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ELECTROCHEMICAL HYDROGEN PEROXIDE GENERATION AND REMOVAL OF MOXIFLOXACIN BY ELECTRO-FENTON PROCESS

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Abstract: In this study, the removal of moxifloxacin, an antibiotic of the fluoroquinolone group, from aqueous solutions was investigated using the electro-Fenton process. As the efficiency of the electro-Fenton process is highly dependent on the amount of H_2O_2 produced during process, the formation of H_2O_2 under acidic conditions was also investigated. In this context, the effects of applied current, cathode type and O_2 flow rate on H_2O_2 production were investigated using boron-doped diamond anode. The highest H_2O_2 production was achieved using the boron-doped diamond anode and the graphite felt cathode. In addition, the optimum conditions for the applied current and oxygen flow rate for H_2O_2 production were determined to be 0.25 A and 0.1 L min⁻¹, respectively. The effects of applied current and Fe^{2+} concentration in the electro-Fenton process on the removal of moxifloxacin were investigated. It was found that the moxifloxacin removal rate increased with increasing applied current. The highest H_2O_2 accumulation was observed at 0.25 A applied current, and moxifloxacin removal also reached 93.6% after 60 min. The moxifloxacin removal rate reached the highest value at Fe^{2+} concentration of 0.01 mM. This study provides promising results for the efficient treatment of moxifloxacin-containing wastewater by the electro-Fenton process without the addition of H_2O_2 using boron-doped diamond anode anode and graphite felt cathode.

Keywords: Electro-Fenton, Electro-generated H₂O₂, Moxifloxacin, Boron-doped diamond anode, Graphite felt cathode

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1. Introduction

Antibiotics, which have a wide range of uses, are drugs used in the treatment of infectious diseases caused by microorganisms and improve the quality of life (Kovalakova et al., 2020; Phoon et al., 2020). Considerable quantities (30 to 90 %) of the antibiotics used to enter the waste stream together with their metabolic products without being metabolized in the body (Carvalho and Santos, 2016). It can be found in surface waters and groundwater due to the widespread use of antibiotics and their inadequate removal in conventional wastewater treatment plants (Kümmerer, 2009; Li et al., 2015; Ngigi et al., 2020; Anh et al., 2021). Therefore, the presence of antibiotics in the aquatic environment leads to a disturbance of flora and fauna and risks to human health (Tiwari et al., 2017). Moxifloxacin (MOX), a third-generation fluoroquinolone, belongs to a group of antimicrobial agents with a broad spectrum of activity and increasing consumption (Van Doorslaer et al., 2011). MOX is widely used against both gram-positive and gram-negative bacteria by inhibiting DNA activity and for the treatment of skin infections (Guay, 2006; Nguyen et al., 2023). However, due to its low biodegradability, it is constantly discharged into the natural environment from conventional wastewater treatment plants (Van Doorslaer et al., 2015).

Antibiotics, which have high production and consumption rates, are not easily biodegradable. Therefore, cost-efficient methods are needed to effectively remove antibiotics from wastewater (Shoorangiz et al., 2019). As conventional treatment processes are not sufficient to remove wastewater containing antibiotics, advanced oxidation processes (AOPs) should be preferred to support them or be used as an alternative (Oturan and Aaron, 2014; Ganzenko et al., 2020; Taoufik et al., 2021). AOPs are methods of great interest for the removal of recalcitrant organics and toxic compounds (such as diclofenac and levofloxacin) (Jia et al., 2024; Qiu et al., 2024). AOPs such as Fenton, ozonation, photocatalysis, activated persulfate, and electrochemical processes have been used to remove toxic and/or recalcitrant organic pollutants (Değermenci et al., 2014; Çobanoğlu and Değermenci, 2022; Li et al., 2023). Among AOPs, Fenton oxidation attracts attention due to its simplicity, which does not require special equipment, and its high efficiency in removing organic pollutants (Arnold et al., 1995; Değermenci, 2023). To avoid disadvantages such as potential risks and loss of

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reactive activity during transportation and storage of H_2O_2 used in Fenton oxidation, the electro-Fenton process was developed in combination with Fe²⁺ addition and in situ electro-generated H_2O_2 (Zhou et al., 2007).

The electro-Fenton process is considered an environmentally friendly and promising method for the effective removal of target pollutants from water (Olvera-Vargas et al., 2021; Liu et al., 2022; Yang et al., 2023; de Oliveira Santiago Santos et al., 2023). In the electro-Fenton process, H₂O₂ production is based on the electrochemical reduction of molecular oxygen (O₂) at the cathode (Equation 1) by introducing air or highpurity O2 into the electrolysis cell, and hydroxyl radicals are formed by the electrochemically assisted Fenton reaction (Equation 2) (Brillas et al., 2009). This process, hydrogen peroxide is continuously generated in situ, which allows better control of the oxidation process (Garcia-Segura et al., 2011; Bensalah et al., 2013). The hydroxyl radical and the hydrogen peroxide produced in the process have a strong oxidative potential (E₀=2.80 V and 1.78 V) (Lucas and Peres, 2006). Non-selective radicals hydroxyl are responsible for the oxidation/mineralization of persistent organic substances that are in the same environment (Olvera-Vargas et al., 2021).

$$O_2 + 2H^+ + 2e^- \to H_2O_2$$
 (1)

$$H_2 O_2 + F e^{2+} \to H O^{\bullet} + F e^{3+} + O H^-$$
 (2)

The performance of the electro-Fenton process depends largely on the electrode materials used during electrolysis (Guinea et al., 2010; Bensalah et al., 2013; Midassi et al., 2020). The type of cathode used influences the amount of H_2O_2 produced by the reduction of molecular oxygen (Brillas et al., 2009; Olvera-Vargas et al., 2021). Materials such as carbon brush, carbon felt, stainless steel, carbon sponge etc. were used as cathodes (Sopaj et al., 2020; Olvera-Vargas et al., 2021). Although H_2O_2 production in the electro-Fenton process depends on the cathode type, the structure of the anode material also plays an important role in the overall performance (Sopaj et al., 2016; Yang et al., 2020). Depending on the anode type, heterogeneous hydroxyl radicals are formed on the anode surface by the oxidation of water (Titchou et al., 2021; Yang et al., 2023). The use of different types of anodes such as Pt, Ti/RuO₂-IrO₂, Ti₄O₇, boron doped diamond (BDD), and graphite felt (GF) in the electro-Fenton process has been investigated in the literature (Sopaj et al., 2016; Zwane et al., 2021). This increases the overall efficiency of the electro-Fenton process, as both the cathodic and anodic reactions contribute to the degradation/mineralization of the organic pollutants (Oturan et al., 2012; Olvera-Vargas et al., 2021). The BDD anode is characterized by a high O₂ evolution overvoltage (around 2.2 V vs SHE for BDD). BDD has proven to be the most effective material for the anodic oxidation of refractory organic pollutants (Panizza and Cerisola, 2009; Olvera-Vargas et al., 2021; Oturan, 2021), and the use of BDD as an anode in the electro-Fenton process has been shown to significantly improve the efficiency of the process (Oturan et al., 2012; Ridruejo et al., 2018; Olvera-Vargas et al., 2021).

In the first part of the study, the effects of different operating variables, such as cathode type, O_2 flow rate, and applied current on H_2O_2 accumulation were discussed. In the second part, the removal of MOX by the electro-Fenton process using a BDD anode and a GF cathode was investigated. The effects of current intensity and Fe²⁺ concentration, which are among the parameters affecting the electro-Fenton process, on MOX removal were investigated.

2. Materials and Methods

2.1. Chemicals

All chemicals and reagents used in this study were used without further purification. Moxifloxacin hydrochloride, potassium hydrogen phthalate, potassium iodide, sodium sulfate, hydrogen peroxide, ammonium heptamolybdate tetrahydrate, sodium hydroxide, and sulphuric acid were purchased from the Merck. All solutions were prepared with distilled water at room temperature.

2.2. Experimental Setup

A scheme of the electrochemical cell used is presented in Figure 1.



Figure 1. Schematic diagram of electrochemical cell. BSJ Eng Sci / Gökçe Didar DEĞERMENCİ and Nejdet DEĞERMENCİ

Electrochemical H₂O₂ production and MOX removal by the electro-Fenton process were carried out in an undivided cylindrical glass reactor with a diameter of 7.5 cm and a solution capacity of 400 mL. BDD electrode (DiaCCon GmbH, Germany) was used as an anode for H₂O₂ production and the electro-Fenton process. GF, BDD, stainless steel (SS), and graphite plate (GP) electrodes were used as cathodes. All electrodes are 5 cm × 10 cm in size. The wall thickness is 3 mm for BDD, SS and GP and 12 mm for GF. The temperature of the solution was kept constant at 20°C using a temperaturecontrolled cooling/heated circulator (LABO, C200-H13). Sodium sulfate (Na₂SO₄) was used as a supporting electrolyte to increase the conductivity of the solution. The aqueous solution was stirred continuously at 700 rpm with a magnetic stirrer (IKA, RCT basic). A power supply unit (GW Instek, PSW 80-40.5) was used in all experiments to ensure constant current operation. This device also displayed the cell voltage during the treatments. Without adding a buffer solution, the pH of the solution was adjusted to the desired value only once at the beginning of the experiment with 1 M H₂SO₄. The pH value of the solution was measured using the portable WTW Multi-Parameter meter (Xylem Analytics, MultiLine® Multi 3620 IDS).

2.3. Analytical Procedures

The H_2O_2 and MOX concentration were measured using a UV-Vis spectrophotometer (HachLange, DR 6000). The H_2O_2 concentration was measured at 352 nm by the iodometric method (Klassen et al., 1994). To measure the MOX concentration, a MOX stock solution was prepared and known MOX concentrations were determined by dilution. These solutions were used to create a calibration curve at 290 nm, and the unknown MOX concentrations were measured by prepared calibration curve. The MOX removal efficiency and energy consumption were calculated using Equation 3 and Equation 4, respectively:

 $MOX \ removal, (\%) = (1 - C_t / C_0) \times 100$ (3)

$$W, (kWh m^{-3}) = V \times I \times t/V_S$$
⁽⁴⁾

where C_0 is the initial MOX concentration (mg L⁻¹), C_t is the MOX concentration at given time t (mg L⁻¹), V is mean cell voltage (V), I is electrolysis current (A), t is electrolysis duration (h), and V_S is solution volume (L).

3. Results and Discussion

3.1. Electrochemical H₂O₂ Production

The reactant required for the Fenton reaction to form strong oxidative free radicals is H_2O_2 (Değermenci et al., 2019). The efficiency of the electro-Fenton process depends largely on the amount of H_2O_2 produced in the system (Zhao et al., 2018). In the electro-Fenton process, H_2O_2 can be formed under acidic conditions by the electrochemical reduction of oxygen at the cathode (Equation 1) (Brillas et al., 2009; Midassi et al., 2020). In this context, the effects of current intensity, cathode type, and O_2 flow rate, which are among the parameters affecting electrochemical H_2O_2 production, were examined using the BDD anode.

3.1.1. Effect of cathode type on H₂O₂ production

H₂O₂ production varies depending on the cathode material (Oturan et al., 2021). Therefore, the H₂O₂ production performance of different cathode types using BDD as anode material was investigated. H₂O₂ formation in the experimental system was measured in a solution saturated with O_2 under acidic conditions (pH = 3) and in the absence of pollutants and Fe2+. H2O2 production was monitored for 60 min by continuously supplying O_2 to the cathode; the results are shown in Figure 2. The H₂O₂ production during 60 min electrolysis is 42.7, 28.1, 15.4, and 11.1 mg L⁻¹ for GF, BDD, SS, and GP, respectively. The highest H₂O₂ production was achieved with GF. The H₂O₂ production during 30 min electrolysis is 36.4, 20, 14.1 and 10.0 mg L⁻¹ for GF, BDD, SS and GP, respectively. These results show that the H₂O₂ production rate depends significantly on the cathode type. However, it can be said that the electrochemical reduction of molecular oxygen (Equation 1) occurs faster when GF is used as the cathode. The type of cathode promotes oxygen adsorption and transfer, electron transfer and provides more active sites, thereby promoting the production of H₂O₂ (Feng et al., 2021). Since the highest H₂O₂ production was obtained with GF, it was used as the cathode in the following studies.



Figure 2. Effect of cathode type on the H_2O_2 generation (Conditions: Current intensity= 1 A, Na_2SO_4 = 50 mM, T= 20°C, initial solution pH= 3, and O_2 flow rate= 1 L min⁻¹).

3.1.2. Effect of applied current on H₂O₂ production

The applied current is one of the most important parameters for electrochemical H_2O_2 production (Köktaş and Gökkuş, 2022). The cathodic production of H_2O_2 via the reaction given in Equation 1 drives the production of hydroxyl radicals in the electro-Fenton process via the reaction given in Equation 2. Therefore, the H_2O_2 accumulation in the electrolysis reactor with BDD anode and GF cathode was investigated. Figure 3 shows the H_2O_2 accumulation at different current values during the 60 min electrolysis at an initial solution pH of 3, an electrolyte concentration of 50 mM Na₂SO₄ and an

oxygen flow rate of 1 L min⁻¹. The H₂O₂ concentration is 23.6 mg L⁻¹ after 60 min of electrolysis at a current of 0.05 A. When the current was raised from 0.10 to 0.25 A, the H₂O₂ concentration increased from 53.8 to 95.7 mg L⁻¹. The reason for this increase is that an increase in the applied current supports the oxygen reduction reaction specified in equation 1. However, a further increase in the applied current led to a decrease in H_2O_2 accumulation. H₂O₂ concentration decreased from 66.8 to 42.7 mg L⁻¹ when the current was increased from 0.50 to 1.00 A, respectively. This is because the competitive reactions increase with increasing applied current, which leads to a depletion of H_2O_2 . These are explained by the reduction of H₂O₂ to H₂O at the cathode (Equation 5) and the oxidation of H_2O_2 at the anode (Equation 6). Similar results have been reported regarding the effect of applied current on H₂O₂ production (Zhou et al., 2019; Midassi et al., 2020; Olvera-Vargas et al., 2021). Subsequent experiments were carried out at 0.10 A in order to determine the effect of other operating parameters and for cost effectiveness.

$$H_2O_2 + 2H^+ + 2e^- \to 2H_2O$$
 (5)

$$H_2 O_2 \to O_2 + 2H^+ + 2e^-$$
 (6)



Figure 3. Effect of applied current on the H_2O_2 generation (Conditions: Na₂SO₄= 50 mM, T= 20°C, initial solution pH= 3, and O_2 flow rate= 1 L min⁻¹).

3.1.3. Effect of O_2 flow rate on H_2O_2 production

The O_2 flow rate supplied to the system is one of the parameters that influence electrochemical H_2O_2 production (Midassi et al., 2020). Figure 4 shows the effects of O_2 flow rate on H_2O_2 production when using a BDD anode and a GF cathode. In the experiments, the effect of different O_2 flow rates (0-1 L min⁻¹) on H_2O_2 production was studied for electrolysis time of 60 min. While H_2O_2 production is 14.9 mg L⁻¹ when no gas is added to the reactor, H_2O_2 production increases when O_2 is introduced. At an O_2 flow rate of 0.1 L min⁻¹, H_2O_2 accumulation reached the highest value of 61.3 mg L⁻¹ in 60 min. A further increase in the gas flow rate reduced H_2O_2 production to 53.9 mg L⁻¹ at 0.2 L min⁻¹ and 53.8 mg L⁻¹ at 1.0 L min⁻¹. Increasing the O_2 flow rate can

increase the concentration of dissolved O_2 and promote the mass transfer rate of dissolved O_2 in the solution, which supports electro-generated H_2O_2 production. At flow rates greater than 0.1 L min⁻¹, excessively large bubbles covering the surface of the gas diffusion electrode lead to reduced H_2O_2 production. Similar results regarding the effect of O_2 flow rate on H_2O_2 production have been reported in some studies (Xia et al., 2019; Köktaş and Gökkuş, 2022). A flow rate of 0.1 L min⁻¹ O_2 is sufficient to generate a high H_2O_2 concentration. These results show that adjusting the optimal O_2 flow rate in the system can not only promote H_2O_2 production but also reduce costs (Zhou et al., 2013).



Figure 4. Effect of the O_2 flow rate on the H_2O_2 generation (Conditions: Na₂SO₄= 50 mM, T= 20°C, initial solution pH= 3, and current intensity= 0.10 A).

3.2. Effect of Different Processes on MOX Removal

In the system in which the highest H₂O₂ production was achieved, graphite felt was used as the cathode and BDD as the anode. In the electrolytic cell, MOX can be removed by adsorption and anodic oxidation together with the electro-Fenton process. A comparison of the MOX removals achieved with these treatment methods is shown in Figure 5. In the experiment to determine the amount of MOX adsorbed on the anode and cathode in the electrolytic cell, no current was applied to the cell and O2 and Fe2+ were not supplied. It was determined that the removal of MOX by adsorption was 11.7% in 10 min and 27.5% in 60 min. Then the removal of MOX by anodic oxidation was determined by applying current (0.10 A) to the electrolytic cell without O₂ and Fe²⁺. While MOX removal by anodic oxidation was 30.9% at the 10 min electrolysis, it increased to 87.7% after 60 min. Finally, MOX removal was determined by the electro-Fenton process by adding O2 and Fe2+ to the electrolytic cell at a certain current value (0.10 A). MOX removal by the electro-Fenton process increased from 67.3% in 10 min to 89.0% after 60 min. From these results, it was concluded that the electro-Fenton process is the treatment process with the highest removal rate.



Figure 5. Comparison between electro-Fenton, anodic oxidation and adsorption (Conditions: MOX= 5 mg L⁻¹, Na₂SO₄= 50 mM, initial solution pH= 3, T= 20°C, current intensity= 0.10 A, O₂ flow rate= 0.1 L min⁻¹, Fe²⁺= 0.01mM).

3.2.1. Effect of applied current on MOX removal in the electro-Fenton process

The applied current considerably influences on the electro-Fenton process and is the most important parameter for controlling the reaction rate (Görmez et al., 2022). The effect of the applied current on the removal of MOX by the electro-Fenton process using a GF cathode and a BDD anode is shown in Figure 6. In the electro-Fenton process, MOX removal efficiencies at 60 min electrolysis time were 86.4%, 89.0%, 93.6%, 95.2% and 95.6% at applied currents of 0.05, 0.10, 0.25, 0.50 and 0.75 A, respectively. During the 10 min electrolysis time, MOX removal was 59.6%, 67.3%, 78.5%, 84.6% and 88.5%, respectively, depending on the increasing current value applied. From these results, it can be concluded that the MOX removal rate increases with the increase of the applied current. Comparing these results with H_2O_2 production, the highest H₂O₂ accumulation was obtained at 0.25 A (Figure 3), which does not correspond to the optimum current value for MOX removal. The decreasing H₂O₂ accumulation at high current values does not mean that H_2O_2 production is low. It means that the rate of competitive reactions (Equations 5 and 6) leading to H₂O₂ depletion is high, so the rate of H₂O₂ decomposition is faster than the formation of H₂O₂ (Olvera-Vargas et al., 2021). The H₂O₂ produced in the electrolytic cell reacted with Fe²⁺ via the Fenton reaction (equation 2) before being destroyed via equations 5 and 6. It should be noted that increasing the applied current value increases electrical energy consumption and operating costs.

The change in energy consumption in the experiments conducted at different current values was calculated using equation 4, and the results are shown in Figure 7. As the current value applied to the system increases, the energy consumption increases along with the increase in voltage. The energy consumption for currents of 0.05, 0.10, 0.25, 0.50 and 0.75 A was calculated to be 0.38, 0.86, 2.53, 6.59 and 12.0 kWh m⁻³, at the end of 60 min,

respectively. Increasing the applied current can lead to chemical changes on the electrode surface and shorten the service life of the electrode (GilPavas et al., 2017). However, a further increase in the applied current can have a negative effect on MOX removal due to side reactions (hydrogen evolution and water electrolysis) (Qiu et al., 2024).



Figure 6. Effect of applied current on the MOX removal in the electro-Fenton process (Conditions: MOX= 5 mg L⁻¹, Na₂SO₄= 50 mM, initial solution pH= 3, T= 20°C, O₂ flow rate= 0.1 L min⁻¹, Fe²⁺= 0.01mM).



Figure 7. Variation of energy consumption with applied current (Conditions: MOX= 5 mg L⁻¹, Na₂SO₄= 50 mM, initial solution pH= 3, T= 20°C, O₂ flow rate= 0.1 L min⁻¹, Fe²⁺= 0.01mM).

3.2.2. Effect of Fe²⁺ concentration on MOX removal in the electro-Fenton process

The catalyst concentration is one of the important parameters affecting the removal of pollutants in the electro-Fenton process (Wang et al., 2021; Karatas et al., 2022). The effect of Fe^{2+} concentration on MOX removal is shown in Figure 8. While in the absence of Fe^{2+} ions the MOX removal in 10 min was about 30.9 %, a significant increase in MOX removal was observed with the addition of Fe^{2+} ions. At an electrolysis time of 10 min, the Fe^{2+} concentration for MOX removal increased to 63.4 % at 0.005 mM and to 67.3 % at 0.010 mM. This increase in MOX removal can be explained by the contribution of the generated hydroxyl radicals (Equation 2). Increasing the

Fe²⁺ concentration to 0.020 mM led to a slight decrease in MOX removal. This negative effect of the high Fe²⁺ concentration can be explained by the increased rate of the parasitic reaction (Equation 7) that occurs between hydroxyl radicals and excess Fe²⁺ (Özdemir et al., 2011; Xia et al., 2019).

$$Fe^{2+} + HO^{\bullet} \to Fe^{3+} + OH^{-} \tag{7}$$



Figure 8. Effect of Fe²⁺ concentration on MOX removal in the electro-Fenton process (Conditions: MOX= 5 mg L⁻¹, Na₂SO₄= 50 mM, initial solution pH= 3, T= 20°C, current intensity= 0.10 A, O₂ flow rate= 0.1 L min⁻¹).

4. Conclusion

In this study, electrochemical H₂O₂ production and MOX removal were successfully performed with a BDD anode. It was found that the electrochemical H₂O₂ production rate was significantly dependent on the cathode type. H₂O₂ production increased with the use of a GF cathode, it was also observed that the applied current and oxygen flow rate also had significant effects on H_2O_2 production. The effects of applied current and Fe2+ concentration on MOX removal in the electro-Fenton process were investigated. It was found that the MOX removal rate in the process with BDD anode and GF cathode increased with the increase of the applied current. However, it was found that increasing current was accompanied by a corresponding increase in energy consumption due to the increased voltage. From the findings, it was concluded that the electro-Fenton process could be an effective method for reducing antibiotic contamination in wastewater.

Author Contributions

The percentage of the author(s) contributions is presented below. The author reviewed and approved the final version of the manuscript.

	G.D.D.	N.D.
С	70	30
D	70	30
S	100	
DCP	50	50
DAI	50	50
L	80	20
W	100	
CR	80	20
SR	100	
РМ	80	20
FA	100	

C=Concept, D= design, S= supervision, DCP= data collection and/or processing, DAI= data analysis and/or interpretation, L= literature search, W= writing, CR= critical review, SR= submission and revision, PM= project management, FA= funding acquisition.

Conflict of Interest

The author declared that there is no conflict of interest.

Ethical Consideration

Ethics committee approval was not required for this study because of there was no study on animals or humans.

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