete developed with fly ash and ultra-fine natural steatite powder," *Journal of Materials Research and Technology*, vol. 13, pp. 431-439, 2021.
- [15]. I. Sosa, P. Tamayo, J. A. Sainz-Aja, C. Thomas, J. Setién, J. A. Polanco, "Durability aspects in self-compacting siderurgical aggregate concrete," *Journal of Building Engineering*, vol. 39, 102268, 2021.
- [16]. V. Revilla-Cuesta, M. Skaf, A. B. Espinosa, and V. Ortega-López, "Multi-criteria feasibility of real use of self-compacting concrete with sustainable aggregate, binder and powder," *Journal of Cleaner Production*, vol. 325, 129327, 2021.
- [17]. W.-Q. Hou, J.J. Yang, Z.X. Zhang, and X.-Q. Yuan, "Experimental study and application of manufactured sand self-compacting concrete in concrete-filled-steel-tube arch bridge: A case study," *Case Studies in Construction Materials*, vol. 15, e00718, 2021.