

Some Results on Point-Line Trajectories in Lorentz 3-space

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(Communicated by Murat Tosun)

ABSTRACT

In this paper, we study curvature theory of point-line trajectories in Lorentz 3-space. We give the characterization by indicatrix, directrix and their relationship in Lorentz 3-space. We use this characterization and relationship to depict a point-line trajectory.

Keywords: Curvature; Directrix; Indicatrix; Point-line trajectories; Lorentzian 3-space.

AMS Subject Classification (2010): 53A04 ; 53A25; 53A40.

1. Introduction

Point-line trajectory is a very commonly encountered topic in many industrial applications such as welding, cutting, painting, milling, screwing and instrument probing. Point-line trajectory is used as a tool to trace a path with the tool axis oriented in a certain direction while the rotation about the axis is irrelevant, [13].

There are many studies dealing with the curvature theory of line trajectory [1, 2, 3, 4, 5, 6, 7]. One of these studies is presented by McCarthy and Roth [6]. Then, Ryuh and Pennock [10] carried out this theory to trajectory planing of robot end-effectors. They studied directrix and the trajectory of the tool center point. But, the relationship and coordination between the directrix and indicatrix are given by Ting and friends [13]. For detailed information, see [2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 1].

This study is related with relationship and coordination between the directrix and indicatrix in Lorentz 3-space and presents curvature theory of point-line trajectories in Lorentz 3-space. We investigate Ting and friends', [13], results in Lorentz 3-space.

2. Setting and Notations

Let \mathbb{E}_1^3 be Lorentz 3-space with the inner product

$$\langle u, v \rangle = -u_1 v_1 + u_2 v_2 + u_3 v_3$$

and the vector product

$$u \times v = \left(- \begin{vmatrix} u_2 & u_3 \\ v_2 & v_3 \end{vmatrix}, \begin{vmatrix} u_3 & u_1 \\ v_3 & v_1 \end{vmatrix}, \begin{vmatrix} u_1 & u_2 \\ v_1 & v_2 \end{vmatrix} \right),$$

where $u = (u_1, u_2, u_3)$, $v = (v_1, v_2, v_3) \in \mathbb{E}_1^3$, [8].

Definition. A vector u in \mathbb{E}_1^3 is said to be spacelike if $\langle u, u \rangle > 0$ or $u = 0$, timelike if $\langle u, u \rangle < 0$, lightlike or null if $\langle u, u \rangle = 0$ and $u \neq 0$. We define the signature of a vector u as

$$\varepsilon = \begin{cases} 1, & u \text{ is spacelike} \\ 0, & u \text{ is lightlike} \\ -1, & u \text{ is timelike.} \end{cases}$$

The norm of a vector $u \in \mathbb{E}_1^3$ is defined by $\|u\| = \sqrt{|\langle u, u \rangle|}$, [8].

3. Characterization by Indicatrix, Directrix and Their Relationship

A point-line trajectory with a one parameter motion is a patch on a ruled surface that can be denoted as a two dimensional set of points defined by the succeeding equation

$$X(t, \psi) = r(t) + \psi R(t) \tag{3.1}$$

where t is an independent parameter, $r(t)$ and $R(t)$ are respectively, the directrix and indicatrix of the point-line trajectory and ψ is also an independent parameter indicating a physical point on the point-line determined by $r(t)$ and $R(t)$.

The *indicatrix* of a point-line trajectory in Lorentz 3-space can be acted as a spherical curve $R(t)$ on a unit pseudo sphere S_1^2 in \mathbb{E}_1^3 . Let s_R be the arc length of the spherical curve

$$s_R = \int_0^t \langle \dot{R}, \dot{R} \rangle^{1/2} dt. \tag{3.2}$$

The unit spacelike tangent vector T to the indicatrix is given by the derivative of R with respect to s_R is

$$R' = T. \tag{3.3}$$

Let $K = R \times T$ be a timelike vector, the three mutually orthogonal unit vectors $[R, T, K]$ define a geodesic trihedron and denoted by $[R]$. The first order derivative of $[R]$ with respect to s_R is

$$\begin{bmatrix} R' \\ T' \\ K' \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ -1 & 0 & \gamma_R \\ 0 & \gamma_R & 0 \end{bmatrix} \begin{bmatrix} R \\ T \\ K \end{bmatrix}, \tag{4}$$

where γ_R is the geodesic curvature.

Unit timelike vector N of $R(t)$ represents the direction of T' . Let $B = -T \times N$ be a spacelike vector and called binormal of $R(t)$. The three mutually orthogonal unit vectors $[T, N, B]$ define a natural trihedron and denoted by $[T]$. Their derivative relations are given as

$$\begin{bmatrix} T' \\ N' \\ B' \end{bmatrix} = \begin{bmatrix} 0 & \kappa_R & 0 \\ \kappa_R & 0 & \tau_R \\ 0 & \tau_R & 0 \end{bmatrix} \begin{bmatrix} T \\ N \\ B \end{bmatrix}, \tag{5}$$

where curvature κ_R and torsion τ_R characterize completely differential properties of the indicatrix up to the third order. Since $R(t)$ stays on a unit pseudo sphere, from [14], it can be proved that

$$\tau_R = \pm \frac{\kappa_R'}{\kappa_R \sqrt{1 \pm \kappa_R^2}} \tag{6}$$

and κ_R and γ_R have the following relationship

$$\kappa_R^2 = \pm(\gamma_R^2 - 1). \tag{7}$$

The relationship between geodesic trihedron $[R]$ and natural trihedron $[T]$ can be expressed as

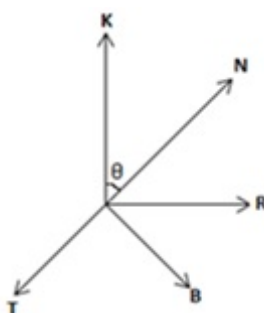
$$\begin{bmatrix} T \\ N \\ B \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 \\ \sinh \theta & 0 & \cosh \theta \\ \cosh \theta & 0 & \sinh \theta \end{bmatrix} \begin{bmatrix} R \\ T \\ K \end{bmatrix}, \tag{8}$$

where θ is referred to as the hyperbolic angle. (See Figure 1.) From equations (4) and (5), we have

$$\sinh \theta = -\frac{1}{\kappa_R} \text{ and } \cosh \theta = \frac{\gamma_R}{\kappa_R}. \tag{9}$$

In some cases it may be desirable the derivatives according to t . So, the derivatives of $R(t)$ are obtained as

$$\dot{R} = \frac{dR}{dt} = \gamma T, \tag{10}$$


 Figure 1. Trihedrons $[R]$ and $[T]$ and the hyperbolic angle

$$\ddot{R} = \dot{\gamma}T + \gamma^2 \kappa_R N, \quad (11)$$

$$\ddot{R} = (\ddot{\gamma} + \gamma^3 \kappa_R^2)T + (3\dot{\gamma}\gamma\kappa_R + \gamma^3 \kappa_R')N + \gamma^3 \kappa_R \tau_R B. \quad (12)$$

Here, $\gamma = \frac{ds_R}{dt}$ is speed of the indicatrix or the angular velocity of the point-line motion.

The directrix of a point-line trajectory is a spacelike curve denoted by $r(t)$. Let s_r refer to the arc length of the directrix,

$$s_r = \int_0^t \langle \dot{r}, \dot{r} \rangle^{1/2} dt \quad (13)$$

and the derivatives of a variable with respect to s_r in the context of directrix be denoted by a superscript prime. The unit spacelike tangent vector \mathbf{t} of the directrix, with respect to s_r :

$$r' = \mathbf{t}. \quad (14)$$

Therefore, the Frenet relations of $r(t)$ can be written as

$$\begin{bmatrix} \mathbf{t}' \\ \mathbf{n}' \\ \mathbf{b}' \end{bmatrix} = \begin{bmatrix} 0 & \kappa_r & 0 \\ \kappa_r & 0 & \tau_r \\ 0 & \tau_r & 0 \end{bmatrix} \begin{bmatrix} \mathbf{t} \\ \mathbf{n} \\ \mathbf{b} \end{bmatrix}, \quad (15)$$

where \mathbf{t} , \mathbf{n} , \mathbf{b} are the unit spacelike tangent, timelike normal and spacelike binormal vectors of $r(t)$ and κ_r and τ_r are the curvature and torsion of $r(t)$. Let us denote the unit vectors \mathbf{t} , \mathbf{n} and \mathbf{b} as $[t]$.

The derivatives of $r(t)$ with respect to t can be expressed as follows;

$$\dot{r} = \frac{dr}{dt} = v\mathbf{t}, \quad (16)$$

$$\ddot{r} = \dot{v}\mathbf{t} + v^2 \kappa_r \mathbf{n}, \quad (17)$$

$$\ddot{r} = (\ddot{v} + v^3 \kappa_r^2)\mathbf{t} + (3v\dot{v}\kappa_r + v^3 \kappa_r')\mathbf{n} + v^3 \kappa_r \tau_r \mathbf{b}, \quad (18)$$

where $v = \frac{ds_r}{dt}$ is the speed of the directrix.

In the text which follows, we will treat the relationship between the directrix and indicatrix curves.

The directrix and indicatrix have been characterized separately up to now. To completely characterize a point-line trajectory, we must also regard the relationship between the directrix and indicatrix.

The relation between the arc lengths s_R and s_r is shown by

$$\xi = \frac{ds_r}{ds_R}, \quad (19)$$

where ξ is referred to as the velocity ratio. Accordingly, the speed of the directrix and its derivatives can be given as follows

$$v = \xi\gamma, \quad (20)$$

$$\dot{v} = \xi'\gamma^2 + \xi\dot{\gamma}, \quad (21)$$

$$\ddot{v} = \xi''\gamma^3 + 3\xi'\gamma\dot{\gamma} + \xi\ddot{\gamma}, \quad (22)$$

where $\xi' = \frac{d\xi}{ds_R}$ and $\xi'' = \frac{d^2\xi}{ds_R^2}$.

4. Coordination of Directrix and Indicatrix

From the point trajectory, the $\{\mathbf{t}, \mathbf{n}, \mathbf{b}\}$ trihedron and the characteristic numbers characterizing the directrix can be determined. To coordinate the direction of the point-line axis with the indicatrix up to the second order, the required characteristic numbers $a_{\mathbf{t}T}$, κ_R , ξ , and ξ' need to be determined, [13].

The orientation of the point-line axis with respect to the point trajectory is characterized by parameters $a_{\mathbf{t}R}$ and $a_{\mathbf{n}R}$. If such a directional relationship is to remain unchanged, $a_{\mathbf{t}R}$ and $a_{\mathbf{n}R}$ must be constant. Since $a_{\mathbf{t}R} = R \cdot \mathbf{t}$ and $a_{\mathbf{n}R} = R \cdot \mathbf{n}$ where R is the unit spacelike vector along the point-line axis, taking the derivatives over the conditions that $a_{\mathbf{t}R}$ and $a_{\mathbf{n}R}$ are constant yields

$$\dot{R} \cdot \mathbf{t} + R \cdot \dot{\mathbf{t}} = 0, \tag{23}$$

$$\dot{R} \cdot \mathbf{n} + R \cdot \dot{\mathbf{n}} = 0. \tag{24}$$

From equations (10), (15) and (19) the above two equations can be rewritten as, respectively,

$$a_{\mathbf{t}T} + \xi \kappa_r a_{\mathbf{n}R} = 0 \tag{25}$$

and

$$a_{\mathbf{n}T} + \xi \kappa_r a_{\mathbf{t}R} + \xi \tau_r a_{\mathbf{b}R} = 0. \tag{26}$$

Equations (23) and (24) or (25) and (26) are the conditions for the point-line axis to maintain a consistent direction with respect to the directrix up to the first order.

Let $T = (T_x, T_y, T_z)$, $\mathbf{t} = (t_x, t_y, t_z)$, $\mathbf{n} = (n_x, n_y, n_z)$ and if we exchange them into equations (25) and (26), we get

$$\begin{aligned} t_x T_x + t_y T_y + t_z T_z + \xi \kappa_r a_{\mathbf{n}R} &= 0, \\ n_x T_x + n_y T_y + n_z T_z + \xi \kappa_r a_{\mathbf{t}R} + \xi \tau_r a_{\mathbf{b}R} &= 0. \end{aligned}$$

Unifying the above two equations with the constraints on the magnitude and direction of T ,

$$T_x^2 + T_y^2 + T_z^2 = 1$$

and

$$R \cdot T = 0 \text{ and } R_x T_x + R_y T_y + R_z T_z = 0,$$

where $R = (R_x, R_y, R_z)$, T and ξ can be solved. If we solve this equation systems, we get T and ξ as below,

$$\begin{aligned} \xi &= \frac{|c_0|}{\sqrt{c_1^2 + c_2^2 + c_3^2}} \\ T_x &= \pm \frac{c_1}{\sqrt{c_1^2 + c_2^2 + c_3^2}}, T_y = \pm \frac{c_2}{\sqrt{c_1^2 + c_2^2 + c_3^2}}, T_z = \pm \frac{c_3}{\sqrt{c_1^2 + c_2^2 + c_3^2}}, \end{aligned}$$

where

$$\begin{aligned} c_0 &= -t_x n_z R_y + t_x n_y R_z - t_y n_x R_z + t_y n_z R_x - t_z n_y R_x + t_z n_x R_y, \\ c_1 &= -a_{\mathbf{t}R} \kappa_r R_y t_z - a_{\mathbf{b}R} \tau_r R_y t_z + a_{\mathbf{n}R} \kappa_r R_y n_z + a_{\mathbf{t}R} \kappa_r R_z t_y \\ &\quad + a_{\mathbf{b}R} \tau_r R_z t_y - a_{\mathbf{n}R} \kappa_r R_z n_y, \\ c_2 &= a_{\mathbf{n}R} \kappa_r R_z n_x + a_{\mathbf{t}R} \kappa_r R_x t_z + a_{\mathbf{b}R} \tau_r R_x t_z - a_{\mathbf{n}R} \kappa_r R_x n_z \\ &\quad - a_{\mathbf{t}R} \kappa_r R_z t_x - a_{\mathbf{b}R} \tau_r R_z t_x, \\ c_3 &= -a_{\mathbf{n}R} \kappa_r R_y n_x - a_{\mathbf{t}R} \kappa_r R_x t_y - a_{\mathbf{b}R} \tau_r R_x t_y + a_{\mathbf{n}R} \kappa_r R_x n_y \\ &\quad + a_{\mathbf{t}R} \kappa_r R_y t_x + a_{\mathbf{b}R} \tau_r R_y t_x. \end{aligned}$$

If we take the derivative over equations (23) and (24), we have

$$\ddot{R} \cdot \mathbf{t} + 2\dot{R} \cdot \dot{\mathbf{t}} + R \cdot \ddot{\mathbf{t}} = 0, \tag{27}$$

$$\ddot{R} \cdot \mathbf{n} + 2\dot{R} \cdot \dot{\mathbf{n}} + R \cdot \ddot{\mathbf{n}} = 0. \tag{28}$$

With equations (10), (11), (15) and (19) – (21) the above equations can be rewritten as

$$\frac{1}{\xi}(\dot{v} - \gamma^2 \xi') a_{tT} + \gamma^2 \kappa_R a_{tN} + 2\gamma v \kappa_r a_{nT} + (\dot{v} \kappa_r + v^2 \kappa_r') a_{nR} + v^2 \kappa_r^2 a_{tR} + v^2 \kappa_r \tau_r a_{bR} = 0, \quad (29)$$

$$\frac{1}{\xi}(\dot{v} - \gamma^2 \xi') a_{nT} + \gamma^2 \kappa_R a_{nN} + 2\gamma v (\kappa_r a_{tT} + \tau_r a_{bT}) + \dot{v} (\kappa_r a_{tR} + \tau_r a_{bR}) + v^2 (\kappa_r' a_{tR} + \kappa_r^2 a_{nR} + \tau_r' a_{bR} + \tau_r^2 a_{nR}) = 0. \quad (30)$$

κ_R and ξ' can be solved from the above two equations. If we solve these equations, we get

$$\xi' = \frac{\begin{vmatrix} c_6 & c_5 \\ c_9 & c_8 \end{vmatrix}}{\begin{vmatrix} c_4 & c_5 \\ c_7 & c_8 \end{vmatrix}} \text{ and } \kappa_R = \frac{\begin{vmatrix} c_4 & c_6 \\ c_7 & c_9 \end{vmatrix}}{\begin{vmatrix} c_4 & c_5 \\ c_7 & c_8 \end{vmatrix}}$$

where

$$\begin{aligned} c_4 &= -\frac{\gamma^2 a_{tT}}{\xi}, \quad c_5 = \gamma^2 a_{tN}, \\ c_6 &= -\frac{\dot{v} a_{tT}}{\xi} - 2\gamma v \kappa_r a_{nT} - (\dot{v} \kappa_r + v^2 \kappa_r') a_{nR} - v^2 \kappa_r^2 a_{tR} - v^2 \kappa_r \tau_r a_{bR}, \\ c_7 &= -\frac{\gamma^2 a_{nT}}{\xi}, \quad c_8 = \gamma^2 a_{nN}, \\ c_9 &= -\frac{\dot{v} a_{nT}}{\xi} - 2\gamma v (\kappa_r a_{tT} + \tau_r a_{bT}) - \dot{v} (\kappa_r a_{tR} + \tau_r a_{bR}) \\ &\quad - v^2 (\kappa_r' a_{tR} + \kappa_r^2 a_{nR} + \tau_r' a_{bR} + \tau_r^2 a_{nR}). \end{aligned}$$

5. Conclusions

This paper gives the properties of the curvature theory of point-line trajectories in Lorentzian 3-space. We have shown that the relation between the curvature and geodesic curvature of indicatrix. The relation between the direction and indicatrix curves are given.

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