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## Effect of ZrO<sub>2</sub> on Radiation Permeability Properties of Polypropylene

Zübeyde ÖZKAN<sup>1,2\*</sup> Berkay ÇAKIR<sup>3</sup> Seda Gürgen AVŞAR<sup>3</sup> Emir OLÇAY<sup>3</sup> Uğur GÖKMEN<sup>3</sup><sup>1</sup> Gazi University, Institute of Science and Technology, Ankara, Türkiye<sup>2</sup> Gazi University, Institute of Science and Technology, Department of Advanced Technologies, Ankara, Türkiye<sup>3</sup> Gazi University, Institute of Science and Technology, Department of Metallurgical and Materials Engineering, Ankara, Türkiye

Keywords	Abstract
Polypropylene (PP) ZrO <sub>2</sub> Gamma Shielding Neutron Composite	The study investigates the radiation permeability properties including mass attenuation coefficient (MAC), linear attenuation coefficient (LAC), tenth value layer (TVL), half value layer (HVL), fast neutron cross section (FNRC), and mean free path (MFP) of polypropylene (PP) polymer, as well as the produced polymer matrix composites (PP+5% ZrO <sub>2</sub> , PP+10% ZrO <sub>2</sub> , PP+15% ZrO <sub>2</sub> ). The studied materials were examined by considering their effect on radiation permeability against gamma and neutron radiation. Additionally, powder size, Archimedes principle (density), XRD, DSC, ATR, and DTA-TG analyses were performed. According to the radiation permeability results of the studied four materials, PP + 15% ZrO <sub>2</sub> was found to have the highest LAC values, while PP was found to have the lowest LAC values. The FNRC values of the PP, PP+5% ZrO <sub>2</sub> , PP+10% ZrO <sub>2</sub> , and PP+15% ZrO <sub>2</sub> materials were found to be 10.038 cm <sup>-1</sup> , 12.651 cm <sup>-1</sup> , 15.002 cm <sup>-1</sup> , and 17.091 cm <sup>-1</sup> , respectively. The most suitable material for gamma and neutron shielding was found to be 15% ZrO <sub>2</sub> reinforced material.

### Cite

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Author ID (ORCID Number)	Article Process
0000-0003-2901-7749	Zübeyde ÖZKAN
0009-0001-5500-9438	Berkay ÇAKIR
0009-0008-9991-7236	Seda Gürgen AVŞAR
0009-0009-5257-6929	Emir OLÇAY
0000-0002-6903-0297	Uğur GÖKMEN
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## 1. INTRODUCTION

With the development of technology, energy demand has been rising with each passing day because of the increase in consumption. Thanks to nuclear power plants, it is possible to generate power in any quantity and at any time in line with demand. Therefore, the number of nuclear power plants has been increasing rapidly across the world. Nuclear power plants, like everything else, have several advantages, as well as some disadvantages. Any leak or explosion causes irreversible damage that will affect nature and human health for many years. As a result of radiation spreading to the environment, it affects not only the immediate surroundings of the nuclear power plant but also areas kilometers away from the power plant. As a result of the Chernobyl disaster that occurred on April 26, 1986, Bulgaria, Türkiye, Romania, etc. they were affected by radioactive substances spread throughout the countries. Therefore, radiation shielding is crucial for nuclear power plants (Akman et al., 2022; Szondy et al., 2024). Having a short wavelength, gamma rays emit high-frequency electromagnetic radiation. Since they are uncharged, neutron particles are not affected by Coulomb forces and do not interact with the nucleus. As a result of this, they have a higher penetration depth. Any leak in a nuclear power plant might pose severe health risks for living beings. It might result in hair loss, cataracts, gene damage, cancer, and even mortality in living beings (Tyagi et al., 2021; Ardiansyah et al., 2023; Aldawood et al., 2024). As a result, radiation shielding material is very important for human health and nature. Recently, Alzahrani et al. (2022), Malidarre et al. (2021), Kamislioglu (2021), and several

other researchers have carried out many studies on materials to offer an alternative radiation shielding material that can eliminate the negative aspects of the shielding material currently used.

In this study, recyclable polypropylene (PP) material was used among polymer materials used for different purposes. In this way, as a result of the recycling of materials that have completed their intended use, their usability as gamma and fast neutron shielding material, which is a new field, has been investigated. Polymer matrix composite materials designed by adding ZrO<sub>2</sub> ceramic material at varying rates of 5-10-15% into the PP polymer matrix; the linear attenuation coefficient (LAC), mass attenuation coefficient (MAC), half value thickness (HVL), tenth value thickness (TVL), mean free distance (MFP) and fast neutron cross section (FNRC) parameters were examined and the radiation transmittance results against gamma and neutron radiations were analyzed. In addition, density, XRD, ATR, DSC and DTA-TG analyses of the PP material and SEM-EDS analyses of the ZrO<sub>2</sub> ceramic material, which provide information on powder grain size analysis and microstructural properties, were carried out.

## 2. MATERIALS AND METHOD

The powder size of the ZrO<sub>2</sub> ceramic powder used was dimensional utilizing Malvern Mastersizer 3000, which is a laser diffraction particle size analyzer. In addition, the microstructure of the material was examined under the SEM microscope to understand the powder grain shape, which is important in determining the production parameters. Then the XRD analyses of the PP were performed. Table 1 shows the chemical composition of the studied materials in the radiation permeability analysis. The melting point and vaporization temperature are crucial parameters in terms of radiation shielding. This is because the degradation of the radiation shielding material's chemical structure is very important for its resistance against radiation. Therefore, ATR, DSC, and DTA-TG analyses were performed on the studied PP polymer materials.

*Table 1. Chemical composition of the materials*

Name of the sample	Composition
S0	PP
S5	PP+5% ZrO <sub>2</sub>
S10	PP+10% ZrO <sub>2</sub>
S15	PP+15% ZrO <sub>2</sub>

The gamma and neutron permeability analyses of polymer composites were performed by employing Phy-x/PSD (Şakar et al., 2020). The LAC and MAC which provide significant details about the material's shielding feature against radiation, are very prominent in the selection of shielding material. LAC ( $\mu$ ), which is the fraction of attenuated radiation in an energy beam per unit thickness of material, is obtained by utilising the Beer-Lambert law (Equation 1). MAC, on the other hand, is obtained by taking into account the density of the material in absorbing the incoming radiation. It is a measure of the possible interaction between photon and matter. The MAC value is given by divide the LAC value by the material intensity, as shown in Equation 2, where  $I_0$ ,  $I$ , and  $x$  are the intensity of the radiation on the material, the intensity of the radiation passing through the material and the thickness of the material (cm), respectively

$$I = I_0 e^{-\mu x} \quad (1)$$

$$\mu_m = \frac{\mu}{\rho} \quad (2)$$

HVL, MFP and TVL are very important parameters as they are utilizing to specify the thick of the radiation shielding material to be used. HVL indicates the thickness at which the shielding material decreases the incident radiation by half the intensity, while TVL indicates the thickness at which it reduces the incident radiation by 90% in centimeters. The mean distance traveled between two successive collisions by an incoming photon is specified by MFP. These parameters are calculated using Equations 3-4-5. FNRC is significant in terms of the absorption of fast neutrons. FNRC is calculated in centimeters by employing Eq. 6 (Kılıçoğlu & Tekin, 2020; Kavun et al., 2022).

$$HVL = \frac{\ln(2)}{\mu} \quad (3)$$

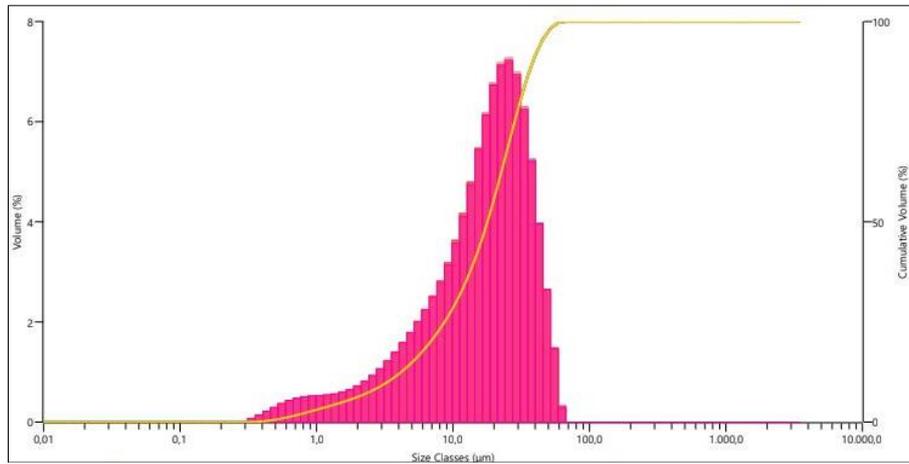
$$TVL = \frac{\ln(10)}{\mu} \quad (4)$$

$$MFP = \frac{1}{\mu} \quad (5)$$

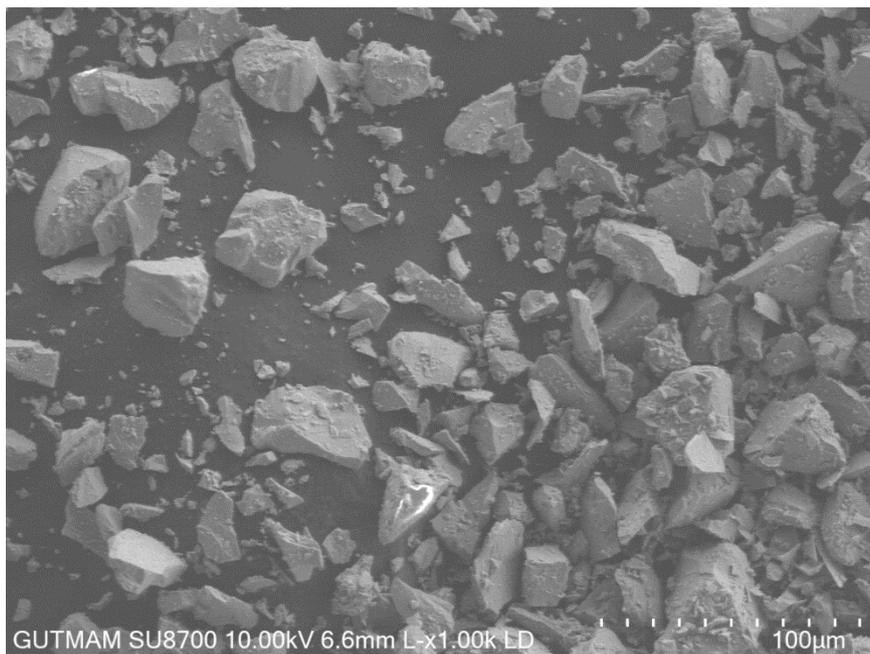
$$\sum_R = \sum_i \rho_i (\sum R/\rho)_i \quad (6)$$

### 3. RESULTS AND DISCUSSION

The average density of the studied PP, which was measured by Archimedes' principle, was found to be approximately 0.77 g/cm<sup>3</sup>. Figure 1 shows the powder grain size distribution of the ZrO<sub>2</sub> ceramic powder used in the study. Dv (90), Dv (50), and Dv (10) values of the ZrO<sub>2</sub> ceramic powder were found to be 38.6 µm, 18.0 µm, and 3.46 µm, respectively. In Figure 2, it can be seen that the ZrO<sub>2</sub> ceramic powder has an angular shape at x1000 magnification. When the SEM image is examined, Dv (90), Dv (50) and Dv (10) differences in the powder grain size distribution are seen.



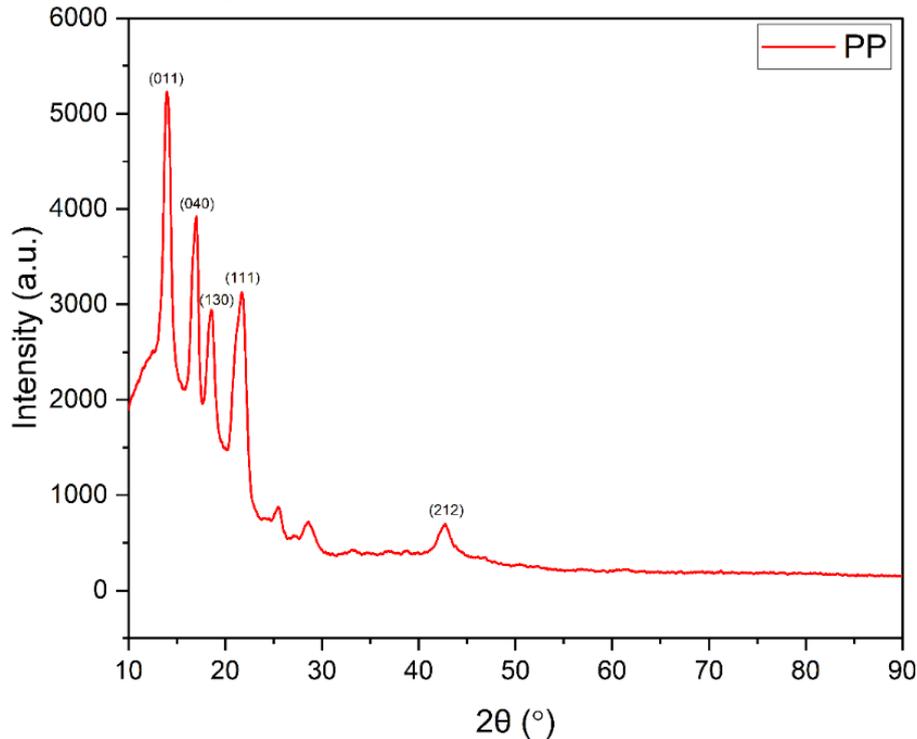
**Figure 1.** Grain size distribution of the ZrO<sub>2</sub> ceramic powder



**Figure 2.** SEM of the ZrO<sub>2</sub> ceramic powder

Figure 3 presents the XRD analysis of PP, as well as the characteristic peaks with (hkl) Miller indices of the material. XRD analyzes of PP material were analyzed at  $2\theta^\circ$  between  $10^\circ$ - $90^\circ$ . At  $2\theta^\circ$ , the PP material gives peaks of (011), (040), (130), (111), and (060) to the crystal planes at about  $14.3^\circ$ ,  $17.2^\circ$ ,  $18.7^\circ$ ,  $21.3^\circ$ , and  $25.5^\circ$ , respectively. The peaks of the XRD spectrum curve are also consistent with those of PP reported in the literature (Akinci et al., 2007; Mingliang et al., 2007). In addition, the crystallinity rate of the studied material was found by measuring the ratio of the entire area under the curve (Figure 3) to the crystal peak areas, using the equation given in Equation 7, and was calculated as 82.24%.

$$\%Crystallinity = \frac{A_{crystal}}{A_{curve}} \times 100 \quad (7)$$



**Figure 3.** XRD spectrum of the polypropylene

Isotactic PP, a widely used commercial polymer, may have a simple chemical composition, but its self-assembly behavior and crystal structures are surprisingly complex. The type of polymer significantly affects semi-crystalline polymers' properties, including crystal thicknesses and crystallinity levels. The morphology of crystals is also greatly affected by thermo-mechanical processes (Labour et al., 2001; Akinci et al., 2007). In polymeric materials, the crystallization rate and amorphous regions change the material's thermal, physical, and mechanical characteristics (Akinci et al., 2007). Pure PP can usually be obtained in the following crystal shapes;  $\alpha$  (monoclinic) $\gamma$  (orthorhombic), and  $\beta$  (trigonal) as well as smectic mesophase, an intermediate state between amorphous and ordered phases. As it is the most stable state in terms of thermodynamic conditions,  $\alpha$  state is the most commonly used form of PP in industry. Also, the melting point of isotactic polypropylene (iPP) is around  $160$ – $165^\circ\text{C}$ , which is relatively higher than other variations (Papageorgiou et al., 2012).

In Figure 4, the DSC spectrum of polypropylene was analyzed between  $25^\circ\text{C}$  -  $250^\circ\text{C}$  with increasing temperature at  $10^\circ\text{C}$  per minute. Multiple endothermic peaks occur at  $136^\circ\text{C}$  and  $168^\circ\text{C}$ , depending on the process involved in various fusion transitions. The main peak is observed at  $168^\circ\text{C}$ . Recrystallization or rearrangement of some crystallized fractions are the primary reasons for these multiple endothermic reactions (Cho et al., 1999). According to the TGA and DSC analysis results, it is observed that the melting point varies between  $168^\circ\text{C}$  and  $172^\circ\text{C}$ . In Figure 5, the DTA spectrum of polypropylene was analyzed between  $25^\circ\text{C}$  -  $600^\circ\text{C}$  with increasing temperature at  $10^\circ\text{C}$  per five minutes. Additionally, thermal decomposition of PP material begins around  $453^\circ\text{C}$ .

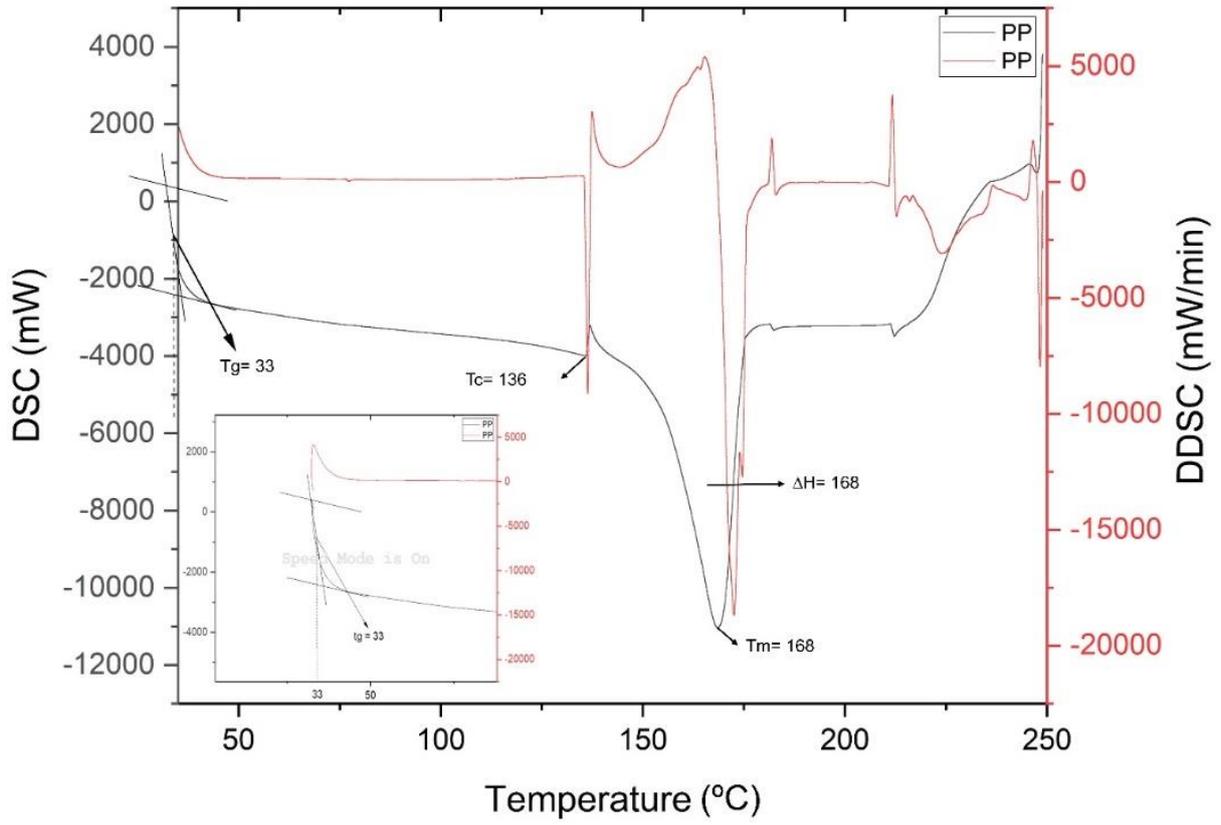


Figure 4. DSC analysis of polypropylene

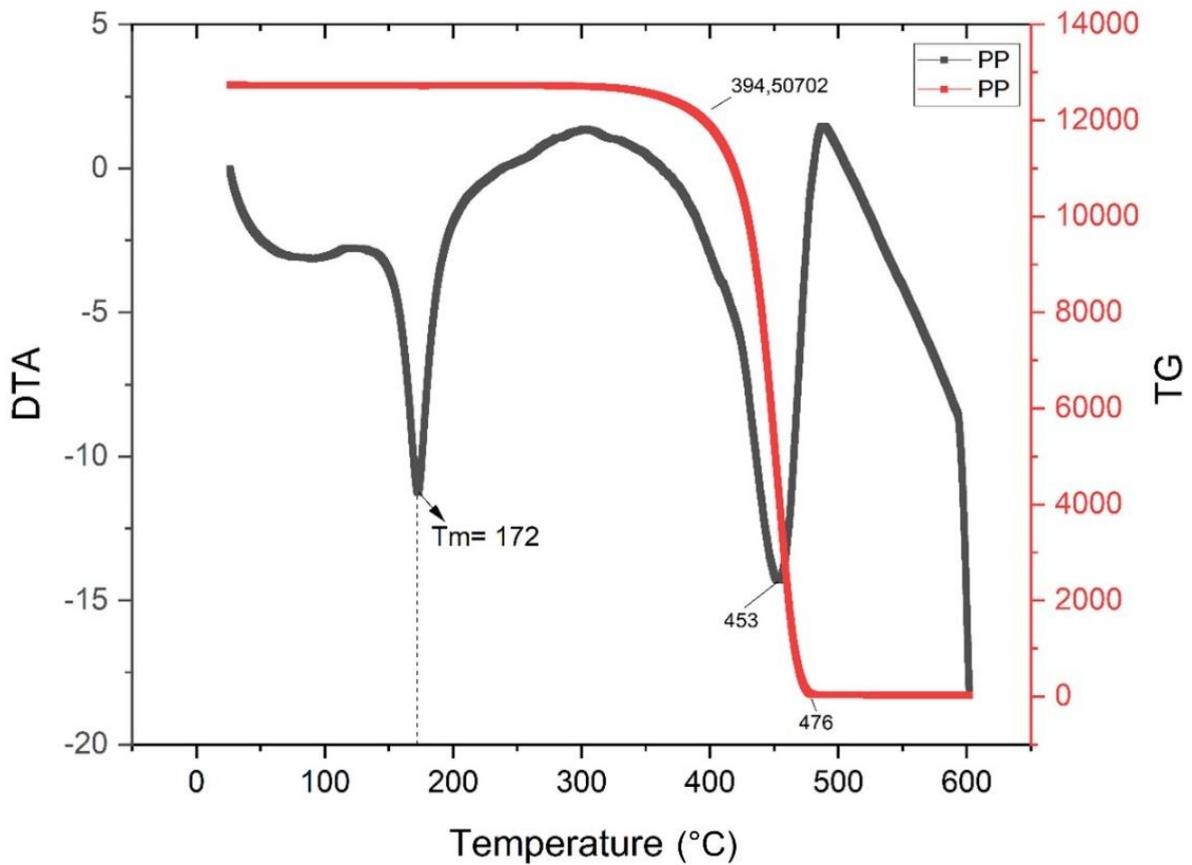
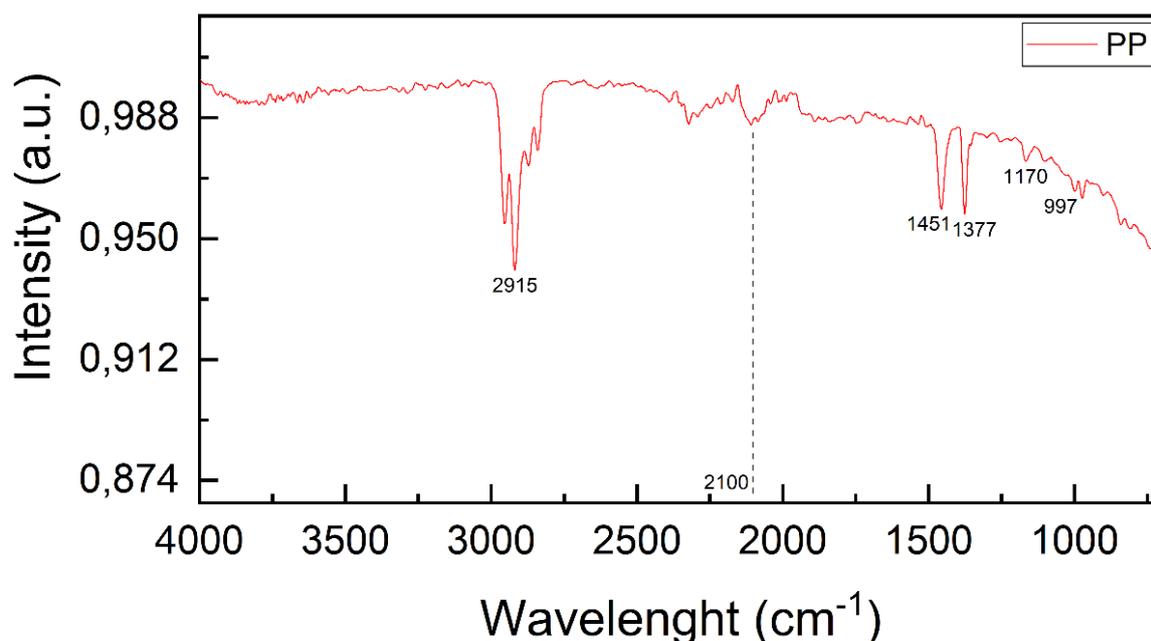


Figure 5. DTA-TGA analysis of polypropylene

ATR analysis PP material was analyzed at wavelengths of  $550\text{ cm}^{-1}$ – $4000\text{ cm}^{-1}$ . Figure 6 shows the spectrum of the PP material and the absorption peaks, which are consistent with those reported by the previous studies. In the isotactic polypropylene spectrum, the methylene group arises between the range from  $1445\text{ cm}^{-1}$  to  $1485\text{ cm}^{-1}$  while the methyl group originates between  $430\text{ cm}^{-1}$  and  $1470\text{ cm}^{-1}$  or between  $1365\text{ cm}^{-1}$  and  $1395\text{ cm}^{-1}$ . In spectrum, such peaks show  $1451\text{ cm}^{-1}$  and  $1377\text{ cm}^{-1}$ , respectively. The peak around  $2915\text{ cm}^{-1}$  was linked to CH band vibration. The pure PP spectrum also contains characteristic peaks at  $840$ ,  $1000$ , and  $1170\text{ cm}^{-1}$ . These characteristic curves are observed at  $1170$ ,  $997$ , and  $840\text{ cm}^{-1}$ ; however, they are not clearly detachable owing to the smoothing process (Krylova & Dukštienė, 2013).



*Figure 6. ATR spectrum of polypropylene*

According to the LAC values (Figure 7), all studied samples have lower LAC figures with the increase in energy. It is observed that the radiation absorption abilities of materials are higher in the low energy range. The addition of 5%  $\text{ZrO}_2$  in PP leads to a two-fold rise in the LAC worth of the PP polymer material. This is mainly because the  $\text{ZrO}_2$  material is a high-density ceramic and contains elements with much higher atomic numbers compared to PP. The sample's LAC value increases depending on the increase in the proportion of the  $\text{ZrO}_2$  addition. The photoelectric effect (PE) occurs dominantly in the of  $0.005888\text{ MeV} < E < 0.511\text{ MeV}$ . In this energy region, the PP, PP+5%  $\text{ZrO}_2$ , PP+10%  $\text{ZrO}_2$ , and PP+15%  $\text{ZrO}_2$  materials exhibit the following ranges of the LAC values:  $777.564\text{ cm}^{-1}$ – $7.764\text{ cm}^{-1}$ ,  $2179.104\text{ cm}^{-1}$ – $10.025\text{ cm}^{-1}$ ,  $4134.525\text{ cm}^{-1}$ – $12.344\text{ cm}^{-1}$ , and  $6643.827\text{ cm}^{-1}$ – $14.633\text{ cm}^{-1}$ , respectively. At the energy of  $0.662\text{ MeV}$  ( $^{137}\text{Cs}$ ), where Compton scattering (CS) is predominant, PP, PP+5%  $\text{ZrO}_2$ , PP+10%  $\text{ZrO}_2$ , and PP+15%  $\text{ZrO}_2$  materials get LAC values of  $6.859\text{ cm}^{-1}$ ,  $8.947\text{ cm}^{-1}$ ,  $11.001\text{ cm}^{-1}$ , and  $13.021\text{ cm}^{-1}$ , respectively. The studied polymer composites' LAC values are observed to get higher figures with the increase in the proportion of the  $\text{ZrO}_2$  addition.

Figure 8 reveals that the MAC and LAC curves of the materials exhibit similar behaviors. While the variation in the studied materials' MAC values is more evident in the low photon energy regions, the variation in the samples' MAC values is closer to each other in the high photon energy region. This is because the materials have more interaction with photons and, accordingly, the absorption amount is higher at lower photon energies. In other words, it is due to the weaker ability of materials to absorb photons at high photon energies. For the energy level of  $0.723\text{ MeV}$  ( $^{131}\text{I}$ ), where CS is dominant, PP, PP+5%  $\text{ZrO}_2$ , PP+10%  $\text{ZrO}_2$  and PP+15%  $\text{ZrO}_2$  materials have the MAC values of  $8.464\text{ cm}^2/\text{g}$ ,  $8.395\text{ cm}^2/\text{g}$ ,  $8.326\text{ cm}^2/\text{g}$ , and  $8.256\text{ cm}^2/\text{g}$ , respectively. MAC values of the materials show well stability in the energy region after  $2\text{ MeV}$ , where pair production predominantly occurs. At a photon energy of  $2\text{ MeV}$ , the MAC values of PP, PP+5%  $\text{ZrO}_2$ , PP+10%  $\text{ZrO}_2$ , and PP+15%  $\text{ZrO}_2$  materials are  $5.064\text{ cm}^2/\text{g}$ ,  $5.023\text{ cm}^2/\text{g}$ ,  $4.981\text{ cm}^2/\text{g}$ , and  $4.939\text{ cm}^2/\text{g}$ , respectively.

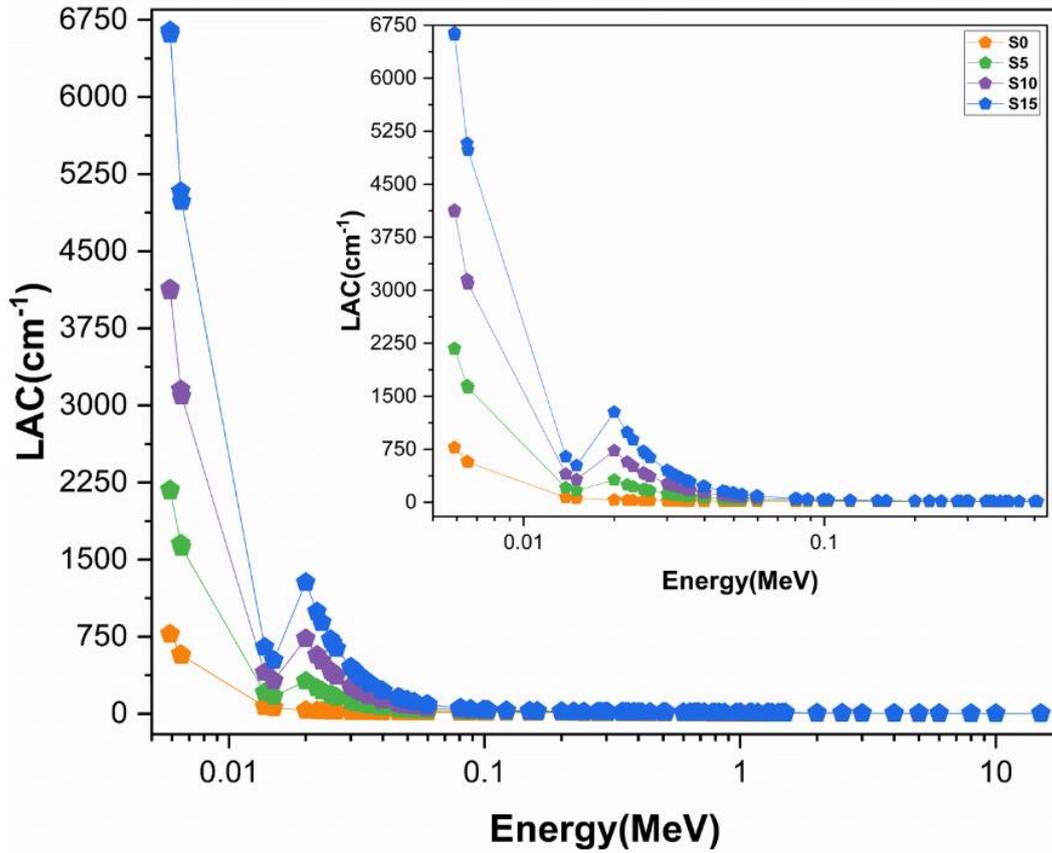


Figure 7. LAC values of the samples

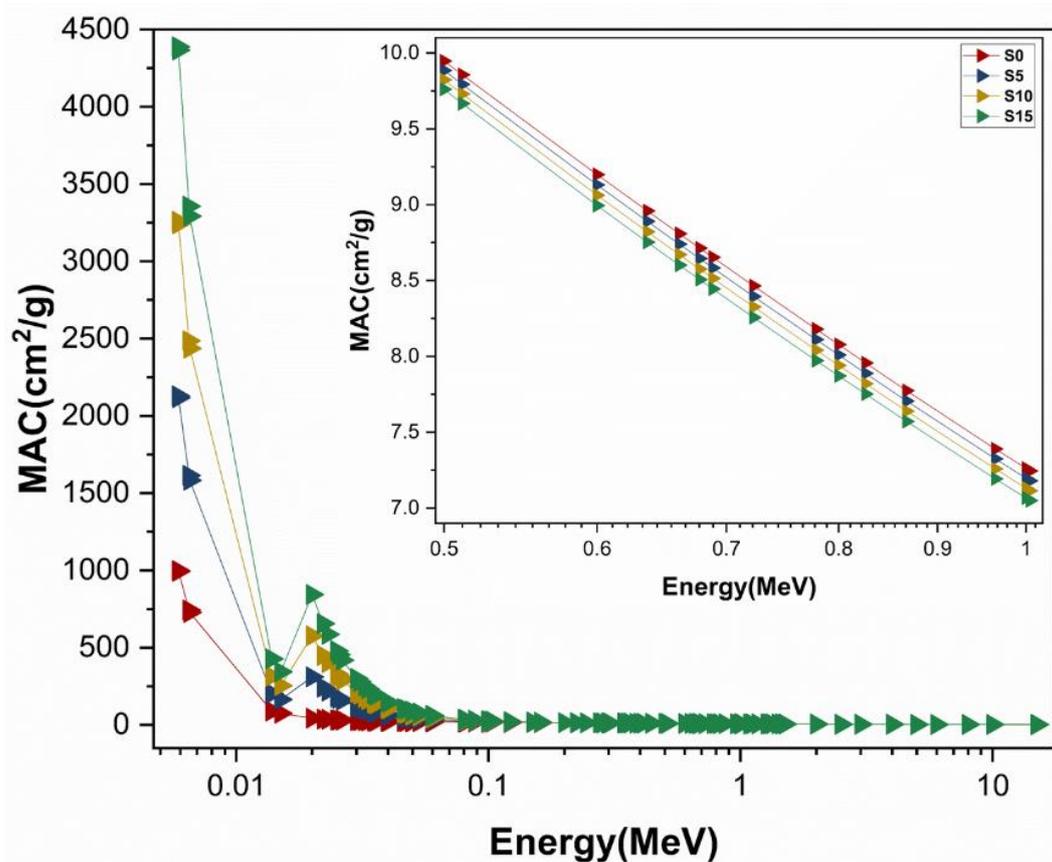


Figure 8. MAC values of the samples

Considering the HVL plot of the studied materials, the HVL values get lower figures due to the higher absorption of the materials at low energies (Figure 9). The HVL values of the PP, PP+5% ZrO<sub>2</sub>, PP+10% ZrO<sub>2</sub>, and PP+15% ZrO<sub>2</sub> samples range from 0.0001 cm to 0.09 cm in the energy range of 0.005888-0.511 MeV, where the PE occurs predominantly. On the other hand, Compton scattering occurs predominantly between the energy levels 0.511-1.02 MeV, where HVL gets a value between 0.047 cm and 0.123 cm. Finally, pair production occurs predominantly in the high energy zone, where HVL values range from 0.123 cm to 0.489 cm. The relationship between the material thickness required to halve the incoming photon power and the incoming photon energy is clearly seen from these HVL values. Figure 8 shows that the material thickness required by the S15 sample, which is produced by adding 15% ZrO<sub>2</sub> ceramic material into the PP, to absorb the same photon energy is reduced to approximately half, even in the high energy region.

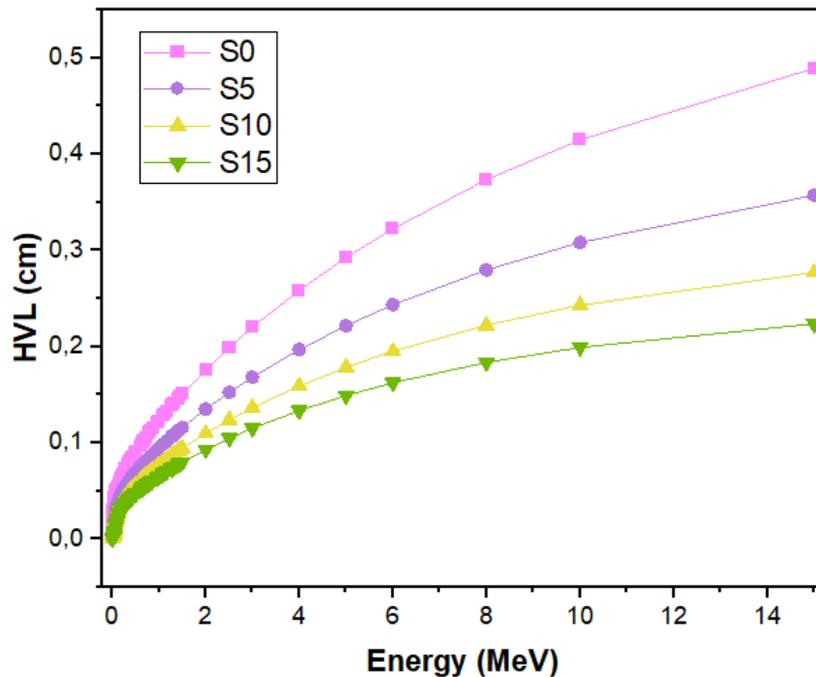


Figure 9. HVL value of the samples

Figure 10 shows the TVL plot, which indicates the material thick necessary to reduce the incoming radiation intensity by 90%. In this figure, it is plainly observed that the thickness values of the studied materials should be higher than their HVL values. The <sup>60</sup>Co source, which is widely used in industry, is a radioactive gamma radiation source. This gamma radiation source has various photopeaks in the energy regions where Compton scattering, PE, and pair production are predominant. When the energy level is 0.3471 MeV, the PE is dominant, and the PP, PP+5% ZrO<sub>2</sub>, PP+10% ZrO<sub>2</sub>, and PP+15% ZrO<sub>2</sub> samples have TVL values of 0.257 cm, 0.196 cm, 0.158 cm, and 0.133 cm, respectively. When the energy level is 0.8261 MeV, the Compton scattering is dominant, and the studied samples get values of 0.372 cm, 0.285 cm, 0.232 cm, and 0.196 cm, respectively. On the other hand, pair production is dominant at the energy level of 1.173 MeV, and these values are observed to be 0.441 cm, 0.338 cm, 0.276 cm, and 0.233 cm, respectively. This analysis results reveal the addition's effect on the radiation shielding material's thickness with the increase in the photon energy emitted from a radioactive source, even if the gamma sources are the same.

Figure 11 shows that the material thick required for successful two-photon interaction increases with the increase in photon energy. It is evident that the increase in ZrO<sub>2</sub> ceramic addition in the studied materials results in decreases in their MFP values. It is because the atomic number and density of the ZrO<sub>2</sub> ceramic are higher than those of the PP material. Therefore, the increase in the ZrO<sub>2</sub> addition results in a large number of electrons' interactions with photons. After 2 MeV, the MFP values of all the studied samples increase rapidly. This is because the LAC values of these materials become more stable after 2 MeV, and the absorption of high-energy photons decreases considerably. At the energy range 2-15 MeV, the materials PP, PP+5% ZrO<sub>2</sub>, PP+10% ZrO<sub>2</sub> and PP+15% ZrO<sub>2</sub> have MFP ranges of 0.254 cm- 0.706 cm; 0.194 cm- 0.515 cm; 0.158 cm- 0.4 cm and 0.134 cm- 0.323 cm respectively.

FNRC is a significant in terms of indicating the shielding performance of a designed material against fast neutrons. The FNRC values of the PP, PP+5% ZrO<sub>2</sub>, PP+10% ZrO<sub>2</sub>, and PP+15% ZrO<sub>2</sub> materials are 10.038 cm<sup>-1</sup>, 12.651 cm<sup>-1</sup>, 15.002 cm<sup>-1</sup>, and 17.091 cm<sup>-1</sup>, respectively. Among the four samples, the PP material has the lowest FNRC value, while the PP+15% ZrO<sub>2</sub> polymer matrix has the highest value (Figure 12). The density value of the PP+15% ZrO<sub>2</sub> polymer composite is about 95% higher than that of the PP material. Also, the FNRC value of the PP+15% ZrO<sub>2</sub> polymer matrix is about 70% higher than that of the PP material. The increase in the ZrO<sub>2</sub> ceramics addition to the PP material leads to more neutron interaction of nuclei; as a result, the FNRC values get higher figures.

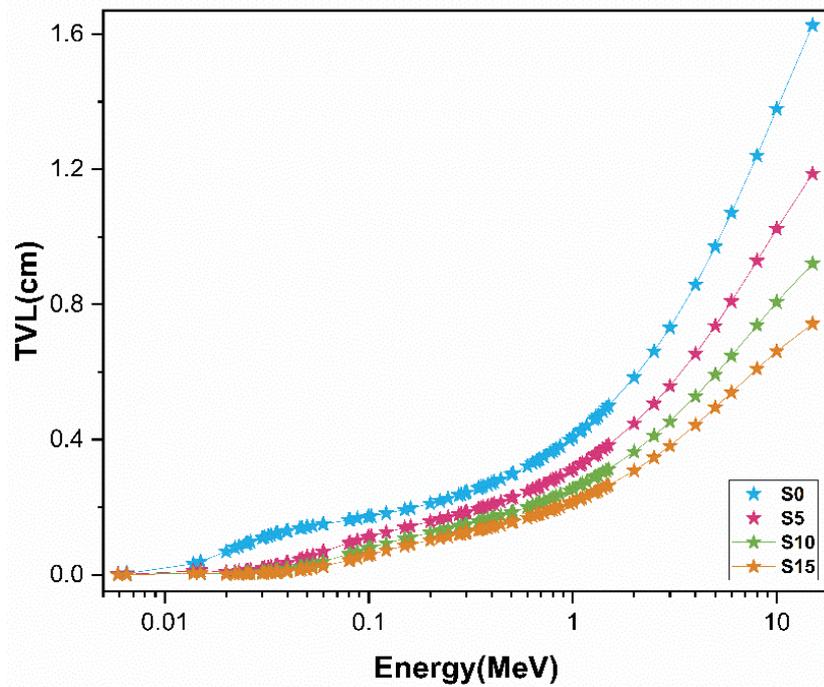


Figure 10. TVL value of the samples

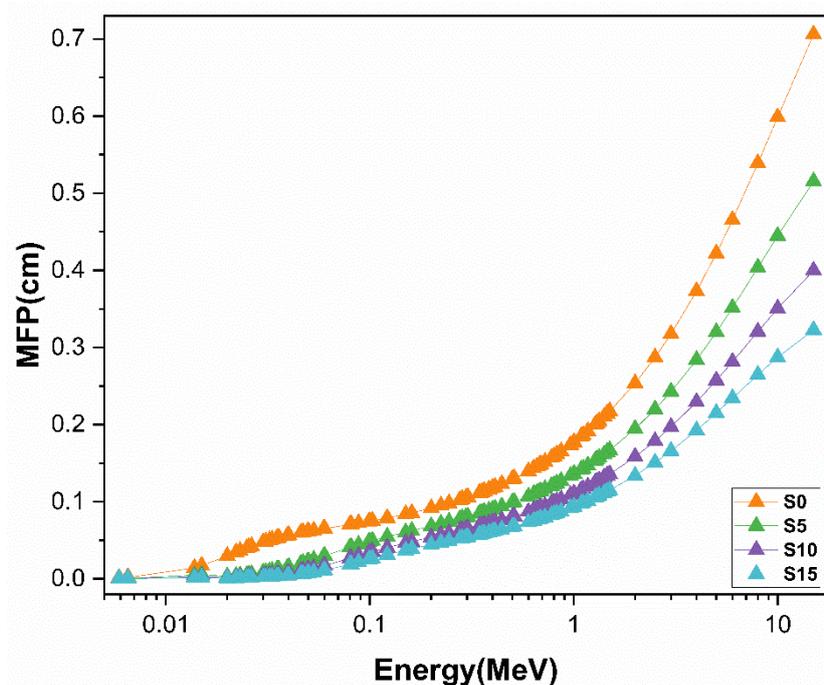
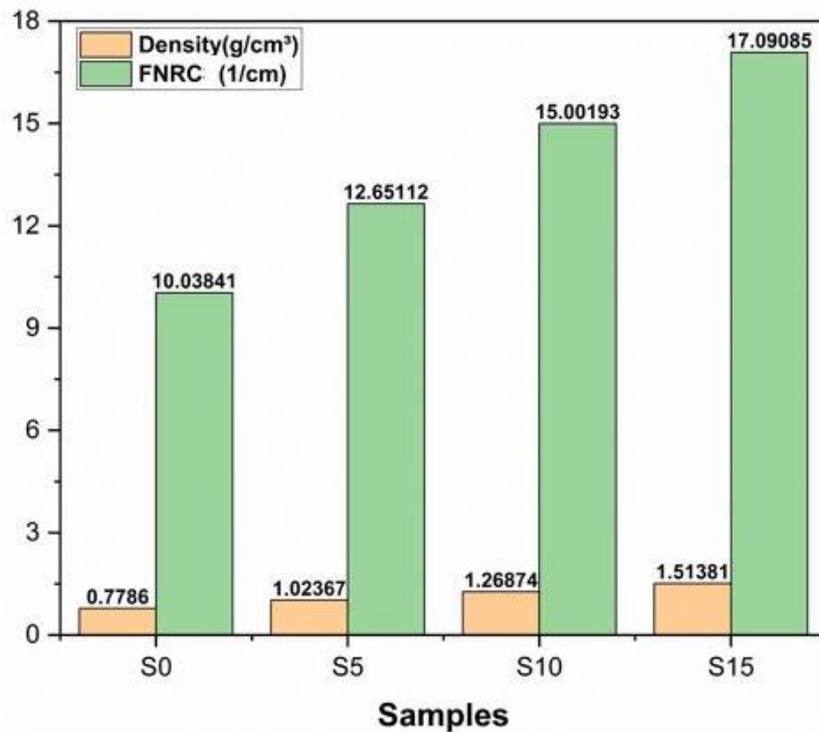


Figure 11. MFP value of the samples



*Figure 12. FNRC and density values of the samples*

#### 4. CONCLUSION

This study examined the radiation shielding performance of polypropylene and polymer matrix composites produced by adding ZrO<sub>2</sub> ceramic powder in varying proportions (5%, 10%, and 15%) to the PP material. The LAC, MAC, HVL, TVL, MFP, and FNRC, which provide significant information about gamma and neutron radiations, were analysed by utilizing the Phy-x/PSD software. Grain size and microstructures of ZrO<sub>2</sub> ceramic material were analyzed by SEM. Moreover, the XRD, ATR, DSC, and DTA-TG analyses were performed to obtain information about the density and characteristic properties of the PP material. Among the studied PP, PP+5% ZrO<sub>2</sub>, PP+10% ZrO<sub>2</sub> and PP+15% ZrO<sub>2</sub> samples, PP+10% ZrO<sub>2</sub> had the highest LAC value while PP had the lowest LAC value. The samples with higher LAC values had lower HVL values. Therefore, the material with the highest HVL value is PP while the material with the lowest HVL value is PP+15% ZrO<sub>2</sub>. As for the FNRC values, PP material has the lowest value (10.038 cm<sup>-1</sup>) while the PP+15%ZrO<sub>2</sub> polymer matrix composite has the highest FNCR value (17.091 cm<sup>-1</sup>). To conclude, the neutron and gamma radiation shielding features of the PP material were improved by increasing the ZrO<sub>2</sub> ceramic addition.

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#### AUTHOR CONTRIBUTIONS

Conceptualization, U.G. and Z.Ö.; methodology, U.G.; fieldwork, Z.Ö, S.G.A., B.Ç and E.O.; software, Z.Ö, B.Ç and E.O.; title, U.G. and Z.Ö.; validation, U.G., Z.Ö. and S.G.A.; laboratory work, Z.Ö, S.G.A., B.Ç and E.O.; formal analysis, U.G.; research, Z.Ö, S.G.A. and B.Ç; sources, Z.Ö and B.Ç.; data curation, Z.Ö and B.Ç.; manuscript-original draft, U.G. and Z.Ö.; manuscript-review and editing, U.G and Z.Ö; visualization, S.G.A, B.Ç and Z.Ö.; supervision, U.G; project management, U.G; funding, Gazi BAP. All authors have read and legally accepted the final version of the article published in the journal.

## CONFLICT OF INTEREST

The authors declare no conflict of interest.

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