# Review and classifications of the ridge parameter estimation techniques

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#### Abstract

Ridge parameter estimation techniques under the influence of multicollinearity in Linear regression model were reviewed and classified into different forms and various types. The different forms are Fixed Maximum (FM), Varying Maximum (VM), Arithmetic Mean (AM), Geometric Mean (GM), Harmonic Mean (HM) and Median (M) and the various types are Original (O), Reciprocal (R), Square Root (SR) and Reciprocal of Square Root (RSR). These classifications resulted into proposing some other techniques of Ridge parameter estimation. Investigation of the existing and proposed ones were done by conducting 1000 Monte-Carlo experiments under five (5) levels of multicollinearity ( $\rho=0.8,0.9,0.95,0.99,0.999)$ , three (3) levels of error variance ( $\sigma^2=0.25,1,25$ ) and five levels of sample size (n=10,20,30,40,50). The relative efficiency ( $RF\leq0.75$ ) of the techniques resulting from the ratio of their mean square error and that of the ordinary least square was used to compare the techniques.

Results show that the proposed techniques perform better than the existing ones in some situations; and that the best technique is generally the ridge parameter in the form of Harmonic Mean, Fixed Maximum and Varying Maximum in their Original and Square Root types.

**Keywords:** Linear Regression Model, Multicollinearity, Ridge Parameter Estimation Techniques, Relative Efficiency.

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#### 1. Introduction

Regression analysis is a study on relationship among variables often classified as dependent and independent variables. The dependent variable is modeled on one or more explanatory variables. The aim is often to estimate the mean value of the dependent variable in terms of the known or fixed value of the explanatory variables. The Ordinary Least Squares (OLS) estimator is the most popularly used estimator to estimate the parameters in a regression model. The estimator under certain assumptions has some very attractive statistical properties which have made it one of the most powerful estimators. One of the assumptions is that the explanatory variables are independent. However, in practice, there may be strong or perfect linear relationships among the explanatory variables. This problem is often referred to as multicollinearity problem. It is well known that the performance of OLS estimator is unsatisfactory in the presence of multicollinearity in that the regression coefficients possess large standard errors and some will even have the wrong sign (Gujarati, 1995). In literature, there are various methods existing to solve this problem. Among them is the ridge regression estimator first introduced by Hoerl and Kennard (1970). Ridge estimator has a smaller mean square error (MSE) than OLS estimator (Vinod and Ullah, 1981).

Consider the standard regression model:

$$(1.1) Y = X\beta + U$$

where X is an  $n \times p$  matrix with full rank, Y is a  $n \times 1$  vector of dependent variable,  $\beta$  is a  $p \times 1$  vector of unknown parameters, and U is the error term such that E(U) = 0 and  $E(UU') = \sigma^2 I_n$ .

The ridge estimator is defined as:

$$(1.2) \qquad \hat{\beta} = \left(X'X + KI\right)^{-1} X'Y$$

where K is a non-negative constant. It is called biasing or ridge parameter. It is observed that when K=0, (2) returns OLS estimates. Ridge regression estimators are biased as K increases but give more precise estimates than OLS estimator (Mardikyan and Cetin, 2008). Hoerl et al. (1975) suggested that the value of K should be chosen small enough such that the mean squared error of ridge estimator is less than the mean squared error of OLS estimator. Different techniques of estimation had been proposed or suggested by various researchers. Hoerl and Kennard (1970) suggested a graphical method called ridge trace to select the value of the ridge parameter K. This is a plot of the values of individual components of  $\hat{\beta}_k$  against a range of values of K (0 < K < 1). The minimum value for which  $\hat{\beta}_k$  become stable and the wrong signs in the regression coefficient is corrected is used. Also, one can select the value of K for which the residual sum of square is not too large. The performance of the Ridge estimator with different Ks had often been compared through simulation study. Most of the researchers have generated data from a normal population as explanatory variables with different number of regressors. The mean squared error (MSE) has been used severally as a performance criterion.

Several techniques had been developed to estimate K. These were reviewed and classified into different forms and various types in this paper. These classifications resulted into proposing new techniques for the ridge parameter estimation. The organization of this paper is as follows: Theoretical background of ridge regression, different methods of estimations are reviewed and proposed estimators are presented in section 2. The model, details of the Monte Carlo simulation study and performance criterion is given in Section 3. Results and discussions are presented in section 4. Some concluding remarks are given in Section 5.

## 2. Ridge regression and ridge estimator

**2.1.** Background of ridge regression. Ridge regression centers on the use of the biased parameter K which yields estimation with a smaller mean square error. Hoerl and Kennard (1970) suggested the optimum ridge parameter as:

(2.1) 
$$K_i = \frac{\sigma^2}{\sigma_i^2}, i = 1, 2, 3, \dots, p$$

Since  $\sigma^2$  and  $\alpha_i^2$  are generally unknown and the  $K_i$  needs to be estimated. Consequently, they suggested the replacement of  $\sigma^2$  and  $\alpha_i^2$  by their corresponding unbiased estimators  $\hat{\sigma}^2$  and  $\hat{\alpha}_i^2$ .

Therefore, the estimator of  $K_i$  is given as:

$$(2.2) K_i = \frac{\sigma^2}{\sigma_i^2}$$

where  $\hat{\sigma}^2 = \frac{\sum_{i=1}^n e_i^2}{n-p}$  and  $\alpha_i$  is the  $i^{th}$  element of the vector  $\hat{\alpha} = Q'\hat{\beta}$  where Q is an orthogonal matrix.

- **2.2.** Review of methods of estimating the ridge parameter. The existing ridge parameters are reviewed as follows:
- **2.2.1.** Estimators based on Hoerl and Kennard (1970). Hoerl and Kennard (1970) proposed  $K_{HK_i} = \frac{\sigma^2}{\alpha_i^2}$ . They suggested estimating ridge parameter by taking the maximum (Fixed Maximum) of  $\alpha_i^2$  such that the estimator of K is:

$$\hat{K}_{HK}^{FM} = \frac{\hat{\sigma}^2}{Max(\hat{\alpha}_i^2)}$$

Hoerl et al. (1975) proposed a different estimator of K by taking the Harmonic Mean of the ridge parameter  $K_{HK_i}$ . This estimator is given as:

(2.4) 
$$\hat{K}_{HK}^{FM} = \frac{P\hat{\sigma}^2}{\sum_{i=1}^{p} \alpha_i^2}$$

Kibria (2003) proposed some new estimators of K by taking the Geometric Mean, Arithmetic Mean and Median ( $p \geq 3$ ) of the ridge parameter  $K_{HK_i}$ . These estimators are respectively defined as:

(2.5) 
$$\hat{K}_{HK}^{GM} = \frac{\hat{\alpha}^2}{(\prod_{i=1}^p \hat{\alpha}_i^2)^{\frac{1}{p}}}$$

$$(2.6) \qquad \hat{K}^{AM}_{HK} = \frac{1}{p} \sum_{i=1}^{p} (\frac{\hat{\alpha}^2}{\hat{\alpha}_i^2})$$

$$\hat{K}_{HK}^{M} = Median(\frac{\hat{\alpha}^{2}}{\hat{\alpha}_{i}^{2}})$$

Furthermore, Muniz and Kibria (2009) proposed some estimators of K in form of Square root of Geometric Mean of  $K_{HK_i}$  and its reciprocal, the Median of the Square root of  $K_{HK_i}$  and its reciprocal, and Varying Maximum of the Square root of  $K_{HK_i}$  and its reciprocal. These estimators are respectively defined as:

(2.8) 
$$\hat{K}_{HK}^{GMSR} = \sqrt{\frac{\hat{\sigma}^2}{(\prod_{i=1}^p \hat{\alpha}_i^2)^{\frac{1}{p}}}}$$

$$(2.9) \qquad \hat{K}_{HK}^{GMRSR} = \frac{1}{\sqrt{\frac{\hat{\sigma}^{2}}{(\prod_{i=1}^{p} \hat{\alpha}_{i}^{2})^{\frac{1}{p}}}}}$$

$$(2.10) \quad \hat{K}^{MSR}_{HK} = Median(\sqrt{\frac{\hat{\alpha}^2}{\hat{\alpha}_i^2}})$$

$$(2.11) \quad \hat{K}_{HK}^{MRSR} = Median(\frac{1}{\sqrt{\frac{\hat{\alpha}^2}{\hat{\alpha}_i^2}}})$$

$$(2.12) \quad \hat{K}^{MRSR}_{HK} = Max(\sqrt{\frac{\hat{\alpha}^2}{\hat{\alpha}_i^2}})$$

$$(2.13) \quad \hat{K}^{MRSR}_{HK} = Max(\frac{1}{\sqrt{\frac{\hat{\alpha}^2}{\hat{\alpha}_i^2}}})$$

**2.2.2.** Estimators based on Lawless and Wang (1976). Lawless and Wang (1976) proposed a different estimator of K resulting from taking the Harmonic Mean of the ridge parameter  $K_{LW_i} = \frac{\sigma^2}{\lambda_i \alpha_i^2}$ . The estimator is defined as:

$$(2.14) \quad \hat{K}_{LW}^{HM} = \frac{p\hat{\sigma}^2}{\sum_{i=1}^p \lambda_i \hat{\alpha}_i^2}$$

where  $\lambda_i$  is the eigenvalue of the matrix X'X.

**2.2.3.** Estimators based on Alkhamisi et al. (2006). Alkhamisi et al. (2006) proposed another ridge parameter  $K_{AKS_i} = \frac{\sigma^2 \lambda_i}{(n-p)\sigma^2 + \lambda_i \alpha_i^2}$ . They proposed estimators of K as the Arithmetic Mean and Median of the ridge parameter  $K_{AKS_i}$ . These estimators are respectively defined as:

(2.15) 
$$\hat{K}_{AKS}^{AM} = \frac{1}{p} \sum_{i=1}^{p} (\frac{\lambda_i \hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + \lambda_i \hat{\alpha}_i^2})$$

(2.16) 
$$\hat{K}_{AKS}^{M} = Median(\frac{\hat{\sigma}^{2}\lambda_{i}}{(n-p)\sigma^{2} + \lambda_{i}\hat{\alpha}_{i}^{2}})$$

However, a new approach of choosing the ridge parameter K suggested by Khalaf and Shukur (2005) can be seen in form of Fixed Maximum of the ridge parameter  $K_{AKS_i}$ . The estimator is defined as:

$$(2.17) \quad \hat{K}_{AKS}^{FM} = \frac{\hat{\sigma}^2 max(\lambda_i)}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)Max(\hat{\alpha}_i^2)}$$

Muniz and Kibria (2009) proposed the estimator of the ridge parameter K as the Geometric Mean of the ridge parameter  $K_{AKS_i}$ . The estimator is given as:

(2.18) 
$$\hat{K}_{AKS}^{GMO} = (\prod_{i=1}^{p} \frac{\lambda_i \hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + \lambda_i \hat{\alpha}_i^2})^{\frac{1}{p}}$$

Muniz et al. (2012) proposed the estimator of the ridge parameter K as the Varying Maximum and Arithmetic Mean of the ridge parameter  $K_{AKS_i}$ . These estimators are defined respectively as:

$$(2.19) \quad \hat{K}_{AKS}^{VMO} = Max(\frac{\lambda_i \hat{\alpha}^2}{(n-p)\hat{\alpha}^2 + \lambda_i \hat{\alpha}_i^2})$$

$$(2.20) \quad \hat{K}_{AKS}^{AMO} = \frac{1}{p} \sum_{i=1}^{p} (\frac{\lambda_i \hat{\alpha}^2}{(n-p)\hat{\alpha}^2 + \lambda_i \hat{\alpha}_i^2})$$

2.2.4. Estimators based on Muniz et al. (2012). Muniz et al. (2012) proposed another ridge parameter  $K_{MAOi} = \frac{\hat{\sigma}^2 Max(\lambda_i)}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\alpha_i^2}$ . They proposed estimators of K as Varying Maximum of  $K_{MAO_s}$  and its reciprocal, its square root and reciprocal of its square root, Median of the reciprocal of  $K_{MAO_i}$ , Median of the reciprocal of the square root of  $K_{MAO_i}$ , and the Geometric Mean of  $K_{MAO_i}$ , its square root and reciprocal of its square root. These estimators are defined respectively as:

$$(2.21) \quad K_{MAOi} = Max(\frac{\hat{\sigma}^2 Max(\lambda_i)}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\alpha_i^2})$$

$$(2.22) \quad \hat{K}^{VMR}_{MAO} = Max(\frac{1}{\hat{K}_{MAO}})$$

$$(2.23) \quad \hat{K}_{MAO}^{VMSR} = Max(\sqrt{\hat{K}}_{MAO})$$

$$(2.24) \quad \hat{K}_{MAO}^{VMRSR} = Max(\frac{1}{\sqrt{\hat{K}_{MAO}}})$$

$$(2.25) \quad \hat{K}^{MR}_{MAO} = Median(\frac{1}{\hat{K}_{MAO}})$$

$$(2.25) \quad \hat{K}_{MAO}^{MR} = Median(\frac{1}{\hat{K}_{MAO}})$$

$$(2.26) \quad \hat{K}_{MAO}^{MRSR} = Median(\frac{1}{\sqrt{\hat{K}_{MAO}}})$$

(2.27) 
$$K_{MAOi} = (\prod_{i=1}^{p} \frac{Max(\lambda_i)\hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\alpha_i^2})^{\frac{1}{p}}$$

$$(2.28) \quad \hat{K}_{MAO}^{GMSR} = \sqrt{\hat{K}_{MAO}^{GMO}}$$

$$\begin{array}{ll} (2.28) & \hat{K}_{MAO}^{GMSR} = \sqrt{\hat{K}_{MAO}^{GMO}} \\ (2.29) & \hat{K}_{MAO}^{GMRSR} = \frac{1}{\sqrt{\hat{K}_{MAO}^{GMO}}} \end{array}$$

It should be noted that the Fixed Maximum of  $K_{MAO_i}$  gives the ridge parameter proposed by Khalaf and Shukur (2005) already defined in (19).

2.3. Summary of the existing and proposed ridge parameters. Following the review in section 2.2, it is observed that the parameters follow some different forms and various types. These are explained and summarized as follows:

#### A. Different forms of K

- 1. Fixed Maximum (FM): This is obtained by taking the highest value of the estimated regression coefficient or the eigenvalue or both.
- 2. Varying Maximum (VM): This allows the estimated regression coefficient and the eigenvalue to vary, and eventually the maximum of the estimated ridge parameter is chosen. That is, the ridge parameter with the highest estimated ridge parameters or eigenvalues or both.
- 3. Arithmetic Mean (AM): It involves taking the average of the estimated ridge parameters.
- 4. Harmonic Mean (HM): The ridge parameter is expressed as Harmonic Mean of the estimated ridge parameters.
- 5. Geometric Mean (GM): The ridge parameter is expressed as the Geometric Mean of the estimated ridge parameters.
- 6. Median (M): This involves taking the Median of the estimated ridge parameters.

#### B. Various types of K

- 1. Original form(O)
- 2. Reciprocal form(R)
- 3. Square root form(SR)

		Varie	ous types of K	
Different Forms	0	R	SR	RSR
FM	$\hat{K}^{FMO}_{HK} = \frac{\hat{\sigma}^2}{Max(\hat{\alpha}_i^2)}$	$\hat{K}_{HK}^{FMR} = \frac{1}{\hat{K}_{HK}^{FMO}}$	$\hat{K}_{HK}^{FMSR} = \sqrt{\hat{K}_{HK}^{FMO}}$	$\hat{K}_{HK}^{FMRSR} = \frac{1}{\sqrt{\hat{K}_{HK}^{FMO}}}$
	Hoerl et al. (1970)	proposed	proposed	proposed
VM	$\hat{K}_{HK}^{VMO} = Max(\frac{\hat{\sigma}^2}{\hat{\alpha}_i^2})$	$\hat{K}_{HK}^{VMR} = Max(\frac{1}{(\frac{\hat{\sigma}^2}{\hat{\alpha}_i^2})})$	$\hat{K}_{HK}^{VMSR} = Max(\sqrt{\frac{\hat{\sigma}^2}{\hat{\alpha}_i^2}})$	$\hat{K}_{HK}^{VMRSR} = Max(\frac{1}{\sqrt{\frac{\hat{\sigma}^2}{\hat{\alpha}_i^2}}})$
	Proposed	Proposed	Proposed	Proposed
AM	$\hat{K}_{HK}^{AMO} = \frac{1}{p} \sum_{i=1}^{p} \frac{\hat{\sigma}^2}{\hat{\alpha}_i^2}$	$\hat{K}_{HK}^{AMR} = \frac{1}{\hat{K}_{HK}^{AMO}}$	$\hat{K}_{HK}^{AMSR} = \sqrt{\hat{K}_{HK}^{AMO}}$	$\hat{K}_{HK}^{AMRSR} = \frac{1}{\sqrt{\hat{K}_{HK}^{AMO}}}$
	Proposed	Proposed	Proposed	Proposed
HM	$\hat{K}_{HK}^{HMO} = \frac{p\hat{\sigma}^2}{\sum_{i=1}^p \hat{\alpha}_i^2}$	$\hat{K}_{HK}^{HMR} = \frac{1}{\hat{K}_{HK}^{HMO}}$	$\hat{K}_{HK}^{HMSR} = \sqrt{\hat{K}_{HK}^{HMO}}$	$\hat{K}_{HK}^{HMRSR} = \frac{1}{\sqrt{\hat{K}_{HK}^{HMO}}}$
	Hoerl et al. (1975)	Proposed	Proposed	Proposed
GM	$\hat{K}_{HK}^{GMO} = \frac{\hat{\sigma}^2}{(\prod_{i=1}^{p} \hat{\alpha}_i^2)^{\frac{1}{p}}}$	$\hat{K}_{HK}^{GMR} = \frac{1}{\hat{K}_{HK}^{GMO}}$	$\hat{K}_{HK}^{GMSR} = \sqrt{\hat{K}_{HK}^{GMO}}$	$\hat{K}_{HK}^{GMRSR} = \frac{1}{\sqrt{\hat{K}_{HK}^{GMO}}}$
	Kibria (2003)	Proposed	Proposed	Proposed
M	$\hat{K}_{HK}^{MO} = Median(\frac{\hat{\sigma}^2}{\hat{\alpha}_i^2})$	$\hat{K}_{HK}^{MR} = Median(\frac{1}{(\frac{\hat{\sigma}^2}{\hat{\alpha}_i^2})})$	$\hat{K}_{HK}^{MSR} = Median(\sqrt{(\frac{\hat{\sigma}^2}{\hat{\alpha}_i^2})})$	$\hat{K}_{HK}^{MRSR} = Median(\frac{1}{\sqrt{(\frac{\hat{\sigma}^2}{\hat{\alpha}_i^2})}})$
	Kibria (2003)	Proposed	Proposed	Muniz and Kibria (2009)

**Table 1.** Summary of Different Forms and Various Types for  $\hat{K}_{HK_i} = \frac{\hat{\sigma}^2}{\hat{\alpha}_i^2}$ 

#### 4. Reciprocal of Square root(RSR)

In the light of this knowledge, the existing and newly proposed ridge parameters are summarized based on the previous works as follows:

**2.3.1.** Ridge Parameter Proposed by Hoerl and Kennard (1970). Hoerl and Kennard (1970) proposed the ridge parameter  $K_{HK_i} = \frac{\sigma^2}{\alpha_i^2}$ . Its estimator in the light of different forms and various types are summarized in Table 1.

Table 1 gives the summary of the different forms and various types of the Hoerl and Kennard (1970) ridge parameter. Those already in existence and the proposed ones are specified.

**2.3.2.** Ridge Parameter Proposed by Lawless and Wang (1976). Lawless and Wang (1976) proposed ridge parameter resulting from the Harmonic Mean of  $K_{LW_i} = \frac{\sigma^2}{\lambda_i \alpha_i^2}$ . Its estimator in the light of different forms and various types are summarized in Table 2.

Table 2 gives the summary of the different forms and various types of the Lawless and Wang (1976) ridge parameter. The one already in existence and the proposed are specified.

**2.3.3.** Ridge Parameter Proposed by Alkhamisi et al. (2006). Alkhamisi et al. (2006) proposed the ridge parameter  $K_{AKS_i} = \frac{\sigma^2 \lambda_i}{(n-p)\sigma^2 + \lambda_i \alpha_i^2}$ . Its estimator in the light of different forms and various types are summarized in Table 3.

Table 3 gives the summary of the different forms and various types of the Alkhamisi et al (2006) ridge parameter. Those already in existence and the proposed ones are also specified.

**2.3.4.** Ridge Parameter Proposed by Muniz et al. (2012). Muniz et al.(2012) proposed the ridge parameter  $K_{MAO_i} = \frac{\hat{\sigma}^2 Max(\lambda_i)}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\alpha_i^2}$ . Its estimator in the light of different forms and various types are summarized in Table 4.

Table 4 gives the summary of the different forms and various types of the Muniz *et al.* (2012) ridge parameter. Those already in existence and the proposed are specified.

**Table 2.** Summary of Different Forms and Various Types for  $\hat{K}_{LW_i} = \frac{\hat{\sigma}^2}{\lambda_i \hat{\alpha}_i^2}$ 

		Variou	s types of K	
Different Forms	О	R	SR	RSR
FM	$\hat{K}_{LW}^{FMO} = \frac{\hat{\sigma}^2}{Max(\lambda_i)Max(\hat{\alpha}_i^2)}$	$\hat{K}_{LW}^{FMR} = \frac{1}{\hat{K}_{LW}^{FMO}}$	$\hat{K}_{LW}^{FMSR} = \sqrt{\hat{K}_{LW}^{FMO}}$	$\hat{K}_{LW}^{FMRSR} = \frac{1}{\sqrt{\hat{K}_{LW}^{FMO}}}$
	Proposed	proposed	proposed	proposed
VM	$\hat{K}_{LW}^{VMO} = Max[\frac{\hat{\sigma}^2}{\lambda_i \hat{\alpha}_i^2}]$	$\hat{K}_{LW}^{VMR} = Max(\frac{1}{\hat{K}_{LW}})$	$\hat{K}_{LW}^{VMSR} = Max(\sqrt{\hat{K}_{LW}})$	$\hat{K}_{LW}^{VMRSR} = Max(\frac{1}{\sqrt{\hat{K}_{LW}}})$
	Proposed	Proposed	Proposed	Proposed
AM	$\hat{K}_{LW}^{AMO} = \frac{1}{p} \sum_{i=1}^{p} \frac{\hat{\sigma}^2}{\lambda_i \hat{\alpha}_i^2}$	$\hat{K}_{LW}^{AMR} = \frac{1}{\hat{K}_{LW}^{AMO}}$	$\hat{K}_{LW}^{AMSR} = \sqrt{\hat{K}_{LW}^{AMO}}$	$\hat{K}_{LW}^{AMRSR} = \frac{1}{\sqrt{\hat{K}_{LW}^{AMO}}}$
	Proposed	Proposed	Proposed	Proposed
HM	$\hat{K}_{LW}^{HMO} = \frac{p\hat{\sigma}^2}{\sum_{i=1}^p \lambda_i \hat{\alpha}_i^2}$	$\hat{K}_{LW}^{HMR} = \frac{1}{\hat{K}_{LW}^{HMO}}$	$\hat{K}_{LW}^{HMSR} = \sqrt{\hat{K}_{LW}^{HMO}}$	$\hat{K}_{LW}^{HMRSR} = \frac{1}{\sqrt{\hat{K}_{LW}^{HMO}}}$
	Lawless and Wang (1976)	Proposed	Proposed	Proposed
GM	$\hat{K}_{LW}^{GMO} = \frac{\hat{\sigma}^2}{(\prod_{i=1}^p \lambda_i \hat{\alpha}_i^2)^{\frac{1}{p}}}$	$\hat{K}_{LW}^{GMR} = \frac{1}{\hat{K}_{LW}^{GMO}}$	$\hat{K}_{LW}^{GMSR} = \sqrt{\hat{K}_{LW}^{GMO}}$	$\hat{K}_{LW}^{GMRSR} = \frac{1}{\sqrt{\hat{K}_{LW}^{GMO}}}$
	Proposed	Proposed	Proposed	Proposed
M	$\hat{K}_{LW}^{MO} = Median(\frac{\hat{\sigma}^2}{\lambda_i \hat{\alpha}_i^2})$	$\hat{K}_{LW}^{MR} = Median(\frac{1}{\hat{K}_{LW}})$	$\hat{K}_{LW}^{MSR} = Median(\sqrt{\hat{K}_{LW}})$	$\hat{K}_{LW}^{MRSR} = Median(\frac{1}{\sqrt{\hat{K}_{LW}}})$
	Proposed	Proposed	Proposed	Proposed

**Table 3.** Summary of Different Forms and Various Types for  $\hat{K}_{AKS_i}=\frac{\sigma^2\lambda_i}{(n-p)\sigma^2+\lambda_i\alpha_i^2}$ 

		Various ty	pes of K	
Different Forms	О	R	SR	RSR
FM	$\hat{K}_{AKS}^{FM} = \frac{\hat{\sigma}^2 Max(\lambda_i)}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)Max(\hat{\alpha}_i^2)}$	$\hat{K}_{AKS}^{FMR} = \frac{1}{\hat{K}_{AKS}^{FMO}}$	$\hat{K}_{AKS}^{FMSR} = \sqrt{\hat{K}_{AKS}^{FMO}}$	$\hat{K}_{AKS}^{FMRSR} = \frac{1}{\sqrt{\hat{K}_{AKS}^{FMO}}}$
	Khalaf and Shukur (2005)	proposed	proposed	propose d
VM	$\hat{K}_{AKS}^{VMO} = Max(\frac{\lambda_i \hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + \lambda_i \hat{\alpha}_i^2})$	$\hat{K}_{AKS}^{VMR} = Max(\frac{1}{\hat{K}_{AKS}})$	$\hat{K}_{AKS}^{VMSR} = Max(\sqrt{\hat{K}_{AKS}})$	$\hat{K}_{AKS}^{VMRSR} = Max(\frac{1}{\sqrt{\hat{K}_{AKS}}})$
	Muniz et al. (2012)	Proposed	Proposed	Propose d
AM	$\hat{K}_{AKS}^{AMO} = \frac{1}{p} \sum_{i=1}^{p} \left( \frac{\lambda_i \hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + \lambda_i \hat{\alpha}_i^2} \right)$	$\hat{K}_{AKS}^{AMR} = \frac{1}{\hat{K}_{AKS}^{AMO}}$	$\hat{K}_{AKS}^{AMSR} = \sqrt{\hat{K}_{AKS}^{AMO}}$	$\hat{K}_{AKS}^{AMRSR} = \frac{1}{\sqrt{\hat{K}_{AKS}^{AMO}}}$
	Muniz et al. (2012)	Propose d	Propose d	Proposed
HM	$\hat{K}_{AKS}^{HMO} = p \sum_{i=1}^{p} \left( \frac{\lambda_i \hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + \lambda_i \hat{\alpha}_i^2} \right)$	$\hat{K}_{AKS}^{HMR} = \frac{1}{\hat{K}_{AKS}^{HMO}}$	$\hat{K}_{AKS}^{HMSR} = \sqrt{\hat{K}_{AKS}^{HMO}}$	$\hat{K}_{AKS}^{HMRSR} = \frac{1}{\sqrt{\hat{K}_{AKS}^{HMO}}}$
	Lawless and Wang (1976)	Proposed	Proposed	Proposed
GM	$\hat{K}_{AKS}^{GMO} = \left(\prod_{i=1}^{p} \frac{\lambda_i \hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + \lambda_i \hat{\alpha}_i^2}\right)^{\frac{1}{p}}$	$\hat{K}_{AKS}^{GMR} = \frac{1}{\hat{K}_{AKS}^{GMO}}$	$\hat{K}_{AKS}^{GMSR} = \sqrt{\hat{K}_{AKS}^{GMO}}$	$\hat{K}_{AKS}^{GMRSR} = \frac{1}{\sqrt{\hat{K}_{AKS}^{GMO}}}$
	Muniz and Kibria (2009)	Propose d	Proposed	Proposed
М	$\hat{K}_{AKS}^{MO} = \left(\frac{\lambda_i \hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + \lambda_i \hat{\alpha}_i^2}\right)$	$\hat{K}_{AKS}^{MR} = Median(\frac{1}{\hat{K}_{AKS}})$	$\hat{K}_{AKS}^{MSR} = Median(\sqrt{\hat{K}_{AKS}})$	$\hat{K}_{AKS}^{MRSR} = Median(\frac{1}{\sqrt{\hat{K}_{AKS}}})$
	Alkhamisi et al.(2006)	Proposed	Propose d	Proposed

**Table 4.** Summary of Different Forms and Various Types for  $K_{MAO_i}=\frac{\hat{\sigma}^2Max(\lambda_i)}{(n-p)\hat{\sigma}^2+Max(\lambda_i)\alpha_i^2}$ 

		Various type	s of K	
Different Forms	0	R	SR	RSR
FM	$\hat{K}_{MAO}^{FM} = \frac{Max(\lambda_i)\hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)Max(\hat{\alpha}_i^2)}$	$\hat{K}_{MAO}^{FMR} = \frac{1}{\hat{K}_{MAO}^{FMO}}$	$\hat{K}_{MAO}^{FMSR} = \sqrt{\hat{K}_{MAO}^{FMO}}$	$\hat{K}_{MAO}^{FMRSR} = \frac{1}{\sqrt{\hat{K}_{MAO}^{FMO}}}$
	Khalaf and Shukur (2005)	proposed	proposed	proposed
VM	$\hat{K}_{MAO}^{VMO} = Max(\frac{Max(\lambda_i)\hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\hat{\alpha}_i^2})$	$\hat{K}_{MAO}^{VMR} = Max(\frac{1}{\hat{K}_{MAO}})$	$\hat{K}_{MAO}^{VMSR} = Max(\sqrt{\hat{K}_{MAO}})$	$\hat{K}_{MAO}^{VMRSR} = Max(\frac{1}{\sqrt{\hat{K}_{MAO}}})$
	Muniz et al. (2010)	Muniz et al. (2010)	Muniz et al. (2012)	Muniz et al. (2012)
AM	$\hat{K}_{MAO}^{AMO} = \frac{1}{p} \sum_{i=1}^{p} \left( \frac{Max(\lambda_i)\hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\hat{\alpha}_i^2} \right)$	$\hat{K}_{MAO}^{AMR} = \frac{1}{\hat{K}_{MAO}^{AMO}}$	$\hat{K}_{MAO}^{AMSR} = \sqrt{\hat{K}_{MAO}^{AMO}}$	$\hat{K}_{MAO}^{AMRSR} = \frac{1}{\sqrt{\hat{K}_{MAO}^{AMO}}}$
	Proposed	Proposed	Proposed	Proposed
HM	$\hat{K}_{MAO}^{HMO} = p \sum_{i=1}^{p} \left( \frac{Max(\lambda_i)\hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\hat{\alpha}_i^2} \right)$	$\hat{K}_{MAO}^{HMR} = \frac{1}{\hat{K}_{MAO}^{HMO}}$	$\hat{K}_{MAO}^{HMSR} = \sqrt{\hat{K}_{MAO}^{HMO}}$	$\hat{K}_{MAO}^{HMRSR} = \frac{1}{\sqrt{\hat{K}_{MAO}^{HMO}}}$
	Lawless and Wang (1976)	Proposed	Proposed	Proposed
GM	$\hat{K}_{MAO}^{GMO} = \left(\prod_{i=1}^{p} \frac{Max(\lambda_i)\hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\hat{\alpha}_i^2}\right)^{\frac{1}{p}}$	$\hat{K}_{MAO}^{GMR} = \frac{1}{\hat{K}_{MAO}^{GMO}}$	$\hat{K}_{MAO}^{GMSR} = \sqrt{\hat{K}_{MAO}^{GMO}}$	$\hat{K}_{MAO}^{GMRSR} = \frac{1}{\sqrt{\hat{K}_{MAO}^{GMO}}}$
	Muniz et al. (2010)	Proposed	Muniz et al. (2012)	Muniz et al. (2012)
M	$\hat{K}_{MAO}^{MO} = Median(\frac{Max(\lambda_i)\hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\hat{\alpha}_i^2})$	$\hat{K}_{MAO}^{MR} = Median(\frac{1}{\hat{K}_{MAO}})$	$\hat{K}_{MAO}^{MSR} = Median(\sqrt{\hat{K}_{MAO}})$	$\hat{K}_{MAO}^{MRSR} = Median(\frac{1}{\sqrt{\hat{K}_{MAO}}})$
		Muniz et al. (2010)	Proposed	Muniz et al. (2010)

# 3. Model formulation and procedure for data generation for simulation study

Consider a linear regression model of the form:

(3.1) 
$$Y_t = \beta_0 + \beta_1 X_{1t} + \beta_2 X_{2t} + \dots + \beta_p X_{pt} + U_t$$
$$t = 1, 2, \dots, n; p = 3, 7$$

where  $U_t \sim N(0, \sigma^2)$ .

The model was studied with fixed regressors,  $X_{it}$ , i = 1, 2, ..., p; t = 1, 2, ..., n such that there exist different levels of multicollinearity among the regressors.

- **3.1. Procedure for generating the error terms.** The error term  $U_t$  was generated to be normally distributed with mean zero and variance  $U_t \sim N(0, \sigma^2)$ . In this study,  $\sigma$  values were 0.5, 1 and 5.
- **3.2.** Procedure for generating the explanatory variables. The procedure used by McDonald and Galarneau (1975), Wichern and Churchill (1978), Gibbons (1981) and Kibria (2003) was also used to generate the explanatory variables in this study. This is given as:

(3.2) 
$$X_{ti} = (1 - \rho^2)^{\frac{1}{2}} Z_{ti} + \rho Z_{tp}$$
$$t = 1, 2, 3, ..., n; i = 1, 2, ..., p$$

where  $Z_{ti}$  is independent standard normal distribution with mean zero and unit variance,  $\rho$  is the correlation between any two explanatory variables and p is the number of explanatory variables. The values of  $\rho$  were taken as 0.8, 0.9, 0.95, 0.99 and 0.999. Thus, the inter-correlation between the variables was the same. In this study, the number of explanatory variable (p) was taken to be three (3) and seven (7).

3.3. Procedure for generating the dependent variable. The regression model is

(3.3) 
$$Y_t = \beta_0 + \beta_1 X_{i1} + \beta_2 X_{i2} + \dots + \beta_p X_{ip} + U_t$$
$$t = 1, 2, \dots, n; p = 3, 7$$

 $\beta_0$  was taken to be identically zero. When p=3, the values of  $\beta$  were chosen to be:  $\beta_1=0.8,\ \beta_2=0.1,\ \beta_3=0.6$ . When p=7, the values of  $\beta$  were chosen to be:  $\beta_1=0.4,\beta_2=0.1,\beta_3=0.6,\beta_4=0.2,\beta_5=0.25,\beta_6=0.3,\beta_7=0.53$ . The parameter values were chosen such that  $\beta'\beta=1$  which is a common restriction in simulation studies of this type (Muniz and Kibria, 2009). We varied the sample sizes between 10, 20, 30, 40 and 50. Three different values of  $\sigma:0.5,1$  and 5 were also used. At a specified value of n,p and  $\sigma$ , the fixed Xs are first generated; followed by the U, and the values of Y are then obtained using the regression model. The experiment is repeated 1000 times.

**3.4.** Criterion for investigation. Several authors in literatures had applied the mean square error (MSE) to evaluate and compare the performance of ridge regression estimator with that of the ordinary least square estimator when there is multicollinearity. Some of these were Hoerl and Kennard (1970), Lawless and Wang (1976), Saleh and Kibria (1993), Kibria (2003), Khalaf and Shukur (2005), Alkhamisi *et al.* (2006), Mansson *et al.* (2010). To investigate whether the ridge estimator is better than the OLS estimator, the MSE is calculated using equation defined already:

(3.4) 
$$MSE(\hat{\beta}_{ridge}) = \hat{\sigma}^2 \sum_{i=1}^p \frac{\lambda_i}{(\lambda_i + \hat{K})^2} + \hat{K}^2 \sum_{i=1}^p \frac{\hat{\alpha}_i^2}{(\lambda_i + \hat{K})^2}$$

(3.5) 
$$MSE(\hat{\beta}_{OLS}) = \hat{\sigma}^2 \sum_{i=1}^{p} \frac{1}{\lambda_i}$$

where  $\lambda_1, \lambda_2, ..., \lambda_p$  are the eigenvalues of  $X'X, \hat{K}$  is the estimator of the ridge parameter  $K, \hat{\alpha}_i$  is the  $i^{th}$  element of the vector  $\hat{\alpha} = Q'\hat{\beta}$  where Q is an orthogonal matrix. This is further examined by computing the relative efficiency of the ridge regression estimator relative to OLS estimator.

(3.6) Relative Efficiency (RE) = 
$$\frac{MSE(\hat{\beta}_{ridge})}{\hat{\beta}(OLS)}$$

Thus, the smaller the efficiency value the better the ridge parameter. Consequently, ridge parameter estimates whose efficiency was not more than 0.75 are preferred and selected. That is, the ridge estimators whose MSE were better than that of OLS by at least 25% of OLS MSE. Furthermore, the number of times they were preferred (RE  $\leq 0.75$ ) over the five (5) levels of multicollinearity and three (3) error variance was counted so as to know the frequency of their efficiency at each level of sample size. Thus, a maximum of fifteen (15) counts was expected.

#### 4. Results and discussion

**4.1. Summary of results with**  $\hat{K}_{HK_i} = \frac{\hat{\sigma}^2}{\hat{\alpha}_1^2}$ . A sample of the relative efficiency of the ridge parameter based on  $\hat{K}_{HK_i}$  of Hoerl and Kennard (1970) at different forms and various types when n=10 is given in Appendix 1. The details are contained in the work of Lukman (2015). The frequency of the relative efficiency over the levels of multicollinearity and error variance is summarized in Table 5.

From Table 5, all the best methods in p=7 are also best in p=3. However, their order of performance differs and GMO which is best in p=3 is not among the best in p=7. It is also noted that two of the newly proposed techniques, **FMSR** and **HMSR**, are among the best five at each number of regressors. Consequently, the best techniques are: HMO, MO, FMO, **FMSR** and **HMSR**.

**4.2.** Summary of Results with  $\hat{K}_{LW_i} = \frac{\hat{\sigma}^2}{\lambda_i \hat{\alpha}_i^2}$ . A sample of the relative efficiency of the ridge parameter based on  $\hat{K}_{LW_i}$  of Lawless and Wang (1975) at different forms and various types when n=30 is given in Appendix 2. The details are contained in the work of Lukman (2015). The frequency of the relative efficiency over the levels of multicollinearity and error variance is summarized in Table 6.

From Table 6, the best methods are MO, GMO, AMSR, GMSR and MSR. All these are newly proposed techniques.

**4.3. Summary of Results with**  $\hat{K}_{AKS_i} = \frac{\hat{\sigma}^2 \lambda_i}{(n-p)\hat{\sigma}^2 + \lambda_i \hat{\alpha}_i^2}$ . The relative efficiency of the ridge parameter based on  $\hat{K}_{AKS_i}$  of Alkhamisi *et al.* (2006) at different forms and various types when n=40 is given in Appendix 3. The details are contained in the work of Lukman (2015). The frequency of the relative efficiency over the levels of multicollinearity and error variance is summarized in Table 7.

From Table 7, the preferred techniques are FMO, FMSR, HMSR, MSR and GMSR. It is also noted that four of the newly proposed techniques, FMSR, HMSR, MSR and GMSR, are among the best five at each number of regressors.

**4.4.** Summary of Results with  $\hat{K}_{MAO_i} = \frac{Max(\lambda_i)\hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\hat{\alpha}_i^2}$ . The relative efficiency

of the ridge parameter based on  $\hat{K}_{MAO_i}$  of Muniz *et al.* (2012) at different forms and various types when n=50 is given in Appendix 4. The details are contained in the work of Lukman (2015). The frequency of the relative efficiency over the levels of multicollinearity and error variance is summarized in Table 8.

From Table 8, the results of p = 3 and p = 7, it can be concluded that the best methods are VMO, FMO, FMSR, VMSR, AMSR, AMO, MSR and GMSR. Among these, two are newly proposed.

**Table 5**: Frequency of the relative efficiency of ridge parameters based on  $\hat{K}_{HK_i} = \frac{\hat{\sigma}^2}{\hat{\alpha}_i^2}$  estimator with Multicollinearity (5 Levels) and Error Variances (3 levels) effect partial out

Different	Various	methods				р	=3						р	=7		
Forms		methods			n							n				
Forms	Types		10	20	30	40	50	Total	Rank	10	20	30	40	50	Total	Rank
	Original	FMO	15	15	15	13	13	71	3.5	15	12	15	13	13	68	1
	Reciprocal	FMR	5	2	6	7	4	24	18.5	0	4	6	7	4	21	15.5
Fixed	Square root	FMSR	14	14	15	13	12	68	5	7	10	13	13	13	56	3
Maximum	Reciprocal of															
	Square root	FMRSR	9	8	10	8	5	40	12.5	0	5	9	8	6	28	10.5
	Original	VMO	8	2	5	4	3	22	20	0	0	0	3	0	3	24
	Reciprocal	VMR	5	2	6	7	4	24	18.5	0	4	6	7	4	21	15.5
Varying	Square root	VMSR	11	8	11	13	11	54	10	0	3	0	6	3	12	21
Maximum	Reciprocal of															
	Square root	VMRSR	9	8	10	8	5	40	12.5	0	5	9	8	6	28	10.5
	Original	AMO	11	6	9	8	8	42	11	0	1	0	4	0	5	23
	Reciprocal	AMR	2	0	2	2	2	8	24	1	1	1	4	1	8	22
Arithmetic	Square root	AMSR	11	11	11	13	11	57	9	0	6	4	11	10	31	9
Mean	Reciprocal of															
	Square root	AMRSR	8	5	7	4	4	28	17	2	3	6	4	3	18	17
	Original	HMO	15	15	15	15	15	75	1	10	10	15	15	15	65	2
	Reciprocal	HMR	4	0	4	4	2	14	22	0	2	6	4	1	13	20
Harmonic	Square root	HMSR	13	12	13	15	13	66	6	4	9	12	14	13	52	4
Mean	Reciprocal of															
	Square root	HMRSR	10	5	8	5	6	34	16	0	6	6	7	4	23	14
	Original	GMO	15	13	13	15	15	71	3.5	2	9	6	15	13	45	6
	Reciprocal	GMR	3	0	3	2	2	10	23	1	3	3	4	3	14	19
Geometric	Square root	GMSR	13	11	13	13	13	63	7	1	7	9	13	12	42	8
Mean	Reciprocal of															
	Square root	GMR SR	10	6	8	7	4	35	15	1	5	6	7	6	25	12.5
	Original	MO	15	14	13	15	15	72	2	2	9	8	15	13	47	5
	Reciprocal	MR	4	2	7	4	4	21	21	1	4	3	4	3	15	18
Median	Square root	MSR	13	11	12	13	11	60	8	1	7	9	13	13	43	7
	Reciprocal of															
	Square root	MRSR	11	6	8	7	7	39	14	1	5	6	7	6	25	12.5

**Table 6:** Frequency of the relative efficiency of ridge parameters based on  $\hat{K}_{LW_i} = \frac{\hat{\sigma}^2}{\lambda_i \hat{\alpha}_i^2}$  estimator with multicollinearity (5 levels) and error variances (3 levels) effect partial out

						D	=3						D	=7		
Different	Various	methods	-		n							n				
Forms	Types		10	20	30	40	50	Total	Rank	10	20	30	40	50	Total	Rank
	Original	FMO	0	0	0	0	0	0	24	0	1	0	0	0	1	24
	Reciprocal	FMR	2	0	3	2	1	- 8	22	0	1	0	2	0	3	23
Fixed	Square root	FMSR	10	6	6	6	3	31	13	13	5	6	3	3	30	11
Maximum	Reciprocal of															
	Square root	FMRSR	5	1	5	5	5	21	17	0	2	0	7	4	13	18
	Original	VMO	11	7	9	6	6	39	11	0	1	0	5	0	6	21
	Reciprocal	VMR	3	0	4	2	1	10	21	0	1	0	3	0	4	22
Varying	Square root	VMSR	11	9	11	13	10	54	1.5	0	6	4	12	9	31	10
Maximum	Reciprocal of															
	Square root	VMRSR	6	3	6	6	5	26	15	0	3	3	7	5	18	16
	Original	AMO	11	11	10	10	8	50	5	0	4	0	8	3	15	17
	Reciprocal	AMR	2	0	2	2	1	7	23	0	3	1	3	2	9	20
Arithmetic	Square root	AMSR	11	11	11	11	10	54	1.5	0	7	8	11	10	36	4
Mean	Reciprocal of															
	Square root	AMRSR	6	4	4	5	4	23	16	2	7	5	4	4	22	15
	Original	HMO	9	5	6	4	3	27	14	7	5	5	5	4	26	13
Harmonic	Reciprocal	HMR	5	0	5	4	2	16	19	0	2	0	6	2	10	19
Mean	Square root	HMSR	11	6	8	6	6	37	12	4	7	6	6	6	29	12
	Reciprocal of															
	Square root	HMRSR	8	7	9	9	9	42	10	0	6	6	12	9	33	8
	Original	GMO	13	9	11	8	7	48	7	2	8	8	11	10	39	2
	Reciprocal	GMR	5	0	5	4	3	17	18	0	8	7	9	8	3.2	9
Geometric	Square root	GMSR	12	11	11	8	7	49	6	1	8	8	10	9	36	4
Mean	Reciprocal of															
	Square root	GMRSR	9	8	11	10	8	46	8.5	1	8	8	10	8	35	6.5
	Original	MO	13	11	11	8	8	51	3.5	2	8	8	10	12	40	1
	Reciprocal	MR	4	0	5	4	2	15	20	0	7	5	7	6	25	14
Median	Square root	MSR	11	11	11	10	8	51	3.5	1	8	8	10	9	36	4
	Reciprocal of															
	Square root	MRSR	9	8	11	10	8	46	8.5	1	8	8	10	8	35	6.5
Note	Note: Proposed methods of ridge parameters are in bold form.												ıb	old	forn	n.

**Table 7:** Frequency of the relative efficiency of ridge parameters based on  $\hat{K}_{AKS_i} = \frac{\hat{\sigma}\lambda_i}{(n-p)\hat{\sigma}^2 + \lambda_i \hat{\alpha}_i^2}$  estimator with multicollinearity (5 levels) and error variances (3 levels) effect partial out

						D	=3						D	=7		
Different	Various	methods	$\vdash$		n							n				
Forms	Types		10	20	30	40	50	Total	Rank	10	20	30	40	50	Total	Rank
	Original	FMO	15	15	15	13	11	69	1	15	12	15	13	13	68	1
	Reciprocal	FMR	7	5	8	8	5	33	21	0	4	6	8	5	23	21
Fixed	Square root	FMSR	14	14	15	12	10	6.5	2	7	10	13	13	12	55	2
Maximum	Reciprocal of		İ	İ	İ					İ				İ		
	Square root	FMRSR	9	8	11	8	5	41	17	0	5	9	8	6	28	17
	Original	VMO	11	10	11	11	10	53	3.5	1	7	9	11	10	38	3.5
	Reciprocal	VMR	6	3	6	7	5	27	22	0	1	2	8	4	15	22
Varying	Square root	VMSR	11	11	11	10	10	53	3.5	1	7	9	11	9	37	3.5
Maximum	Reciprocal of															
İ	Square root	VMRSR	9	5	9	11	9	43	15.5	0	5	6	11	9	31	15.5
	Original	AMO	13	9	11	7	5	45	13.5	3	9	10	7	7	36	13.5
İ	Reciprocal	AMR	9	8	11	10	8	46	11.5	0	5	7	11	10	33	11.5
Arithmetic	Square root	AMSR	11	11	13	8	7	50	7	2	8	12	8	7	37	7
Mean	Reciprocal of	İ	$\overline{}$													
	Square root	AMRSR	11	9	11	8	10	49	9	1	6	9	11	10	37	9
	Original	нмо	15	0	0	0	0	15	24	10	4	0	0	0	14	24
	Reciprocal	HMR	7	4	7	9	8	35	20	0	3	3	9	7	22	20
Harmonic	Square root	HMSR	15	11	12	6	6	50	7	5	10	12	9	9	45	7
Mean	Reciprocal of															
	Square root	HMRSR	9	8	9	11	8	45	13.5	0	6	9	9	8	3.2	13.5
	Original	GMO	15	9	10	6	3	43	15.5	7	10	9	1	3	30	15.5
	Reciprocal	GMR	8	5	9	10	7	39	18.5	0	4	6	11	9	30	18.5
Geometric	Square root	GMSR	13	11	11	9	6	50	7	2	9	13	9	9	42	7
Mean	Reciprocal of															
	Square root	GMRSR	9	8	11	10	8	46	11.5	0	6	9	11	9	3.5	11.5
	Original	MO	15	0	7	0	0	22	23	6	10	10	6	0	32	23
	Reciprocal	MR	7	5	9	9	9	39	18.5	0	4	6	9	9	28	18.5
Median	Square root	MSR	13	11	13	9	6	52	5	2	10	13	9	9	43	5
	Reciprocal of															
	Square root	MRSR	9	8	11	11	8	47	10	0	6	9	11	9	35	10

Note: Proposed methods of ridge parameters are in bold form.

**Table 8:** Frequency of the relative efficiency of ridge parameters based on  $\hat{K}_{MAO_i} = \frac{Max(\lambda_i)\hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + Max(\lambda_i)\hat{\alpha}_i^2}$  estimator with multicollinearity (5 levels) and error variances (3 levels) effect partial out

Forms			=7	D						=3	D						
Part					n							n			methods	Various	Different
Fixed Maximum   Square moot   FMR   Square moot   FMSR   Square moot   FMSR   Square moot   FMSR   Square moot   FMSR   Square moot   Square moot   FMSR   Square moot   Square moot   FMSR   Square moot   Square moot   FMRSR   Square moot	otal Rank	Total	50	40	30	20	10	Rank	Total	50	40	30	20	10		Types	Forms
Square most Reciprocal of Square most Reciprocal of Square most Square most PMRSR   13   11   13   10   10   57   4   5   5   9   12   13   12	58 1.5	68	13	13	15	12	15	1.5	69	11	13	15	15	15	FMO	Original	
Maximum   Reciprocal of Square motor   FMR SR   1   0   11   0   0   7   47   11   0   6   0   8   6   0   0   0   0   0   0   0   0   0	26 18.5	26	6	7	8	5	0	18	39	5	8	10	7	9	FMR	Reciprocal	
Square moot   FMR SR   1   9   11   9   7   47   11   0   6   9   8   6	51 3.5	51	12	13	12	9	5	4	57	10	10	13	11	13	FMSR	Square root	Fixed
Varying   Reciprocal of Manament   Variable   Variabl																Reciprocal of	Maximum
Reciprocal of Square most   MR SR   S   S   S   S   S   S   S   S   S	29   16	29	6	8	9	6	0	11	47	7	9	11	9	11	FMRSR	Square root	
Varying   Square moot   VMSR   13   11   13   10   10   57   4   5   9   12   13   12   12   13   12   13   13		68	13	13	15	12	15			11	13	15	15	15	VMO	Original	
Maximum   Reciprocal of Square most   VMRSR   0   5   9   11   0   43   16   0   5   6   11   9		15				1	0	22					3	6	VMR	Reciprocal	
Square root   Square root	51 3.5	51	12	13	12	9	5	4	57	10	10	13	11	13	VMSR	Square root	Varying
Original Reciprocal AMR   State   St																Reciprocal of	Maximum
Reciprocal AMR   S   S   S   S   S   S   S   S   S		31									11		5		VMRSR	Square root	
Arithmetic Mean   Square moot Reciprocal of Square moot Reciprocal of Square moot Reciprocal of Square moot Reciprocal of Square moot Reciprocal of Reciproc		46	7	7	12	10	10	6.5	54	7	9	13	10	15			
Mean   Square moto   AMR SR   0   8   11   8   8   44   14.5   0   5   9   11   10		30					0	14.5							AMR	Reciprocal	
Square moof   AMR SR   9   8   11   8   8   44   14.5   0   5   9   11   10	48 5.5	48	10	10	13	10	5	4	57	9	10	13	12	13	AMSR	Square root	Arithmetic
Harmonic   Reciprocal   HMO   3   0   0   0   0   13   24   10   2   0   0   0   0   0   0   0   0																Reciprocal of	Mean
Harmonic Mean   Reciprocal Square moot   HMR R   7   5   7   9   8   36   21   0   3   3   9   7		3.5	10	11	9					8	8	11	8			Square root	
Mean   Square root   Reciprocal of Square root   Reciprocal of Square root   Square		12		0	0		10			0	0		0			Original	
Reciprocal of Square mod   HMR SR   9   8   9   11   8   45   13   0   5   6   11   9   9   9   9   9   9   9   9		22	7	9		3	0			8	9		5	7	HMR	Reciprocal	Harmonic
Square mot   HMRSR   9   8   9   11   8   45   13   0   5   6   11   9	43 9	43	9	6	12	10	6	9	50	6	6	12	11	15	HMSR	Square root	Mean
Original Reciprocal GMR   S   0   0   4   1   38   20   10   8   6   0   0   0																Reciprocal of	
Reciprocal Reciprocal   GMR   7   5   9   9   9   39   18   0   3   5   9   9   9   9   9   9   9   9   9	31 13	31	9	11	6	5	0	13	45	8	11	9	8	9	HMRSR	Square root	
Geometric   Square most   Reciprocal of Square most   GMRSR   14   11   13   9   6   53   8   5   10   12   9   9		24	0	0	6	8	10			1	4	9	9	15	GMO	Original	
Reciprocal of Square moot   GMR SR   9   8   11   11   8   47   11   0   5   6   11   9   1   1   1   1   1   1   1		24	7	9		3	0	18		9	9		5	7	GMR	Reciprocal	
Square poot         GMR SR         9         8         11         11         8         47         11         0         5         6         611         9           Original         MO         15         0         6         0         0         21         23         10         8         9         0         0           Reciprocal         MR         7         5         9         9         9         39         18         0         4         6         9         7	45 8	45	9	9	12	10	5	- 8	53	6	9	13	11	14	GMSR	Square root	Geometric
Original Reciprocal         MO         15         0         6         0         0         21         23         10         8         9         0         0           Reciprocal         MR         7         5         9         9         9         39         18         0         4         6         9         7																Reciprocal of	Mean
Reciprocal MR 7 5 9 9 9 39 18 0 4 6 9 7		31	9	11	6	5				8	11	11	8			Square root	
		27		0	9	8	10			0	0	6			MO	Original	
Madian   Community   MCD   15   11   12   0   6   54   65   5   10   15   0   0		26															
Median   aquare root   Mark   10   11   13   9   0   54   0.5   5   10   15   9   9	48 5.5	48	9	9	15	10	5	6.5	54	6	9	13	11	15	MSR	Square root	Median
Reciprocal of																Reciprocal of	
Square root   MR SR   9   8   11   11   8   47   11   0   5   8   11   9	33 11	33	9	11	8	5	0	11	47	8	11	11	8	9	MRSR	Square root	

Note: Proposed methods of ridge parameters are in bold form.

### 5. Summary and concluding remarks

Table 9 presents the summary of the five best ridge parameters estimation techniques having obtained their relative efficiency, counting the relative efficiency (RE $\leq$  0.75) over the five (5) levels of multicollinearity, three (3) levels of error variances and the five (5) levels of sample sizes. Thus, a maximum of seventy five (75) counts is expected.

**Table 9:** Summary of best ridge parameters

Ridge		p=3			p=7	
parameter	Best Method	Frequency	Best	Best Method	Frequency	$\mathbf{Best}$
	HMO	75		HMO	65	
	MO	72		MO	47	
$K_{HK}$	FMO	71	HMO	FMO	68	FMO
	GMO	71		GMO	45	
	FMSR	68		FMSR	56	
	HMSR	66		HMSR	52	
	MO	51		MO	40	
	GMO	48		GMO	39	
$K_{LW}$	AMSR	54	MSR	AMSR	36	MO
	GMSR	49		GMSR	36	
	MSR	51		MSR	36	
	VMO	69		VMO	68	
	FMO	69		FMO	68	
	FMSR	57		FMSR	51	
$K_{LS}$	VMSR	57		VMSR	51	VMO/FMO
	AMSR	57	VMO/FMO	AMSR	48	
	AMO	54		AMO	46	
	MSR	54		MSR	48	
	GMSR	53		GMSR	45	
	FMO	69		FMO	68	·
	FMSR	65		FMSR	55	
$K_{ALK}$	HMSR	50	FMO	FMSR	45	FMO
	MSR	52		MSR	43	
	GMSR	50		GMSR	42	

Source: Table 5, 6, 7 and 8

From Table 9, the best estimators of the ridge parameter techniques are of the different forms and various types. These are generally Fixed Maximum Original, Varying Maximum Original, Harmonic Mean Original, Geometric Mean Original and Arithmetic Mean Square root. The best ridge parameter techniques consist of both the existing ones and newly proposed. The proposed techniques also perform better than the existing ones in some cases. Moreover, with  $\hat{K}_{LW_i}$ , the existing Harmonic Mean version is not even among the best five.

The conclusions of this paper are restricted to the simulation study that has been conducted in this paper. To make a definite statement, one might need more data from different kind of populations. However, the findings of this paper can be generalized for a great population with high confidence.

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Appendix 1: MSE of OLS and Relative efficiency of the ridge parameter based on  $\hat{K}_{HK}$ 

								10 p =3							
Method			$\sigma = 0.5$	5				$\sigma = 1$					$\sigma = 5$		
	0.8	0.9	0.95	0.99	0.999	0.8	0.9	0.95	0.99	0.999	0.8	0.9	8.95	0.99	0.999
MSE OLS	0.920	1.988	1.889	22.661	248 6 16	0.985	2.043	4.315	24.262	266.182	3.034	6.292	13.291	74.738	8 19 9 54
FMO	0.520	0.438	0.401	0.380	0.374	0.512	0.433	0.397	0.376	0.370	0.475	0.431	0.405	0.3 73	0.354
FMR	0.771	0.840	0.935	1.003	0.998	0.773	0.831	0.915	0.974	0.966	0.739	0.705	8.724	0.708	0.667
FMSR	0.534	0.447	0.428	0.538	0.764	0.529	0.443	8.424	0.529	0.744	0.508	0.444	8.422	0.463	0.557
FMRSR	0.662	0.692	0.811	0.975	0.996	0.664	0.687	0.795	0.947	0.964	0.652	0.605	0.642	0.691	0.666
VMO	0.866	0.732	0.729	0.878	0.980	0.846	0.722	0.721	0.859	0.949	0.818	0.729	0.695	0.678	0.663
VMR	0.771	0.840	0.935	1.003	0.998	0.773	0.831	0.915	0.974	0.966	0.739	0.705	0.724	0.708	0.667
VMSR	0.587	0.598	0.671	0.880	0.982	0.571	0.590	0.663	0.859	0.951	0.615	0.621	0.637	8.667	0.662
VMRSR	0.662	0.692	0.8117	0.975	0.996	0.664	0.687	0.795	0.947	0.964	0.652	0.605	0.642	0.691	0.666
AMO	0.703	0.614	0.617	0.773	0.952	0.682	0.605	0.611	0.760	0.925	0.725	0.664	0.643	0.646	0.656
AMR	0.897	0.847	0.834	0.921	0.988	0.896	0.840	0.822	0.898	0.957	0.933	0.859	0.776	0.703	0.676
AMSR	0.537	0.542	0.607	0.830	0.972	8.522	0.535	0.600	0.811	0.942	0.569	0.578	0.601	8.649	0.659
A MR SR	0.791	0.708	0.711	0.887	0.985	0.789	0.704	0.705	0.864	0.954	0.832	0.716	0.637	8.6 26	0.650
HMO	0.443	0.407	0.397	0.397	0.398	0.439	0.404	0.394	0.394	0.395	0.455	0.432	0.416	0.392	0.375
HMR	0.803	0.809	0.889	0.993	0.997	0.805	0.804	0.872	0.964	0.965	0.804	0.707	0.696	0.704	0.667
HMSR	0.490	0.445	0.468	8.627	0.832	0.486	0.442	0.464	0.616	0.809	0.478	0.448	0.456	0.519	0.592
HMRSR	0.689	0.669	0.764	0.961	0.995	0.691	0.665	0.750	0.933	0.963	0.695	0.602	0.612	0.681	0.666
GMO	0.487	0.476	0.497	0.595	0.736	0.479	0.472	0.493	0.588	0.721	0.573	0.559	0.556	0.562	0.584
GMR	0.858	0.817	0.845	0.968	0.996	0.857	0.812	0.834	0.940	0.964	0.889	0.788	0.705	8.671	0.665
GM SR	0.470	0.474	0.536	0.748	0.927	8.467	8.471	0.531	0.733	0.899	0.496	0.506	0.536	0.604	0.641
GMRSR	0.740	0.675	0.724	0.932	0.993	0.738	0.670	0.715	0.905	0.961	0.768	0.644	0.590	8.647	0.663
MO	0.455	0.459	0.513	0.628	0.667	0.451	0.458	0.514	0.621	0.654	0.549	0.551	0.568	0.569	0.545
MR	0.823	0.767	0.804	0.951	0.995	0.818	0.760	0.785	0.922	0.963	0.846	0.741	0.663	0.661	0.665
MSR	0.470	0.471	0.544	0.750	0.900	0.468	0.470	0.542	0.736	0.875	0.501	0.507	0.543	0.604	0.630
MRSR	0.716	0.654	0.709	0.925	0.992	0.714	0.647	0.694	0.898	0.961	0.737	0.620	0.572	0.645	0.663
								10 p=7							
MSE OLS	18.560	41.405	91811	549.321	6229.414	19.622	43.773	97.063	580.746	6 58 5 . 779	52.209	116.469	258.2579	1545.204	17522960
FMO	0.379	0.369	0.362	0.353	0.348	0.402	0.391	0.385	0.376	0.371	0.679	0.671	0.666	0.658	0.653
FMR	0.874	0.881	0.883	0.883	0.881	1.017	1.0 29	1.033	1.035	1.035	2.631	2.687	2.716	2.745	2.759
FMSR	0.493	0.550	0.609	0.721	0.809	0.550	0.624	0.701	0.842	0.951	1.245	1.519	1.78 2	2.242	2.559
FMRSR	0.829	0.857	0.871	0.881	0.881	0.970	1,003	1.0 21	1.033	1.035	2.563	2.6 58	2.704	2.744	2.759
VMO	0.879	0.868	0.866	0.871	0.879	1.0 18	1.0 13	1.0 13	1.0 22	1.033	2.614	2.662	2.694	2.73 7	2.757
VMR	0.874	0.881	0.883	0.883	0.881	1.017	1.0 29	1.033	1.035	1.035	2.631	2.687	2.716	2.745	2.759
VMSR	0.831	0.845	0.856	0.871	0.880	0.969	0.989	1,003	1.0 22	1.033	2.546	2.6 24	2.6 74	2,733	2.757
V MR SR AM O	0.829	0.857 0.832	0.871 0.839	0.881 0.852	0.881	0.970	1.003	1.0 21	1.033	1.035	2.563	2.6 58	2.704	2.744	2.759 2.753
AMR	0.827	0.832	0.839	0.852	0.871 0.882	0.965 0.822	0.975	0.984 0.902	1.003	1.0 24	2.553 1.338	2.6 13 1.8 10	2.6 56	2.716	2.753
AMSR	0.759	0.750	0.777	0.863	0.882 0.877	0.8 22	0.847	0.902	1.007	1.026	2.483	2.581	2.18 2	2.607	2.748
AMRSR	0.793	0.820	0.839	0.859	0.877	0.76.2	0.962	0.984	1.014	1.031	1.697	2.153	2.4.23	2.721	2.755
HMO	0.009	0.727	0.780	0.485	0.880	0.762	0.549	0.529	0.535	0.538	1.107	1.131	1.146	1.164	1.173
HMR	0.471	0.476	0.480	0.882	0.488 0.881	0.517	1.010	1.0 25	1.034	1.035	2.573	2,668	2.718	2.745	2.759
HMR	0.842	0.863	0.875	0.788	0.881	0.983	0.771	0.832	0.926	0.990	1.780	2.668	2.710	2.745	2.759
HMRSR	0.007	0.837	0.712	0.700	0.881	0.098	0.771	1.010	1.032	1.035	2.484	2.6 24	2.220	2.743	2.759
GMO	0.796	0.837	0.861	0.794	0.8815	0.934	0.877	0.901	0.937	0.964	2.454	2.440	2.50 2	2.743	2.739
GMR	0.718	0.743	0.763	0.794	0.813	0.865	0.577	0.901	1.030	1.035	2.817	2.449	2.50 2	2.739	2.759
GMSR	0.734	0.769	0.843	0.844	0.869	0.852	0.946	8.944	0.993	1.033	2.338	2.475	2.570	2.683	2.740
GMRSR	0.724	0.794	0.836	0.875	0.881	0.850	0.933	0.944	1.0 27	1.035	2.169	2.478	2.570	2.733	2.758
MO	0.714	0.754	0.777	0.801	0.8811	0.842	0.887	0.917	0.947	0.959	2.489	2.495	2.549	2.689	2.638
MR	0.714	0.795	0.839	0.877	0.881	0.848	0.9 26	0.983	1.0 29	1.035	1.872	2.373	2.545	2.738	2,759
MSR	0.736	0.793	0.839	0.845	0.868	0.851	0.9 26	0.950	0.996	1.033	2.364	2.501	2.58 7	2.738	2.739
MRSR	0.725	0.772	0.833	0.843	0.881	0.846	0.910	0.9 79	1.0 26	1.021	2.113	2.447	2.56 10	2.73 2	2.758
MILSE	0.726	0.791	0.033	0 2 74	0.881	0.246	0.0.28	0.079	1.020	1.033	2.113	2,447	2010	2.732	2.735

**Appendix 2:** MSE of OLS and Relative efficiency of the ridge parameter based on  $\hat{K}_{LW}$ 

							n=10 p	=3							
Method			$\sigma = 0$	.5				$\sigma = 1$					$\sigma = 1$	5	
	0.8	8.9	0.95	0.99	0.999	0.8	0.9	0.95	0.99	0.999	8.8	0.9	0.95	0.99	0.999
M SE OLS	0.386	0.804	1.700	9.536	104.240	0.396	0.8 26	1.746	9.794	10 7.0 59	0.732	1.526	3.226	18.094	19 7.79 2
FMO	0.993	0.988	0.980	0.946	0.909	0.993	0.988	0.979	0.945	0.908	0.984	0.972	0.953	0.899	0.865
FMR	1940	1.568	1348	1.125	1.0 56	1.877	1.524	1.313	1,099	1.032	0.941	0.814	0.728	0.630	0.594
FM SR	0.946	0.898	0.823	0.595	0.421	0.945	0.897	0.821	0.592	0.418	0.920	0.854	0.758	0.508	0.321
FM SR	0.946	0.898	0.823	0.595	0.421	0.945	0.897	0.821	0.592	0.418	0.920	0.854	0.758	0.508	0.321
FMR SR	0.809	0.956	1.041	1.064	1.051	0.790	0.932	1.016	1.040	1.0 26	0.525	0.552	0.585	0.599	0.591
VMO	0.777	0.629	0.647	0.860	1.017	0.765	0.621	0.638	0.843	0.995	0.546	0.437	0.429	0.517	0.579
VMR	1864	1.473	1.258	1.087	1.051	1.80 2	1.430	1.225	1.061	1.0 26	0.890	0.753	0.674	0.607	0.591
VMRSR	9.606	0.509	0.569	0.854	1.0 20	0.597	0.504	0.560	0.836	0.997	0.484	0.382	0.379	0.501	0.577
VMSR	0.762	0.872	0.954	1.0 29	1.045	0.744	0.850	0.931	1.005	1.021	0.500	0.504	0.531	0.574	0.588
AMO	0.775	0.593	0.557	0.755	0.991	0.7587	0.586	0.551	0.741	0.969	0.570	0.429	0.382	0.466	0.568
AMR	0.915	0.921	0.931	0.965	1.025	0.908	0.912	0.919	0.951	1.001	0.853	0.818	0.780	0.686	0.613
AMSR	0.651	0.515	0.520	0.795	1.009	0.643	0.510	0.514	0.779	0.986	0.543	0.405	0.362	0.473	0.572
AMR SR	0.791	0.763	0.766	0.865	1.006	0.789	0.758	0.757	0.848	0.977	0.785	0.706	0.635	0.546	0.562
HMO HMR	0.981	0.960	0.916	0.671	0.653 1.049	0.980	0.959	0.914	0.666 1.039	0.645 1.024	0.952	0.904	0.817	0.494 0.593	0.429 0.589
HMR	1.276 0.910	1.191 0.827	0.701	1.064 0.556	0.900	0.909	1.157 0.824	1.098	0.550	0.881	0.660	0.625	0.607	0.593	0.589 0.522
HMRSR	0.649	0.747	0.701	1.001	1.042	0.909	0.824	0.697	0.550	1.018	0.867	0.754	0.597	0.5577	0.522 0.585
GMO															
GMR	0.843	0.701	0.555 0.925	0.536	0.905	0.841	0.696	0.552	0.529 0.974	0.887 1.012	0.731	0.558	0.408	0.364	0.532
GMSR	0.875	0.502	0.503	0.995	1.038	0.858 0.777	0.884 0.616	0.903	0.657	0.955	0.704	0.501	0.627 0.387	0.578	0.581 0.557
GMR SR	0.779	0.688	0.303	0.009	1.030	0.679	0.679	0.499	0.537	1.005	0.704	0.521	0.387	0.417	8.577
MO	0.827	0.643	0.743	0.923	0.944	0.679	0.638	0.728	0.586	8.924	0.034	0.369	0.321	0.326	0.547
MR	0.8 26	0.853	0.300	0.394	1.842	0.812	0.837	8.886	0.356	1.018	0.698	0.457	8.662	0.616	0.588
MSR	0.771	0.592	0.490	0.704	0.989	0.768	0.588	8.485	0.570	0.967	0.686	8.487	0.002	0.432	8.562
MRSR	0.664	0.669	0.728	0.911	1.027	0.661	0.662	8.716	0.890	1.002	0.656	8.587	8.542	0.532	8.575
								=7							
M SE OLS	1.124	2347	4961	27.78.2	303.180	1.152	2.405	5.085	28.472	3 10 . 719	2.050	4.280	9.847	50,660	552.848
FMO	0.996	0.994	0.992	0.988	0.986	0.996	0.994	0.992	0.988	0.986	0.996	0.995	5.549	0.991	0.989
FMR	1311	1.212	1.149	1.0 73	1.050	1.307	1.213	1.151	1.074	1.051	1.310	1.245	6.099	1,089	1.044
FM SR	0.956	0.920	0.869	0.721	0.534	0.955	0.920	0.870	8.722	0.534	0.953	0.923	4.139	0.739	0.532
FMR SR	0.772	0.908	0.990	1.043	1.048	8.776	0.912	0.994	1.045	1.049	0.865	0.999	5,998	1.0 70	1.043
VMO	0.993	0.975	0.984	1.025	1.045	0.985	0.970	0.988	1.0 27	1.045	1.074	1.042	5,888	1.051	1.040
VMR	1.271	1.154	1.095	1.0 53	1.048	1.265	1.153	1.096	1.055	1.049	1.189	1.153	6.006	1.0 73	1.043
VMRSR	0.657	0.740	0.828	0.979	1.040	0.665	0.734	0.831	0.980	1.040	0.755	0.809	5.6 24	1.004	1.035
VMSR	0.739	0.855	0.936	1.0 21	1.045	0.741	0.857	0.938	1.0 2 2	1.045	0.744	0.862	5.783	1.033	1.839
AMO	0.761	0.793	0.848	0.976	1.038	0.761	0.784	0.851	0.976	1.038	0.861	0.861	5.611	1.002	1.034
AMR	0.904	0.860	0.816	0.777	0.872	0.904	0.861	0.821	0.783	0.880	0.918	0.864	4.151	0.741	0.832
AMSR	0.606	0.650	0.734	0.932	1.032	0.615	0.642	0.737	0.933	1.033	0.670	0.698	5,337	0.953	1.0 28
AMR SR	0.837	0.760	0.698	0.733	0.936	0.835	0.758	0.703	0.732	0.934	0.852	8.762	3,898	0.696	0.905
HMO	0.974	0.948	0.895	0.657	0.708	0.974	0.947	0.893	0.653	0.708	0.946	0.897	3.235	0.578	0.756
HMR HMSR	0.878	0.957	0.999	1.035	1.047	0.879	0.959	1.001	1.037	1.047	0.829	0.932	5.848	1.044	1.040
HMRSR	0.889	0.796	0.677	0.626	0.903	0.888	0.795	0.675	0.625	0.904	0.851	0.741	3.498	0.623	0.921 1.032
	0.609	0.712	0.822	0.983	1.041	0.611	0.713	0.823	0.984	1.041	0.617	0.694	5.487	0.980	
GM O GM R	0.638	0.565	0.582	0.803	1.003	0.639	0.563	0.583	0.804	1.003	0.632	0.577	4.649	0.830	1.004
	0.737	0.699	0.709	0.849	1.007	0.735	0.698	0.708	0.849	1.007	0.758	0.688	4.567	0.816	0.991
GM SR	0.649	0.565	0.588	0.815	1.009	0.649	0.564	0.588	0.816	1.010	0.638	0.565	4.652	0.831	1.007
GMR SR M O	0.701	0.558	0.653	0.835	1.011	0.701	0.639	0.652	0.835 0.812	1.011	0.716 0.637	0.629	4.584	0.819	1.000
MR	0.756	0.718	0.590	0.842	1.006	8.756	0.717	0.589	0.812	1.006	0.637	0.583	4.553	0.838	0.989
MSR	0.756	0.718	0.720	0.842	1.000	0.756	0.717	0.719	0.843	1.001	0.760	0.695	4.675	0.813	1.007
MRSR	0.713	0.360	0.390	0.830	1.011	0.638	0.560	0.590	0.831	1.011	0.638	0.566	4.568	0.835	1.007
MILDIC	0.113		Not.		ropo					ara b			4.000	0 2 10	1.000

Note: Proposed techniques are bolded.

**Appendix 3:** MSE of OLS and Relative efficiency of the ridge parameter based on  $\hat{K}_{AKS}$ 

							n =40	n =3							_
Method			$\sigma = 0$	.5				σ=					$\sigma = 0$	5	
	0.8	0.9	0.95	0.99	0.999	0.8	0.9	0.95	0.99	0.999	0.8	0.9	0.95	0.99	8,999
MSE OLS	0.100	0.429	0.891	4.8 70	52,452	0.215	0.438	0.909	4.968	53,506	0.352	0.716	1.486	8.123	87.482
FMO	0.818	0.695	0.571	0.430	0.407	0.816	0.689	0.567	0.427	0.404	0.746	0.598	0.465	0.334	0.314
FMR	0.817	0.712	0.691	0.960	1.031	0.818	0.689	0.684	0.942	1.0.13	0.857	0.744	0.624	0.598	8.643
FMSR	0.818	0.693	0.565	8.465	0.656	0.817	0.690	0.562	0.461	0.647	0.781	0.635	0.488	0.347	0.438
FMRSR	0.817	0.699	0.623	0.855	1.022	0.818	0.691	0.619	0.839	1.004	0.836	0.709	0.569	0.536	8,636
VMO	0.817	0.691	0.575	0.648	0.957	0.815	0.691	8.571	0.640	0.940	0.742	0.588	0.457	0.448	8,686
VMR	0.646	0.852	1.889	1.104	1.045	8 641	0.837	1.069	1.084	1 0 26	0.544	0.555	0.6.78	0.688	0.652
VMSR	0.818	0.692	0.575	0.6 56	0.961	0.817	0.690	0.572	0.647	0.944	0.779	0.630	0.485	0.442	0,603
VMRSR	0.694	0.589	0.712	1.006	1.031	0.693	0.583	0.701	0.987	1.0 13	0.665	0.480	0.473	0.626	0.644
AMO	0.891	0.822	0.719	0.534	0.847	0.890	0.820	0.716	0.529	0.834	0.856	0.761	0.6.29	0.400	0.548
AMR	0.727	0.601	0.607	0.863	1.009	0.727	0.598	0.598	0.846	0.991	0.755	0.591	0.482	0.520	8.624
AM SR	0.858	0.761	0.639	0.576	0.917	0.857	0.759	0.637	0.569	0.901	0.835	0.719	0.572	0.409	0.579
AMRSR	0.773	0.633	0.563	0.770	0.992	0.773	0.632	0.558	0.755	0.9.74	0.784	0.628	0.490	0.480	0.615
HMO	0.929	0.921	0.915	0.909	0.905	0.929	0.920	0.915	0.908	0.905	0.925	8917	8 9 1 2	0.907	0.904
HMR	0.666	0.662	0.925	1.0 72	1.042	0.664	0.652	0.908	1.052	1.0 24	0.630	0.478	0.580	0.668	0.651
HMSR	0.884	0.831	0.767	0.611	0.545	0.883	0.830	0.767	0.610	0.538	0.879	0.824	0.757	0.576	0.416
HMRSR	0.737	0.589	0.634	8.9 75	1.030	0.736	0.585	0.625	0.958	1.011	0.724	0.518	0.445	0.607	0.643
GMO	0.913	0.883	0.849	8.754	0.610	0.912	0.883	0.848	0.753	0.608	0.898	0.865	0.8 26	0.718	0.549
GMR	0.693	0.603	0.765	1.0 29	1.034	0.692	0.596	0.751	1.010	1.015	0.689	0.494	0.491	0.638	8,645
GM SR	0.872	0.800	0.712	0.544	0.677	0.871	0.799	0.710	0.541	0.666	0.860	0.78.2	0.682	0.459	0.444
GMRSR	0.754	0.604	0.587	0.911	1.024	0.754	0.602	0.579	0.894	1.006	0.753	0.562	0.445	0.565	8,639
MO	0.917	0.902	0.890	0.871	0.858	0.916	0.902	0.890	0.871	0.858	0.912	0.898	0.887	0.868	0.855
MR	0.687	0.623	0.856	1.0 59	1.040	0.685	0.615	0.840	1.040	1.0 2 2	0.659	0.474	0.543	0.668	8.649
MSR	0.875	0.815	0.744	0.586	0.569	0.874	0.814	0.743	0.584	0.561	0.869	0.807	0.731	0.539	0.413
MR SR	0.750	0.595	0.609	0.957	1.029	0.750	0.592	0.600	0.940	1.011	0.739	0.534	0.440	0.596	8.642
							n =40 :	=7							
MSE OLS	0.612	1.225	2.508	13.382	141652	0.625	1.252	2.562	13.669	144.689	1.047	2,098	4.294	22988	242.498
FMO	0.793	0.684	0.600	0.542	0.530	0.790	0.680	0.595	0.538	0.527	0.690	0.567	8.49.2	0.443	0.431
FMR	0.813	0.707	0.675	0.939	1.021	0.815	0.707	0.669	0.923	1.005	0.867	0.752	868.0	0.608	0.683
FM SR	0.800	0.684	0.581	0.506	0.641	0.798	0.681	0.578	0.502	0.633	0.748	0.614	0.502	0.394	0.448
FMRSR	0.809	0.693	0.618	0.835	1.013	0.810	0.693	0.613	0.820	0.996	0.837	0.711	0.562	0.541	8.676
VMO	0.791	0.671	0.572	0.655	0.948	0.788	8.667	0.568	0.647	0.934	0.685	0.542	8.448	0.478	8.646
VMR	0.580	0.755	0.965	1.039	1.026	0.575	0.743	0.950	1.0 23	1.0 10	8.484	0.510	8.645	0.700	0.687
VMRSR	0.798	0.678	0.577	0.655	0.949	8.797	0.676	0.573	8.647	0.934	8.746	0.600	8.474	0.460	0.639
VMSR	0.657	0.564	0.682	0.977	1.020	0.655	0.559	8.671	0.962	1.004	8.627	8.457	8.467	0.654	0.684
AM O	0.895	0.856	0.791	0.585	0.723	0.895	0.854	0.789	0.581	0.713	0.869	0.807	0.711	0.455	0.514
AMR	0.684	0.569	0.640	0.913	1.010	0.684	0.565	0.630	0.897	0.993	0.706	0.530	0.468	0.577	0.669
AMSR	0.855	0.778	0.678	0.562	0.860	0.855	8.777	0.676	0.556	0.846	0.837	0.741	0.614	0.420	0.582
AMRSR	0.746	0.604	0.565	0.800	0.991	0.746	0.603	0.559	0.785	0.975	0.754	0.588	8.472	0.514	0.656
HM O	0.926	0.920	0.915	0.906	0.900	0.926	0.920	0.915	0.906	0.900	0.924	0.918	0.913	0.904	0.897
HMR	0.627	0.602	0.825	1.0 24	1.025	0.625	0.594	0.812	1.007	1.008	0.591	0.445	0.549	0.689	0.686
HMSR	0.877	0.827	0.767	8.627	0.571	0.877	0.827	0.767	0.625	0.565	0.873	0.821	0.756	0.587	0.441
HMRSR	0.761	0.617	0.559	0.8 21	1.006	0.760	0.615	0.553	0.807	0.990	0.751	0.577	0.451	0.543	8.6 73
GMO	0.913	0.897	0.879	0.836	0.775	0.912	0.896	0.879	0.835	0.774	0.904	0.887	0.868	0.820	0.752
GMR	0.653	0.575	0.753	1.0 10	1.023	0.652	0.569	0.740	0.994	1,006	0.638	0.455	0.500	0.677	0.685
GM SR	0.867	0.807	0.735	0.589	0.610	0.867	0.807	0.734	0.586	0.602	0.859	0.794	0.713	0.523	0.433
GMRSR	0.729	0.583	0.585	0.910	1.017	0.729	0.580	0.578	0.895	1,000	0.722	0.531	0.438	0.602	0.681
MO	0.909	0.901	0.892	0.875	0.861	0.909	0.901	0.892	0.875	0.861	0.907	0.898	0.889	0.871	0.857
MR	0.658	0.576	0.775	1.0 18	1.024	0.657	0.569	0.763	1.001	1.007	0.631	0.446	0.518	0.684	0.686
MSR	0.865	0.811	0.746	8.687	0.583	0.864	0.810	0.745	0.605	0.576	0.861	0.804	0.732	0.558	0.435
MR SR	0.732	0.580	0.591	0.9 26	1.018	0.732	0.577	0.583	0.911	1.002	0.719	0.520	0.435	0.616	0.682

Appendix 4: MSE of OLS and Relative efficiency of the ridge parameter based on  $\hat{K}_{MAO}$ 

	n =10 p =3														
Method			$\sigma = 0$ .					$\sigma =$					$\sigma = 1$		
	0.8	0.9	0.95	0.99	0.999	0.8	0.9	0.95	0.99	0.999	0.8	0.9	0.95	0.99	0.999
M SE OLS	0.165	0.333	8.686	3.711	39.738	0.168	0.338	0.696	3.768	40.352	0.249	0.502	1.035	5,604	60.002
FMO	0.860	0.756	0.630	0.445	0.410	0.859	0.753	0.627	0.443	0.408	0.810	0.680	0.541	0.365	0.335
FMR	0.868	0.771	0.711	0.953	1.051	0.869	0.772	0.709	0.939	1.037	0.895	0.804	0.696	0.667	0.718
FM SR	0.863	0.756	0.625	0.454	0.617	0.862	0.755	0.623	0.451	0.611	0.838	0.714	0.567	0.369	0.455
FMR SR	0.867	8.762	0.658	0.8 22	1.039	0.867	0.762	0.656	0.811	1.0 24	0.880	0.777	0.643	0.581	0.708
VMO	0.707	0.591	0.543	0.676	0.965	0.706	0.588	0.539	0.669	0.952	0.667	0.526	0.447	0.500	0.670
VMR	0.868	0.771	0.711	0.953	1.051	0.869	0.772	0.709	0.939	1.037	0.895	0.804	0.696	0.667	0.718
VMSR	0.788	0.660	0.557	0.643	0.965	0.788	0.659	0.555	0.636	0.952	0.772	0.628	0.497	8.474	0.665
VMRSR	0.867	0.762	0.658	0.8 22	1.039	0.867	0.762	0.656	0.811	1.0 24	0.888	0.777	0.643	0.581	0.708
AMO	0.762	0.630	0.529	0.560	0.867	0.761	0.628	0.527	0.555	0.857	0.722	0.572	0.455	0.430	0.614
AMR AMSR	8.9 29	0.858	8.749	0.710	1.005	0.929	0.859	0.749	0.701	0.990	0.937	0.872	0.757	0.539	0.681
	0.818	8.694	0.573	0.583	0.923	0.817	0.693	0.571	0.577	0.911	0.799	0.661	0.519	0.440	0.640
AMRSR	0.901	0.813	8.691	0.661	0.989	0.902	0.813	0.690	0.653	0.974	0.906	0.818	0.683	0.494	0.672
HMO	0.801	0.675	0.552	0.425	0.420	0.800	0.673	0.549	0.423	0.418	0.751	0.605	0.473	0.346	0.339
HMR	0.910	0.8 28	0.730	0.875	1.047	0.911	0.828	0.729	0.862	1.033	0.925	0.852	0.737	0.628	0.714
HMSR	0.835	0.717	0.588	0.488	0.715	0.835	0.716	0.586	0.485	0.707	0.812	0.678	0.531	0.386	0.516
HMR SR GM O	0.878 0.782	8.777 8.651	8.653 8.536	0.691	1.009	0.878	0.777	0.652	0.682	0.995 0.643	0.881 0.737	0.778	0.635 0.461	0.506 0.382	0.688 0.486
GMR	0.78 2	0.651	0.736	0.481	1.036	0.780	0.649		0.478			0.588	0.461	0.382	0.486
GMSR	0.9 20	0.843	0.736	0.792	8.842	0.9 20	0.844	0.736 0.577	0.761	1.0 2 2 0.8 3 2	0.931 0.805	0.669	8.525	0.380	0.703
GMR SR	0.827	0.703	0.579	0.706	1.015	0.826	0.704	0.577	0.697	1.001	0.803	0.669	0.525	0.413	0.592
MO	0.896	0.643	0.535	0.706	0.678	0.896	0.804	0.682	0.697	0.672	0.728	0.580	0.676	0.318	0.691
MR	0.774	0.841	0.731	0.740	1.024	0.773	0.841	0.730	0.334	1.009	0.720	0.360	8.741	0.550	0.503
MSR	8.8 24	0.702	0.731	8.567	8.838	0.8 23	0.700	8.576	0.562	0.828	0.803	0.666	8.524	8.434	0.094
MRSR	0.896	0.702	0.683	0.679	1.008	0.896	8.885	8.682	0.671	0.994	0.903	0.812	8.676	0.502	0.551
MICSIC	0.050	0.003	0.003	0.015	1.000	0.000	n=40		0.071	0.334	0.502	0.012	0.070	0.302	0.003
M SE OLS	0.520	1.082	2.279	12.668	46.852	0.528	1.099	2.315	12.868	139.689	0.785	1.634	3.441	19.128	20 7.6 49
FMO	0.795	0.669	0.571	0.498	0.485	0.793	0.732	0.569	0.496	0.483	0.732	0,609	0.528	8.472	0.459
FMR	0.805	0.720	0.724	0.9.20	1.009	0.806	0.792	0.721	0.912	1.001	0.844	0.736	0.676	0.791	0.875
FMSR	8.797	8.6 78	0.567	0.521	0.664	8.796	0.735	0.565	0.518	0.660	0.766	0.634	0.535	0.480	0.589
FMRSR	0.802	8.694	8.6 59	0.833	1.000	0.802	0.763	0.656	0.826	0.992	8.822	0.699	0.618	8.716	0.867
VMO	0.588	0.633	8.721	0.878	0.968	0.585	0.691	0.716	0.872	0.961	0.545	0.563	0.632	0.768	0.846
VMR	0.805	0.720	8.724	0.920	1.009	0.806	0.792	0.721	0.912	1.001	0.844	0.736	0.676	0.791	0.875
VMRSR	8.657	0.585	0.608	0.788	0.958	0.656	0.641	0.605	0.782	0.950	8.642	0.548	0.546	0.687	8.834
VMSR	0.802	8.694	8.6 59	0.833	1.000	0.802	0.763	0.656	0.826	8.992	0.822	0.699	0.618	0.716	0.867
AMO	0.589	8.569	0.615	0.758	0.894	0.587	0.623	0.612	8.754	0.888	0.558	0.522	0.550	8.667	0.786
AMR	0.943	0.876	8.758	0.653	0.950	0.943	0.963	0.758	0.649	0.943	0.945	0.879	0.757	0.580	0.817
AMSR	0.684	0.590	0.581	0.721	0.919	0.683	0.647	0.578	0.717	0.913	0.670	0.561	0.530	0.631	0.801
AMRSR	0.889	0.786	8.664	0.665	0.946	0.889	0.864	0.664	0.661	0.939	0.890	0.785	0.650	0.583	0.816
HMO	0.630	0.545	0.513	0.513	0.525	0.628	0.596	0.511	0.511	0.523	0.590	0.507	0.478	0.476	0.484
HMR	0.914	0.8 21	0.726	0.828	1.005	0.914	0.903	0.726	0.821	0.997	0.925	0.834	0.710	0.711	0.871
HMSR	0.716	0.602	0.547	0.598	0.773	0.715	0.660	0.545	0.594	0.768	0.694	0.573	0.511	0.536	0.677
HMRSR	0.835	0.716	8.627	0.730	0.972	0.835	0.786	0.626	0.724	0.965	0.838	0.712	0.598	0.632	0.842
GMO	0.599	0.550	0.566	0.664	0.765	0.598	0.602	0.563	0.660	0.760	0.568	0.510	0.516	0.591	0.672
GMR	0.932	0.852	0.728	0.729	0.991	0.933	0.937	0.728	0.724	0.984	0.938	0.860	0.726	0.632	0.858
GMSR	0.696	0.593	8.566	8.675	0.866	0.695	0.650	0.563	0.670	0.860	0.679	0.565	0.522	0.594	0.753
GMR SR	0.880	8.771	0.656	0.707	0.974	0.880	0.848	0.655	0.702	0.966	0.884	0.772	0.639	0.614	0.843
MO	0.583	0.563	0.589	0.687	0.774	0.581	0.616	0.586	0.683	0.769	0.553	0.520	0.534	0.614	0.673
MR	0.945	0.8 73	8.747	0.705	0.987	0.945	0.960	0.746	0.700	0.979	0.948	0.876	0.741	0.613	0.854
MSR	0.679	0.588	0.572	0.687	0.867	0.678	0.645	0.570	0.682	0.860	0.664	0.560	0.527	0.605	0.751
MRSR	0.891	0.786	0.663	0.695	0.971	0.891	0.864	0.662	0.690	0.964	0.893	0.785	0.645	0.604	0.841
Note: Proposed techniques are bolded.															