

International Journal of Earth Sciences Knowledge and Applications journal homepage: http://www.ijeska.com/index.php/ijeska

Research Article

e-ISSN: 2687-5993

Determination of Groundwater Status and Characteristics of the Subsurface Layers Using Electrical Vertical Sounding (VES) and Dipole-Dipole Configuration at Osasogie Road and Environs Southern, Nigeria

Ese Anthony Aladin¹*, Sikiru Salami¹, Omasan Akperi¹

¹Department of Geology, University of Benin, Benin City, Nigeria

INFORMATION

Article history

Received 27 April 2023 Revised 26 June 2023 Accepted 26 June 2023

Keywords

Transmissivity Aquifer zone Subsurface Resistivity Dipole-Dipole

Contact

*Ese Anthony Aladin anthonyoriginal26@gmail.com

ABSTRACT

The study area is situated between latitudes 5.605188°N to 5.622456°N and longitudes 6.377649°E to 6.389605°E and the aim of this study is to determine the groundwater status and characterise the subsurface layers using Electrical Vertical Sounding (VES) and Dipole- Dipole configuration at OSASOGIE Road and Environs Southern, Nigeria. ABEM SAS-300C Terrameter along with necessary accessories equipment were used to carried out eleven (11) VES and one (1) Dipole-Dipole data acquisition. From the results interpretation of VES 1-11, it reveals five (5) to six (6) geo-electric layer and the aquifer apparent resistivity ranges from $646.45\Omega m$ to $3852.6\Omega m$ with an average of $2249.62\Omega m$. The presence clay materials in the study have depth range of 7m to 14m deep which has a negative impact on the roads constructed in the area. When rain falls, the roads are flooded causing the clay materials to expand and contrast leading to cracks on the road, because the Engineering geologist and Civil engineers fails to identify characteristics of the subsurface soil. From the result of Dipole-Dipole, it is revealed that the profile point from 60m to 150m at a depth of 0.0m to 20.0m has very low resistivity and very high conductivity because the surface soil has a high porosity and high permeability which allow surface water to flow into the soil. The Longitudinal conductance values range from 0.00416 to 0.06025 Ω -1 with an average of 0.032205 Ω -1 and Transmissivity values range from 452.869248 to 504.481402 m2/day with an average of 478.675325m2/day. The presence of clay materials in the subsurface soil of the study must be excavated first during construction of road to avoid failure and crack in the road. This research will help engineering geologist and civil engineer to suggest the best foundation design for a building and reduce cost of maintenance of failed if the clay material is put into consideration first before construction.

1. Introduction

Flooding, Failed Road and contaminated water bodies is a major in developing countries like Nigeria. Flood and Failed Roads are major problems in Benin city especially the Osasogie road and environs in Egor local Government Area of Edo State (ELGA, 2021). This problem is a serious issue, because it has caused many house owners to relocate from their homes. When rain falls the road is flooded which causes the road to fail because the water does not infiltrate easily into soil and also there is bad drainage system in that area leading to the contamination of the groundwater in that area. The aim of this research is to determine and identify the

lithological characteristics of the subsurface soil using VES and dipole-dipole survey of electrical resistivity method. This research work will enable Civil Engineers and Engineering Geologist to have proper knowledge of the subsurface layer characteristics and to safe money in reconstruction of the failed roads. This research will help people living around the study area to know whether the groundwater is contaminated or not.

The VES method is used to investigate the electrical properties of subsurface layers and it has been used for wide variety of environmental and engineering problems (Zohdy,

Copyright (c) 2023 Authors



This work is licensed under a Creative Commons Attribution-NonCommercial-NoDerivatives 4.0 International License. The authors keep the copyrights of the published materials with them, but the authors are agree to give an exclusive license to the publisher that transfers all publishing and commercial exploitation rights to the publisher. The publisher then shares the content published in this journal under CC BY-NC-ND license.

1975). This geophysical method is used because it is one of the simplest and less costly methods and can be used to identify geological structures (Al-Sayed et al., 2007). The VES had been used to delineate the different subsurface layers and also been used in delineating the aquifer units, subsurface structure and their characteristics (Okonkwo et al., 2013).

The study is carried out in Egor Local Government Area (ELGA, 2021), Benin City, Edo State. It is situated between latitudes 5.605188°N to 5.622456°N and longitudes 6.377649°E to 6.389605°E. Egor Local Government Area falls under the Tropical Savannah Climate while the LGA covers a total area of 93 km² (Giuseppe et al., 2019; ELGA, 2021). It has an area of 93 km² and a population of 444171 (National Bureau of Statistic, 2020).

There are different tribal groups that made up the local government namely: the Esan, Bini, and the Owan. The area experiences two major seasons which are the rainy and the dry seasons while the average temperature of the area is at 28 °C. The estimated humidity level of the Egor Local Government Area (ELGA, 2021) is estimated at 68 percent. The people are predominantly farmers.

Benin City's climate is hot and humid. The rainy season is from April to November while the dry season is from December to March. Temperature in Benin City is very high with an average daily temperature of about 28 °C in the dry season and about 24 °C in the wet season. The study area has a low temperature range. Benin City and its environs experience intense rainfall especially in the rainy or wet season. Rainfall is present all year, with an annual total of 2000–2300 mm, and monthly average of about 180 mm (Ministry of Environment, Benin Report, 2009). This intense rainfall is induced by excessive evapotranspiration in the urban area due to prevalent high temperature. Relative humidity in the study area is also high, reaching about 80% in the wet season and 70% in the dry season (Manpower Nigeria, 2020).



Fig. 1. Base map of the study area

2.1. Geology of the Study Area

The Delta Region is underlain by Sedimentary Formation of the South Sedimentary Basin (Short and Stauble, 1967). The South Sedimentary Basin is made up of Sedimentary Formation which the Benin Region is lying on. The geology is marked by top reddish earth, composed of ferruginous or lateralized clay sand. The term Benin sand was first used to describe the reddish earth underlain by sands, sandy clays and ferruginous sandstone that marked the Paleo-coastal Environment of Paleocene-Pleistocene Age. Delta Region comprises of Benin Formation, alluvium, drift/top soil and Azagba-Ogwashi (Asaba-Ogwashi) Formation (Short and Stauble, 1967). The geology of the study area is marked by lateralized Clay, Sand and Sandstone. The Sandstone marks the Paleo-Coastal Environment of Palaeocene-Pleistocene Age (Reyment, 1965). These sediments spread across the southern fringes of the Anambra Basin and marking the upper facies off-flaps of the Niger Delta Basin (Catherine, 2016). The name Coastal Plain Sands is use to describe the Formation of red earth underlain by Sands and Clays that mark an ancient Coastal Plain Environment now exposed in Calabar, Owerri, Onitsha (Catherine, 2016). The Delta Region is Oligocene-Pleistocene in age. The dip direction of the Benin Formation southward.



Fig. 2. Geological map of Delta State, Nigeria

The study area is underlain by the Benin Formation which is an important groundwater reservoir. This basin is characterized by top reddish to reddish brown lateritic massive fairly indurated clay and sand, capping thick sequences of poorly bedded friable-loose sand gravelly- pebbly sand and pinkish-white clay stringers (Oomkens, 1974).



Fig. 3. Schlumberger array



Fig. 4. Dipole-dipole array

The hydraulic conductivity and transmissivity have an average value of 20.662 m/day and 893.57 m²/day, respectively. Four groundwater potential zones were delineated including medium grain sandstones, sand, clayey-sand and shaly-sand (Kwami et al., 2019).

In 'Characterization of Aquifers Using Geo-electrical Methods in Parts of Abia State, South-eastern Nigeria', the highly productive aquifers in Abia State are confined to the alluvial deposits and the coastal plain sands lithologies, which consist of fine, medium and coarse-grained and often siliceous sands with some intercalation of clays. The alluvium occurs mainly in the Ukwa West and East local government areas. Drilling depths in this aquifer range from 30 m to 140 m (Abija et al., 2018).

| Table 1. A summary of the VES interpretation and resistivity model parameter | and lithology |
|--|---------------|
|--|---------------|

| S/N | Coordinate point | Geo-electric layers | Resistivity (Ωm) | Thickness (m) | Depth (m) | Lithology | Curve Type |
|--------|---|----------------------------|--|---|---|--|------------|
| VES 1 | 6.38888°N, 5.62056°E Elevation: 102 m | 1 2 3 4 5 | 64.777 233.48 1351.5 1272.4 286.92 | 0.72979 7.0064 5.0315 30.463 Infinity | 0.72979 7.72064 12.768 43.231 Infinity | Top soil Lateritic Clay Medium-Coarse Sand Medium-Coarse Sand (aquifer zone) | AKQ |
| VES 2 | 6.38583°N, 5.61972°E Elevation: 106 m | 1 2 3 4 5 | 133.97 308.58 959.3 2543.4 3636.7 | 0.8395 0.74536 23.873 10.624 Infinity | 0.8395 1.5849 25.457 36.081 Infinity | Top soil Lateritic Clay Medium Sand Medium-Coarse Sand (Aquifer zone) | AKA |
| VES 3 | 6.38700°N, 5.61678°E Elevation: 106 m | 1 2 3 4 5 | 84.223 205.75 114.38 1267.4 20.821 | 0.69649 7.7159 6.2064 27.441 Infinity | 0.69649 8.4124 14.619 42.059 Infinity | Top soil Lateritic Clay Silt Medium-Coarse Sand | АНК |
| VES 4 | 6.38475°N, 5.61642°E Elevation: 108 m | 1 2 3 4 5 | 178.14 410.61 191.5 1915.8 761.6 | 0.8279 4.0902 7.3309 32.691 Infinity | 0.8279 4.9181 12.332 44.94 Infinity | Top soil Clay Silt Medium-Coarse Sand | КНК |
| VES 5 | 6.38698°N, 5.61344°E Elevation: 108 m | 1 2 3 4 5 | 95.839 407.33 643.06 879.21 210.89 | 1.0826 5.9593 35.009 52.979 Infinity | 1.0826 7.0418 42.051 95.03 Infinity | Top soil Clay Fine Sand Medium Sand (Aquifer zone) | AAK |
| VES 6 | 6.38344°N, 5.61444°E Elevation: 108 m | 1 2 3 4 5 6 | 38.928 405 276.25 255.31 2681.6 137.71 | 0.55197 1.0373 4.9671 6.4387 37.677 Infinity | 0.55197 1.5892 6.5564 12.995 50.672 Infinity | Top soil Clay Clay Clay Medium-Coarse Sand (Aquifer zone) | КНК |
| VES 7 | 6.38791°N, 5.614917°E Elevation: 112 m | 1 2 3 4 5 6 | 110.28 207.2 352.46 86.143 2106.5 2672.1 | 1.0922 2.6522 10.545 18.664 25.129 Infinity | 1.0922 3.7443 14.289 32.953 58.082 Infinity | Top soil Clay Clay Silt Medium-Coarse Sand (Aquifer zone) | АКН |
| VES 8 | 6.38287°N, 5.620262°E Elevation: 110 m | 1 2 3 4 5 | 62.198 266.83 2149.4 3852.6 3216.3 | 0.32082 6.4922 2.9061 37.522 Infinity | 0.3978 6.813 9.7191 47.242 Infinity | Top soil Clay Medium-Coarse Sand Medium-Coarse Sand (Aquifer zone) | AKA |
| VES 9 | 6.39340°N, 5.615137°E Elevation: 108 m | 1 2 3 4 5 | 31.187 221.64 3083.3 646.45 235.6 | 0.59836 8.6452 9.6362 21.076 Infinity | 0.59836 9.2436 18.88 39.956 Infinity | Top soil Clay Medium-Coarse Sand Fine Sand | AAK |
| VES 10 | 6.38344°N, 5.61508°E Elevation: 108 m | 1 2 3 4 5 6 | 50.884 1147.6 123.41 5263.5 924.35 557.32 | 1.0666 1.3438 1.2575 19.25 34.78 Infinity | 1.0666 2.4104 3.6679 22.918 57.698 Infinity | Top soil Lateritic Sandy-Clay Silt Medium-Coarse Sand Medium Sand (aquifer zone) | НАА |
| VES 11 | 6.38583°N, 5.619725°E Elevation: 106 m | 1 2 3 4 5 6 | 8.5807 1879.5 87.042 190.28 1123.3 739.39 | 0.35327 2.4528 5.0626 4.6882 31.9 Infinity | 0.35327 2.8061 7.8687 12.557 44.457 Infinity | Top soil Lateritic Sandy-Clay Silt Silt Medium-Coarse Sand (Aquifer zone) | АКА |

Also, in 'Geoelectric Evaluation of Aquifer Vulnerability in Igbanke, Orhionmwon Local Government Area of Edo State, Nigeria. The results of the geoelectric investigation revealed six geoelectric layers namely the topsoil, laterite clayey sand, fine to medium sand, medium sand, medium to coarse Sand and coarse sand which are in agreement with the driller's log obtained from the borehole. The overburden protective capacity in the area was evaluated using the total longitudinal unit conductance values. The values obtained show poor and weak protective capacity rating in almost all parts of the study area. The aquifer of the study area is not protected since the protective capacity rating is poor (< 0.1) (Egbai et al., 2015).

According to Ojeogal et al. (2022), Geotechnical Investigations of Road Failures along Benin Technical School Road, Benin City, Edo State was carried out. The results of the test showed that the soil samples were mainly silty /clay with little amount of fine sand and the CBR result reveals none of the soil samples met the criteria for road subgrade as CBR values for all the soil samples were above the required 10%.

Findings indicates that failure along the study area were due to the unsuitability of the soils as sub grade material and effect of ground water intrusion and unstable geotechnical properties of soils in the study area, wrong drainage designs and improper application and usage of constructional materials.

| Table 2. A Summary of electrical properties of aquifer for all VES stations |
|---|
|---|

| S/N | Resistivity (ρ, Ωm) | Thickness (m) | Conductivity $(\delta, \Omega m^{-1})$ | Longitudinal conductance (S, Ω^{-1}) | Transverse Resistance (TR, Ωm^2) | Hydraulic conductivity (K) | Transmissivity (Tr, m²/day) |
|---------------|------------------------|------------------|--|--|---|-------------------------------|--------------------------------|
| VES 1 | 1272.4 | 30.463 | 0.00078 | 0.02394 | 38761.12 | 15.95620 | 486.073721 |
| VES 2 | 2543.4 | 10.624 | 0.00039 | 0.00416 | 27021.08 | 42.62700 | 452.869248 |
| VES 3 | 1267.4 | 27.441 | 0.00079 | 0.02165 | 34778.72 | 17.89541 | 491.067946 |
| VES 4 | 1915.8 | 32.691 | 0.00052 | 0.01706 | 62629.42 | 14.93940 | 488.383925 |
| VES 5 | 879.21 | 52.979 | 0.00114 | 0.06025 | 46579.67 | 9.522290 | 504.481402 |
| VES 6 | 2681.6 | 37.677 | 0.00037 | 0.01405 | 101034.64 | 13.08657 | 493.062697 |
| VES 7 | 2106.5 | 25.129 | 0.00047 | 0.01193 | 52934.24 | 19.09465 | 479.829460 |
| VES 8 | 3852.6 | 37.522 | 0.00026 | 0.00974 | 144549.55 | 13.13699 | 492.926139 |
| VES 9 | 646.45 | 21.076 | 0.00155 | 0.03260 | 13624.580 | 22.49924 | 474.193982 |
| VES 10 | 924.35 | 34.780 | 0.00108 | 0.03763 | 32148.893 | 14.10063 | 490.419911 |
| VES 11 | 1123.3 | 31.900 | 0.00089 | 0.02840 | 35833.270 | 15.28467 | 487.580973 |

3. Materials and Methods

In this research work, the Dipole-Dipole and Schlumberger array of Electrical Resistivity Survey method was adopted. ABEM Terrameter SAS 300C was used to carry out this survey which is powered by a 12.5v D.C power source. Other accessories attached to the Terrameter includes the booster, four metal electrodes, cables for current and potential electrodes, hammers (3), measuring tapes, mobile phones for a long-distance spread. Dipole-Dipole array is also called 2D resistivity surveying and its electrode spacing configuration is 10 m.

The Schlumberger configuration was adopted for the vertical electrical sounding with a maximum current electrode separation AB of 430 m, which was deemed sufficient in allowing a depth penetration of 215 m (AB/2) while the Potential electrode separation was increased several times during the sounding at MN/2 equals 0.2 m to 10 m. A Global Positioning Satellite (Germin model) instrument was used to determine well coordinates and elevation. Different electrode spacing is used when sending electric current into the ground depending on which part of the earth the anomaly is to be investigated.

3.1. Field Methods

The Schlumberger array is more complex when spacing between the current electrodes is not equal to the spacing between the potential electrodes. The vertical electrical sounding with Schlumberger array as a low-cost technique and veritable tool in groundwater exploration is more suitable for hydrological survey of sedimentary basin. The method is regularly used to solve a wide variety of groundwater problems. Formula for geometric factor (G) and Apparent Resistivity (pa) for Schlumberger array is given as:

$$G = \pi \frac{b(b+a)}{a}, \rho a = \frac{V}{I} \pi \frac{b(b+a)}{a}$$
(1)

Dipole-Dipole array uses apparent resistivity to generate 2D imaging which represent the various layers in subsurface soil. The spacing between the current electrode pair, C2-C1, is given as 'a' (Ria, 2017) which is the same as the distance between the potential electrodes pair P1-P2. The array has another factor marked as 'n' which is the ratio between the C1 and P1 electrodes to C2-C1 (or P1-P2) dipole separation 'a'. For surveys with this array, the 'a' spacing is initially kept fixed and the 'n' factor is increased from 1 to 2 to 3 until up to about 6 in order to increase the depth of investigation (Loke, 2000).

The array is most sensitive to resistivity changes between the electrodes in each dipole pair. Note that the sensitivity contour pattern is almost vertical. Thus, the dipole array is very sensitive to horizontal changes in resistivity. That means it is good in mapping vertical structures, such as dykes and cavities, but relatively poor in mapping horizontal structures such as sills or sedimentary layers (Loke, 2004).

The median depth of investigation of this array also depends on the 'n' factor, as well as 'a' factor. The formular for Geometric factor (*G*) and Apparent resistivity (ρ_a) for Dipole-Dipole arrey is given as:

$$G = \pi a n (n+1)(n+), \rho a = \frac{V}{I} \pi a n (n+1)(n+2)$$
 (2)

3.2. Data Processing

The data collected were pre-processed by ensuring data quality, and calculating the resistivity of the various reading

by multiplying it with the necessary constant. Also, field graphs were plotted using manual graphs. The IX1Dv3 and Dipro software application was used to determine the thickness and resistivity values. The Schlumberger values was first match curve manually before inputting it into the computer software program to obtained the resistivity model parameters and the values is now run by the program as a routine which in turn displayed an automatically plotted graph with an error tolerance limit set forth eprogram iteration and when this is done, the model parameters become the interpreted geoelectric layer as shown in the Table 1. The data obtained, both from Schlumberger and Dipole-Dipole array were analyzed using the geophysical software IX1Dv3 and Dipro. The geoelectric layers, depth was generated, as well as the resistivity spread. The analyzed data was interpreted to determine the aquifer potential and delineate the lithology of the investigated area.

The resistivity values and depths obtained after iteration were used to interpret the lithology of the study area which showed five (5) to six (6) layers from the eleven (11) VES location and five layers from the Dipole-Dipole location respectively as shown in (Table 1 and 5, Figs. 4 and 5).



Fig. 5. Map of study area showing the variation in Longitudinal Conductance



Fig. 6. Map of study area showing the variation in Transmissivity

3.3. Hydraulic Parameters

Longitudinal conductance (S) is a measure of the impermeability of a rock layer (Billing, 1972). The formulas for longitudinal conductance and Transverse Resistance is given as;

$$Si = \frac{h1}{\rho_1} \tag{3}$$

 $Ti = \rho 1 \times h 1 \tag{4}$

For a sequence of horizontal, homogeneous and isotropic

layers of resistivity $\rho 1$ and thickness h1. Eqs. 3 and 4 defined the Dar Zarrouk parameters (Maillet, 1947), (Longitudinal conductance (S) and Transverse resistance (TR) as follows:

$$S = \frac{h1}{\rho 1} + \frac{h2}{\rho 2} + \frac{h3}{\rho 3} \dots \dots \dots \dots \dots \dots \dots \sum_{i=o}^{n} \left(\frac{hi}{\rho i}\right)$$
(5)

For Transverse Resistance (TR)

$$TR = h1\rho 1 + h2\rho 2 + h3\rho 3 \dots \dots \sum_{i=0}^{n} (hi\rho i)$$
 (6)

It shows the relationship between aquifer transmissivity, and longitudinal conductance as proposed by Todd (1980).

$$Tr = K\delta TR = Kh \tag{7}$$

where *Tr*: aquifer transmissivity, *K*: hydraulic conductivity, σ : electrical conductivity (reciprocal of resistivity), *TR*: traverse resistance, *S*: longitudinal conductance and *h*: aquifer thickness. The tydraulic conductivity (*K*) was determined using the equation given by Heigold et al. (1979).

$$K = 386.40 Rrw^{0.93283} \tag{8}$$

4. Interpretation of Results

4.1 Interpretation for Schlumberger Array

The apparent resistivity of VES 1–11 obtained from the field for aquifer yield potential ranges 646.45 to 3852.6 Ω m with thickness range of 10.624 to 52.979 m, the drill depth to

groundwater for VES 1 ranges from 33 m (108) to 44m(144ft); VES 2 ranges from 36 m (118ft) to 46 m (150 ft); VES 3 ranges from 56 m (184 ft) to 66 m (216 ft); VES 4 ranges from 36 m (118 ft); VES 5 ranges from 44 m (144 ft) to 54 m (177 ft); VES 6 ranges from 48 m (157 ft) to 58 m (190 ft); VES 7 ranges from 33 m (108 ft) to 59 m (193 ft); VES 8 ranges from 46 m (151 ft) to 56 m (184 ft); VES 9 ranges from 43 m (143 ft) to 53 m (174 ft); VES 10 ranges from 43 m (141 ft) to 61 m (200 ft); and VES 11 ranges from 33 m (108 ft) to 43 m (141 ft). The curve types for VES 1-11 are: AKQ, AKA, AHK, KHK, AAK, KHK, AKH, AKA, AAK, HAA, and AKA.

The electrical properties of the aquifer are conductivity, longitudinal conductance, transverse resistance, hydraulic conductivity and transmissivity. The conductivity ranges from 0.00026 to 0.00155 Ω m⁻¹, longitudinal conductance ranges from 0.00416 to 0.06025 Ω ⁻¹, transverse resistance ranges from 13624.580 to 144549.55 Ω m².

Table 3. A Summary of longitudinal conductance(S) and transmissivity (Tr) of aquifer with its indication according to (Oladapo and Akintorinwa 2007; Offodile, 1983)

| S/N | Location coordinate points | Longitudinal conductance (S, Ω^{-1}) | Protective capacity rating | Transmissivity (Tr, m²/day) | Classification of well |
|---------------|---|--|----------------------------|--------------------------------|------------------------|
| VES 1 | 6.38888°N, 5.62056°E Elevation: 102 m | 0.02394 | Poor | 486.073721 | Moderate potential |
| VES 2 | 6.38583°N, 5.61972°E Elevation: 10 6m | 0.00416 | Poor | 452.869248 | Moderate potential |
| VES 3 | 6.38700°N, 5.61678°E Elevation: 106 m | 0.02165 | Poor | 491.067946 | Moderate potential |
| VES 4 | 6.38475°N, 5.61642°E Elevation: 108 m | 0.01706 | Poor | 488.383925 | Moderate potential |
| VES 5 | 6.38698°N, 5.61344°E Elevation: 108 m | 0.06025 | Poor | 504.481402 | Excellent potential |
| VES 6 | 6.38344°N, 5.61444°E Elevation: 108 m | 0.01405 | Poor | 493.062697 | Moderate potential |
| VES 7 | 6.38791°N, 5.614917°E Elevation: 112 m | 0.01193 | Poor | 479.829460 | Moderate potential |
| VES 8 | 6.38287°N, 5.620262°E Elevation: 110 m | 0.00974 | Poor | 492.926139 | Moderate potential |
| VES 9 | 6.39340°N, 5.615137°E Elevation: 108 m | 0.03260 | Poor | 474.193982 | Moderate potential |
| VES 10 | 6.38344°N, 5.61508°E Elevation: 108 m | 0.03763 | Poor | 490.419911 | Moderate potential |
| VES 11 | 6.38583°N, 5.619725°E Elevation: 106 m | 0.02840 | Poor | 487.580973 | Moderate potential |

Table 4. Aquifer protective capacity of longitudinal conductance (according to Oladapo and Akintorinwa (2007)) and aquifer classification based on transmissivity values (Offodile, 1983)

| S/N | Longitudinal Conductance (Ω-1) | Protective Capacity Rating | Transmissivity (m2/day) | Classification of well |
|-----|--------------------------------|----------------------------|-------------------------|------------------------|
| 1 | >10 | Excellent | >500 | High potential |
| 2 | 5–10 | Very good | 50–500 | Moderate potential |
| 3 | 0.7–4.9 | Good | 5–50 | Low potential |
| 4 | 0.2–0.69 | Moderate | 0.5–5 | Very low potential |
| 5 | 0.1-0.19 | Weak | <0.5 | Negligible potential |
| 6 | <0.1 | Poor | | |

Table 5. Summary of 2D resistivity structure of Dipole-Dipole array

| Layers | Colour Indication | Resistivity Ranges | Lithology |
|--------|--------------------------|---------------------------|--------------------------------------|
| 1 | Blue | 20.8 – 52.5 Ωm | Leachate |
| 2 | Green | $52.5-472 \ \Omega m$ | Clay |
| 3 | Yellow | 544 – 929 Ωm | Fine – Medium Sand |
| 4 | Light Brown | 1111 - 3498 Ωm | Medium – Coarse Sand |
| 5 | Deep Brown | 4114 - 13374 Ωm | Coarse - very Coarse Sand, Sandstone |



PG2019 DD L1 (Field Data Pseudosection)

PG2019 DD L1 (Theoretical Data Pseudosection)







Fig. 7. Dipro Inversion based on FEM modeling of Dipole-Dipole array

Hydraulic conductivity ranges from 9.522290 to 42.62700 and the transmissivity ranges from 452.869248 to 504.481402 m²/day as in Figs. 6 and 7. The aquifer has a poor protective capacity because the overburden lithology is highly porous according to Oladapo and Akintorinwa (2007) and the transmissivity classification of the wells is moderate to excellent Offodile (1983) as shown in Table 2, 3 and 4.

4.2. Interpretation for Dipole-Dipole Array

From Table 5, Figs. 7 and 8), it reveals that the blue colouration represent leachate which has apparent resistivity range of 20.8 Ω m to 52.5 Ω m, the green colouration represents the topsoil (surface) of the study area which has apparent resistivity range of 52.5 Ω m to 472 Ω m which is mainly made-up clay materials of low resistivity. While the yellow colouration represents immediate layer which has apparent resistivity range of 544 Ω m to 929 Ω m which is mainly fine to medium sand then the light brown colouration represents the weathered rock which has apparent resistivity range of 1111 Ω m to 3498 Ω m which is medium to coarse sand and the red colouration represent bedrock which has apparent resistivity range of 4114 Ω m to 13374 Ω m which is mainly coarse to very coarse sand with little present of sandstones.

It is revealed that the leachate has migrated from 60 m to 130

m along the horizontal profiling with a depth range of 0 m to 10 m deep and 130 m to 140 m along the horizontal profiling with depth 0m to 20m deep, the leachate has infiltrated deep into the soil to contaminated the groundwater at 20 m deep because the surface soil has a high porosity and high permeability which allow surface water to flow into the soil.

5. Discussion

From Table 1, VES 3, 4, 6, 7 and 11 with 6.38700°N, 5.61678°E with an elevation of 106m and 6.38475°N, 5.61642°E with an elevation of 108m, 6.38344°N, 5.61444°E with an elevation of 108m, 6.38791°N, 5.614917°E with an elevation of 112 m and 6.38583°N, 5.619725°E with an elevation of 106 m respectively. The result reveal that both locations has more of clay-materials and Silt in the subsurface soil up to a depth of 14m, the presence of the clay-material and silt has caused the road constructed in those location to fail because when the clay materials come in contact with water its expanse and contrasts which cause the road to crack or fail and full of pot-holes. When rain falls the water does not easily infiltrate into the soil, the water stays in the location for a long time, which causes the road in that area to fail. This fail roads costs the Edo State government a lot of money to maintain but with this research the engineering geologist and civil engineers will be able to provide measure to avoid failure of road in that area.

From Tables 2 and 3, the aquifer protective capacity is poor because the sediment/lithology overlying the aquifer is porous and the aquifer transmissivity classification is moderate to excellent.

From Tables 1 and 5, the apparent resistivity values from the VES 1-11 and Dipole-Dipole array ranges from $646.45 \ \Omega m$

to 3852.6 Ω m and 1111 Ω m to 3498 Ω m respectively. The lithology of the aquifer zone is medium to coarse Sand.

From Figs. 7 and 8, the survey reveals the presence of leachate plume which has infiltrate into subsurface soil to a depth of 20 m and can contaminate the groundwater because the aquifer protecting capacity is poor.









Fig. 8: Dipro Inversion based on FEM modeling with contour of Dipole-Dipole array

6. Conclusion and Recommendation

6.1. Conclusion

The aquifer transmissivity classification is moderate and the water yield of boreholes in the study will be also moderate. The curve types are: AKQ, AKA, AHK, KHK, AAK, KHK, AKH, AKA, AAK, HAA, and AKA. The software used to analysis the data are IX1Dv3 and Dipro respectively. This research has been to discover the cause of the failed roads and suggest solution to the failed road in the study.

The presence of clay materials in the subsurface soil of the study must be excavated first during construction of road to avoid failure and crack in the road. This research will help engineering geologist and civil engineer to suggest the best foundation design for a building and reduce cost of maintenance of failed if the clay material is put into consideration first before construction.

6.2. Recommendation

The recommended drill depth to groundwater for VES 1 is an average range of 38 m (126 ft); for VES 2 is an average range of 41 m (134 ft); for VES 3 is an average range of 60 m (200 ft); for VES 4 is an average range 41 m(134 ft); VES 5 is an average range of 49 m (160 ft); VES 6 is an average range 43 m (141 ft); VES 7 is an average range of 46 m (151ft); VES 8 is an average range of 51 m (167 ft); VES 9 is an average range of 48 m (158 ft); VES 10 is an average range of 52 m(170 ft); VES 11 is an average range of 38 m (125 ft). From (Figs. 5 and 6). I recommend deep borehole for the study area to avoid contamination from leachate plume. Soil test must be carried out before starting any project. Before construction of road is been carry out in the study, the clay materials must be excavated to a reasonable depth to avoid failure and loss of tax payer money on a failed project. Proper drainage system must be done to avoid infiltration of bad or wasted water into soil which will contaminate the groundwater in that area.

References

- Abija, F.A., Nwankwoala, H.O., 2018. Characterization of Aquifers Using Geo-electrical Methods in parts of Abia State, Southeastern Nigeria. Centre for Geomechanics, Energy and Environmental Sustainability (Igees), Port Harcourt, Nigeria. Sumerianz Journal of Scientific Research 1 (1), 1-7.
- Al-Sayed, E.A., El-Qudy, G., 2007. Evaluation of seawater intrusion using the electrical resistivity and transient electromagnetic survey: Case study at fan of Feiran, Sinai, Egypt. EGM 2007 International Workshop Innovation in EM, Grav and Mag Methods:a new Perspective for Exploration Capri, Italy.
- Ikhile, C.I., 2016. Geomorphology and Hydrology of the Benin Region, Edo State, Nigeria. International Journal of Geosciences 7, 144-157.
- Egbai, J.C., Efeya, P., Iserhien-Emekeme, R.E., 2015. Geoelectric Evaluation of Aquifer Vulnerability in Igbanke, Orhionmwon Local Government Area of Edo State, Nigeria. International Journal of Science, Environment 4 (3), 701-715.
- ELGA, 2021. Egor Local Government Area. Avaliable at: www.manpower.com.ng. Retrieved 2021-07-14.
- Floyd, A.C., Oikpor, R., Ekene, B., 2016. An Assessment of Climate Change in Benin City, Edo State, Nigeria. FUTY Journal of the Environment 10 (1), 1-10.
- Cirella, G.T., Iyalomhe, F.O., Adekola, P.O., 2019. Determinants of Flooding and Strategies for Mitigation: Two-Year Case Study of Benin City. Geosciences 9 (3), 136. https://doi.org/10.3390/geosciences9030136.
- Paul, H.C., Gilkeson, R.H., Cartwright, K., Reed, P.C., 1979. Aquifer Transmissivity from Surficial Electrical Methods. Groundwater 17, 330-345.
- Oseji, J.O., Egbai, J.C., Ijeh-Edoso, A.E., 2020. Aquifer vulnerability using geophysical and physiochemical methods in parts of Ethiope West Local Government Area of Delta State, Nigeria. AIP Advances 10, 1-21.
- Ojeaga, K., Archinbong, U.D., Afokoghene, A., 2022. Geotechnical Investigations of Road Failures Along

Benin Technical School Road, Benin City, Edo State. NIPES Journal of Science and Technology Research 4 (1), 179-185.

- Kwami, I.A., Ishaku, J.M., Mukkafa, S., Haruna, A.I., Ankidawa, B.A., 2019. Delineation of aquifer potential zones using hydraulic parameters in Gombe and environs, north eastern, Nigeria. Heliyon Journal 5, 1-13.
- Maillet, R., 1947. The fundamental equations of Electrical Prospecting. Geophysics 12 527-556.
- Ministry of Environment, 2009. Benin City Report; Ministry of Environment, Benin City: Benin City, Nigeria.
- Offodile, M.I., 1983. The Occurrence and Exploritation of groundwater in Nigeria Basement Complex. Mining Geology, 20 (3), 131-146.
- Oladapo, M.I., Akintorinwa, O.J., 2007. Hydro geophysical study of Ogbese Southwest, Nigeria. Global Journal Pure Applied Science 13 (1), 55-61.

National Bureau of Statistic, 2020. Republic of Nigeria.

- Loke, M.H., 2000. Electrical Imaging Surveys for Environmental and Engineering Studies 1-67.
- Loke, M.H., 2004. Tutorial for 2-D and 3-D Surveys. Pp 1-136.
- Oomkens, E., 1974. Lithofacies relations in the late quaternary Niger Delta Complex. AAPG Bulletin 24, 195-222.
- Okonkwo, A.C., Ujam, I.I., 2013. Geoelectrical Studies for the delineation of potential groundwater zones at Oduma in Enugu State, Southeastern Nigeria. International Journal of Physical Sciences 8, 1761-1771.
- Rai, S.N., 2017. Mapping and Sustainable Development. American Society of Civil Engineers (ASCE).
- Reyment, R.A., 1965. Aspects of the Geology of Nigeria. Ibadan University Press, Ibadan.
- Short, K.C., Stauble, A.J., 1967. Outline of Geology of Niger Delta. AAPG Bulletin 51, 761-779.
- Todd, D.K., 2004. Groundwater Hydrology, 2nd Edition, John Wiley & Sons, New York.

UNOCHA. 2013. Rainy Season Overview West and Central Africa Rainfall Patterns; United Nations Office for the Coordination of Humanitarian Affairs: Abuja, Nigeria.

Zohdy, A.A.R., 1975. Automatic Interpretation of Schlumberger sounding curves, using modified Dar Zarrouk function. U.S. Geological Survey Bulletin 1313, 1-39.