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ESTIMATING THE EARTHQUAKE SOURCE PARAMETERS: SIMULATED ANNEALING VERSUS NELDER-MEAD SIMPLEX ALGORITHM

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ABSTRACT. The parameter estimation is an important process in many earth science problems in order to define the features of ground movement. It is clear that the model nonlinearity makes the estimation of parameters more difficult and more challenging. In this case, metaheuristic algorithms and derivative free optimization methods are more proper than classical optimization methods. In this study, Simulated Annealing (SA), a well known metaheuristic algorithm, and Nelder-Mead simplex algorithm, a derivative free optimization method, are used to estimate the earthquake source parameters. The algorithms are applied on a synthetically generated data set. The estimated parameter results show that the SA is better than Nelder-Mead simplex method.

1. INTRODUCTION

An earthquake is defined by source parameters. Modeling of the source parameters requires wide knowledge of elastic half space theory due to the elastic structure of the crust. Many past attempts to infer source geometry from deformation fields have used elasticity theory to find geologically plausible models that fit the major features of the observed deformation field. The fault plane is used to determine surface displacements on definite coordinates. The correct estimation of source parameters gives good predictions for the next earthquake occurance. In this case, the estimation of the fault plane parameters becomes important as modeling. Many new methodologies have been developed in the field of estimating the source parameters [9, 11, 20, 22]. Derivative based searching algorithms; e.g., a Quasi-Newton method [6], derivative free optimization algorithms; e.g., Nelder-Mead simplex algorithm [5, 15], heuristic optimization methods; e.g., SA algorithm [2, 3, 7, 21] and genetic algorithms [8, 18], Monte-Carlo methods [26] are used for the estimation of crust model parameters.

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In this study, SA algorithm is used to estimate the earthquake source parameters using analitical solution for deformation. The SA algorithm is a random search method based on the analogy between cooling and the freezing of the metals and some liquid materials at crystal structure with minimum energy and researching the minimum of a general system. The SA is based upon that of [24], which was originally proposed as a means of finding the equilibrium configurations of a collection of atoms at a given temperature. Kirkpatrick [19] was first proposed the algorithm basis of an optimization technique for combinatorial problems. The SA permits the efficient period for the dispersion of the molecules again by decreasing the temperature gradually. Thus, the method can be considered as a minimization algorithm based on natural events and nature. Also the SA is a stochastic computational method with quick approximations to global solutions for hard optimization problems in different fields [10, 13, 28, 16, 17, 27, 30, 31]. The SA algorithm has advantages in dealing with the strong nonlinearities and discontinuities in the hilly structure of cost function. This paper describes the SA algorithm and explores its ability to optimize NP-hard functions in geosciences through an efficient exploration of the parameter space. And also the paper gives a comparison for parameter estimation with a derivative free optimization method, called Nelder-Mead simplex method [25]. The synthetically generated data set is used for the application. All the calculations are done by using Matlab.

The rest of the paper is organized as follows: In Section 2 fault plane geometry is showed and inverse problem formulation is presented. In the next section the SA algorithm is briefly reviewed and the implementation of SA algorithm to fault plane parameter estimation procedure is given. This is followed by simulation results that illustrates the both proposed approaches via the Monte Carlo simulation. In the last part, numerical results of the estimations are compared and the performance of the optimization algorithms is analyzed.

2. FAULT PLANE MODEL AND INVERSE PROBLEM FORMULATION

2.1. The fault plane geometry. The fault plane parameters play an important role for defining the characteristics of surface displacements. It is a hard work to estimate earthquake source parameters and it requires a well defined model. The most commonly used crustal model is the homogeneous, isotropic, linear, and elastic half-space. In spite of its limitations, the elastic half space model is widely used because of the simplicity of the expressions [7]. Figure 1 illustrates the fault plane geometry in three dimensions.



Figure 1. The fault geometry and the relocation on the fault

The paran	nete	ers defined on the fault plane in Figure 1 are
l	:	the lenght of the fault plane (km),
w	:	the wideness of the fault plane (km),
d	:	the depth of the fault plane (km),
δ	:	dip angle (radian),
α	:	strike (radian),
(xf, yf)	:	the coordinates of the fault starting point where xf (km) is
		east ofset and yf (km) is north ofset,
SS	:	the component of the slip vector (S) in the direction of the fault $(Strike Slip)$ (m)
		of the fault (Strike-Shp) (m), $(\Omega) = 0$
DS	:	the component of the slip vector (5) as vertical to $(1 - 1)^{1/2}$
<i>(</i>)		the fault direction (Dip-Slip) (m),
(x_0, y_0)	:	the location of the fault center defined on the surface.

In this study, a plate model, which is expressed by Aktuğ [4], is considered because of its simplicity and speed in computing. In the model surface relocations, caused by the slip vector, is defined as analitical equations for quadrangular area. The slip is consist of two components such as "lateral range" in the direction of the fault plane and the "vertical range" as vertical to lateral range. The both range functions are given below:

Lateral range :

$$u_x = -\frac{u_1}{2\pi} \left(\frac{\xi q}{R(R+\eta)} + \tan^{-1} \frac{\xi \eta}{qR} + I_1 \sin \delta \right)$$
$$u_y = -\frac{u_1}{2\pi} \left(\frac{y'q}{R(R+\eta)} + \frac{q\cos\delta}{R+\eta} + I_2 \sin\delta \right)$$
$$u_z = -\frac{u_1}{2\pi} \left(\frac{d'q}{R(R+\eta)} + \frac{q\sin\delta}{R+\eta} + I_4 \sin\delta \right)$$

Vertical range :

$$u_x = -\frac{u_2}{2\pi} \left(\frac{q}{R} + I_1 \sin \delta \cos \delta \right)$$

$$u_y = -\frac{u_2}{2\pi} \left(\frac{y'q}{R(R+\eta)} + \cos \delta \tan^{-1} \frac{\eta x}{R+\eta} - I_1 \sin \delta \cos \delta \right)$$

$$u_z = -\frac{u_2}{2\pi} \left(\frac{y'q}{R(R+\xi)} + \sin \delta \tan^{-1} \frac{\xi \eta}{qR} - I_5 \sin \delta \cos \delta \right)$$

where the I_1, I_2, I_3, I_4, I_5 are analitical equations and contain source parameters. These equations are consist of nonlinear combinations of the fault plane parameters. The reader is referred to the works by [4] for a detailed description of parameters. The equation systems, given above with lateral and vertical ranges, show the functional relations between the fault geometry and surface displacements. Because of the nonlinearity of these complex analitical functions, classical parameter estimation methods may fail. In this case, estimation of fault plane parameters by the SA algorithm makes certain facilities to get global solutions; e.g. providing sufficient convergence, escaping local traps, easy implementation to real world NP hard optimization problems.

2.2. **Inverse problem formulation.** One of the main aim of geophysical inversion is to identify the all models which give an acceptable loss between predicted and observed data. In terms of the loss function, a measure of the difference between observed and synthetic data that varies as a function of solution parameters [23]. In this study, the inversion problem, which describes the geometry and the slip of the fault plane, is formed with analitical lateral and vertical range equations.

Let **p** be the nine dimensional vector whose elements p_j are the geometrical source parameters wanted to be estimated denoted by $\mathbf{p} \equiv [l \ w \ d \ \delta \ \alpha \ xf \ yf \ SS \ DS]$. Let $\mathbf{g} \equiv \mathbf{g}(\mathbf{p}) \equiv [\mathbf{g}_1 \ \mathbf{g}_2 \ \cdots \ \mathbf{g}_N]$ be the *N*-dimensional vector whose *i*th element $\mathbf{g}_i, i = 1, 2, ..., N$ is the surface relocation vector with three dimensions (x, y, z)at the *i*th observation point. Therefore, the observed surface displacements \mathbf{u} can be written as a function \mathbf{g} of the fault model parameters \mathbf{p}

$$\mathbf{u} = \mathbf{g}\left(\mathbf{p}\right) + \mathbf{e} \tag{2.1}$$

where **e** is a vector of observational errors. The surface relocation vector **u** consists of two components as in the lateral direction, $\mathbf{u}^l = [u_x^l, u_y^l, u_z^l]$ and in the vertical direction, $\mathbf{u}^v = [u_x^v, u_y^v, u_z^v]$. Thus, the equation 2.1 can be written as

$$u_{ij} = g_{ij}(\mathbf{p}) + e_{ij}$$
, $i = 1, 2, ..., 50$, $j = x, y, z.$ (2.2)

The surface displacements are related nonlinearly to the fault plane parameters as seen from the lateral and vertical equations. Hence, the estimation of the fault plane parameters becomes to a nonlinear optimization problem. Estimating \mathbf{p} from \mathbf{g} is formulated as the minimization of the function f given

$$f\left(\mathbf{u},\mathbf{g}\right) = \left\|\mathbf{u} - \mathbf{g}\left(\mathbf{p}\right)\right\|_{2} \tag{2.3}$$

where $\|\cdot\|$ is the Euclidean norm. The optimal parameter values \mathbf{p}^* minimize the L_2 norm of the loss function given by 2.3, which is considered as an objective function [29]. Therefore, the nonlinear unconstrained optimization problem can be written as

$$\min_{\mathbf{p} \in S} f(\mathbf{u}, \mathbf{g}) \tag{2.4}$$

where S is the domain of parameters.

The analytical solution of the problem seems to be unavailable because of the nonlinearity of fault plane model. The size of parameter space, the existence of local minima, the continuity of objective function and the sensitivity of objective function to each of the model parameters must be considered. In order to solve the inverse problem commonly used techniques such as simple Monte Carlo methods become inefficient or impractical in very large solution spaces. More recently a number of guided search techniques from the field of artificial intelligence and heuristic methods have been developed. In this study, SA is used to estimate the overall earthquake geometry using the optimization problem given with lateral and vertical equations.

3. Application of the SA algorithm to the estimation problem

The SA algorithm derives its name from an analogy to the cooling of metals. As a metal cools, the atoms fluctuate between relatively higher and lower energy levels. If the temperature is dropped slowly enough, the atoms will all reach their ground state. This cooling process is called as "annealing". However, if the temperature is dropped too quickly, the system will get trapped in a less than optimum configuration. So the temperature is considered as the control parameter in the method. If the energy function of this physical system is instead replaced by an objective function, then the progression of this function towards the global minimum is analogous to the physical progression towards the ground state.

Convenience of application to real world problems and obtainment of good solutions makes the SA algorithm be one of the most powerful and popular heuristics to solve many optimization problems. Some factors need to be considered when designing the SA algorithm. The following elements must be provided for implementing the SA to a problem:

- (i) are presentation of possible solutions,
- (ii) a generator of random changes in solutions,
- (iii) a means of evaluating the probability functions, and
- (iv) an annealing schedule, an initial temperature and rules for lowering it as the search progresses[1].

The optimization problem given in equation 2.4 will be minimized to estimate the nine fault plane parameters with the SA algorithm. The algorithm has two cycles, inner and outer. A neighboring parameter set of the current parameter set is generated, in the inner cycle of the algorithm. If the new state is better than the current state then the generated solution replaces the current solution, otherwise the solution is accepted with a criterion probability. The value of the temperature, control parameter, decreases in each iteration of the outer cycle of the algorithm. In this regard, the steps of this algorithm are briefly looked into:

Step 1: T_0 is chosen as the initial temperature, \mathbf{p}_0 is chosen arbitrarily as an initial parameter set on the definition space, n is the dimension of fault parameter set, T_{\min} is chosen as the final temperature (stopping criteria of outer cycle), L is chosen as the number of neighborhood solutions generated at a certain temperature T to get equilibrium (stopping criteria of inner cycle), \mathbf{a} and \mathbf{b} are chosen lower and upper bound sets for parameters respectively. Firstly, the initial temperature is considered as the system temperature, $T_k = T_0$ for k = 0 and optimal parameter value \mathbf{p}^* is set to \mathbf{p}_0 , $\mathbf{p}^* = \mathbf{p}_0$.

Step 2: Under kth temperature, if the inner loop condition is met, go to Step 3; otherwise the new parameter set is produced at a given temperature as

$$\mathbf{p}_{j+1} = \mathbf{p}_j + \mathbf{y} \left(\mathbf{b} - \mathbf{a} \right) \quad , \quad \mathbf{y} \in \operatorname{rand} \left(-1, 1 \right) \tag{3.1}$$

where, **p** is constrained by $\mathbf{p} \in [\mathbf{a}, \mathbf{b}]$. Later on, the new function value $f(\mathbf{p}_{j+1}) = f_{j+1}$ and $\Delta f = f_{j+1} - f_j$ are computed. If $\Delta f < 0$, the new state is accepted. Otherwise, the Metropolis criterion is followed to accept \mathbf{p}_{j+1} with a probability of $\min\left(1, e^{-\frac{\Delta f}{T_k}}\right)$ and Step 2 continues.

Step 3: The temperature is reduced according to a specified cooling schedule, $T_k = T_0 c^k$, 0 < c < 1, where c is analogous to the Boltzmann's constant that can be used to tune the algorithm. If outer loop break condition is met computation stops and optimal parameter set is reached. Otherwise, Step 2 is repeated.

The definition of the starting temperature, the cooling schedule of the temperature, the iteration number at each temperature and the definition of the stopping criteria have great roles in the efficiency of the algorithm [12]. Various SA algorithms are based on the same principle explained above, e.g., Boltzmann annealing [19], fast simulated annealing [28], very fast simulated annealing [16], and adaptive simulated annealing [17]. These algorithms vary in probability distribution, annealing schedule, and the generation methods of random change. In this study, geometric cooling schedule is chosen and applied to earthquake source parameter estimation scheme.

4. Numerical Example

In this section, a numerical example is used to investigate the performance of the SA algorithm. An operation region is defined for performing the simulated data. The surface relocations, taken as outputs of the estimation scheme, are generated on the experimental region for defined coordinates using Matlab code. It is tried to get the optimal values of fault plane parameters. In the conclusion part of the simulation study, SA and Nelder-Mead simplex algorithm are compared in terms of their convergency to optimal value of nine source parameters.

4.1. **Data.** An operation region, a quadrangular area, is defined for performing simulated data and considered as a definite place of earth surface where earthquake has been occured. The simulated earthquake area is formed in $(-30, 20) \times (-50, 20)$ coordinates with 50 geodetic points which are signed on the graph given in Figure 2.



Figure 2. Defined 50 coordinates around the fault direction

As can be seen from the Figure 2 that the fault direct, passed along the origin with a straight line, is formed and 50 random generated coordinate values (x, y) are fixed around the fault direction. The surface relocations, denoted as [x, y, z], are generated by using Matlab code taken from the geodynamics laboratory page (http:// www.gpsg.mit.edu) of the Massachusetts Technology Institute for each coordinate. The fixed 50 coordinates and the surface relocations are given in Table 1. The fault plane parameters, used for synthetic data set and the lower and the upper bounds of the parameters are presented in Table 2.

Number of	Coordinates of the locations	Surface relocations on defined	Number of	Coordinates of the locations	Surface relocations on defined		
locations on the surface		coordinates	locations	on the surface	coordinates		
	(x_0, y_0)	(u_x, u_y, u_z)		(x_0, y_0)	(u_x, u_y, u_z)		
1	(2,-34)	(-0.1275 0.2515 -0.1019)	26	(-20, -15)	(0.0098 0.1118 -0.0765)		
2	(-3,9)	(-0.0014 0.0541 -0.0307)	27	(-17, -20)	(0.0128 0.1496 -0.1237)		
3	(-20, 1)	(0.0009 0.0625 -0.0362)	28	(-15, -26)	(0.0101 0.1950 -0.2330)		
4	(4,-1)	(-0.0044 0.0680 -0.0393)	29	(11, 14)	(-0.0020 0.0417 -0.0222)		
5	(-18, -23)	(0.0270 0.1681 -0.1532)	30	(-9,-39)	(-0.3500 0.7122 -0.2765)		
6	(6, -16)	(-0.0197 0.1046 -0.0600)	31	(-4,-23)	(-0.0339 0.1756 -0.1282)		
7	(-10, 18)	(-0.0008 0.0423 -0.0231)	32	(16, 18)	(-0.0020 0.0355 -0.0183)		
8	(-10,5)	(-0.0010 0.0611 -0.0357)	33	(-11, -45)	(-0.6662 1.0287 -0.1170)		
9	(-9, -21)	(-0.0153 0.1673 -0.1380)	34	(2, -28)	(-0.0680 0.1887 -0.1022)		
10	(-23, 17)	(-0.0001 0.0385 -0.0204)	35	(-21, -41)	(0.0294 -0.7021 1.0330)		
11	(14,-36)	(-0.1098 0.1485 -0.0293)	36	(9, -42)	(-0.1974 0.2469 -0.0338)		
12	(-29, -13)	(0.0144 0.0736 -0.0367)	37	(-12, -38)	(-0.4933 0.9630 -0.4768)		
13	(16, -15)	(-0.0218 0.0749 -0.0350)	38	(9, -43)	(-0.2121 0.2581 -0.0308)		
14	(2, -16)	(-0.0173 0.1154 -0.0716)	39	(-13, -13)	(0.0001 0.1155 -0.0820)		
15	(-27, -24)	(0.0491 0.1241 -0.0519)	40	(9,3)	(-0.0041 0.0562 -0.0309)		
16	(2, -14)	(-0.0139 0.1073 -0.0664)	41	(-23, -21)	(0.0309 0.1325 -0.0877)		
17	(8,7)	(-0.0029 0.0515 -0.0283)	42	(-23,8)	(0.0005 0.0484 -0.0264)		
18	(8,-35)	(-0.1184 0.1944 -0.0574)	43	(2,6)	(-0.0023 0.0569 -0.0323)		
19	(10, -23)	(-0.0405 0.1158 -0.0549)	44	(-25, -49)	(0.3093 -0.1076 0.2482)		
20	(-3, -47)	(-0.5171 0.6714 -0.0800)	45	(16, -5)	(-0.0100 0.0589 -0.0300)		
21	(-6, -29)	(-0.0870 0.2555 -0.1988)	46	(-6, -42)	(-0.3824 0.6424 -0.1471)		
22	(-8,7)	(-0.0011 0.0577 -0.0333)	47	(-22, -35)	(0.3027 0.7685 -0.0648)		
23	(1,-2)	(-0.0040 0.0729 -0.0432)	48	(-16, 14)	(-0.0005 0.0453 -0.0249)		
24	(-26, 12)	(0.0005 0.0412 -0.0217)	49	(-23, -40)	(-0.1164 0.0907 0.6267)		
25	(-3, -44)	(-0.3982 0.5752 -0.0957)	50	(-29, -35)	(0.1065 0.1422 0.1135)		

Table 1. The coordinates of locations and relocations

Table2. The true values and the definition intervals of the fault plane parameters

Parameters	Parameter Values	Bounds of Parameters
Lenght (km)	60	20 - 100
Width (km)	12	5 - 15
Depth (km)	1	0 - 5
Dip (radian)	1.2217	0.8727 - 2.0944
Strike (radian)	5.4978	4.7124 - 6.2832
East offset (km)	-20	-50 - 0
North offset (km)	-40	-50 - 0
Strike Slip (m)	2	-5 - 5
Dip Slip (m)	0.2	-5 - 5

4.2. **Results of the SA algorithm.** The objective function is analyzed in the parameter space during the parameter optimization procedure with SA algorithm. In the absence of any prior information about where the good feasible solutions might lie, it's reasonable to set each parameters midway between its lower bound and upper bound in order to start the search in the middle of the feasible region. For a sample run, initial parameter set is taken

 $\mathbf{p}_0 = [60\ 10\ 2.5\ 1.48355\ 4.5978\ -25\ -25\ 0\ 0]$. The initial temperature and Boltzmann's constant are considered T_0 and c = 0.9, respectively. The inner loop break condition is taken $n \times 10$, where n is the dimension of parameter set. Table 3 shows the results of SA algorithm for different stopping criteria (T_{\min}) . For each T_{\min} , the iteration number and computation time (CPU) are shown together with the objective function value (f) and estimated values of source parameters (\mathbf{p}^*) . It can be seen from the Table 3 that when the T_{\min} is decreased the loss function value gets smaller and the calculation period gets longer. The objective function takes the smallest value when the stopping criteria is choosen 10^{-12} . The change on temperature and the minimization of loss function value during the search process of SA are given in Figure 3. It can be seen from Figure 4 that while the temperature drops constantly from the beginning of the search, the objective function value given in equation 2.3 reaches the global minimum value.

			_			
			Tmin			
p	0.1	0.01	0.0001	0.000001	10-9	10-12
1	57.3532	76.1398	54.8002	79.6284	60.2159	62.6849
w	5.0056	6.5283	11.7820	10.4386	9.3609	10.8719
d	3.6522	0.2262	1.4992	0.5131	0	0.4829
8	1.8191	1.3041	1.4041	1.3183	1.3613	1.2285
α	5.1913	5.2409	5.4309	5.5042	5.5095	5.4989
хf	-43.6191	-19.4205	-18.8446	-19.4553	-19.1055	-19.8070
Уſ	-29.5504	-38.6611	-39.4626	-39.2952	-38.8713	-39.6528
SS	3.8168	3.2850	2.1505	2.1709	2.3917	2.1388
DS	3.4505	1.4016	-0.2640	0.2040	0.2564	0.2331
Iteration number	67	89	133	176	242	307
CPU (in seconds)	54	72	108	144	201	263
f	9.6048	2.0675	0.2177	0.0251	0.0286	0.0024

Table 3. Estimated values of source parameters for $T_0 = 100$ and c = 0.9



Figure 3. Cooling schedule and loss (misfit) function value of SA for $T_{\rm min}=10^{-12}$



Figure 4. Estimation results of fault plane parameters

Figure 4 shows the estimation results of source parameters during the search processes. The broken line illustrates the true values of the parameters. It's quite clear that the estimated values of the source parameters are very close to the true values, given in Table 2, while the algorithm gets the global minimum.

A single run of global converging algorithms is not sufficient to find the global solutions. The model parameters obtained by several runs may differ from each other because of the stochastic structure of the algorithm. Since the SA is a probabilistic search algorithm, different runs may result in dissimilar configurations. Therefore, several seperate runs are performed to ensure that the true global minimum has been located. The average results of 100 Monte Carlo simulations for the different initial values of fault plane parameters and average computation times (ACPU) are reported in Table 4. The initial temperature, Boltzmann's constant and stopping criteria are choosen 100, 0.9, and 10^{-8} respectively for all test runs. It has been observed from the simulation results that the average loss function value converges the global minimum for the arbitrary initials. It can be easily said that SA largely independent of the initial values and it can escape local minimum through selective uphill moves.

			1	₀ =100	c =(0.9	$T_{min} = 10$	-9			
	Arbitra	ary Initial	paramet	er value	s (p ₀)			Best	Average	Worst	ACPU
w	d	8	α	xf	Уſ	SS	DS	loss	loss	1oss	(s)
9	2	1.0472	5.3233	-17	-37	-3	2	0.0032	0.3763	3.5885	199
10	3	1.7453	5.4578	-45	-35	-3.5	2.7	0.0016	0.0233	0.0159	198
14	3.5	1.3963	5.0615	-34	-43	4	1	0.0001	1.1131	7.5599	200
6	1.5	1.7453	6.1959	-49	-27	3	-1	0.0028	0.7639	4.0373	201
7	3	1.7104	4.9742	-25	-32	-4	3	0.0033	0.7612	7.4845	199
.2.5	3.75	1.7889	5.8905	-12.5	-12.5	2.5	2.5	0.0014	0.5239	7.4839	198
5.1	0.1	0.88	4.72	-49.5	-49.5	-4.9	-4.9	0.0078	0.9570	7.4835	199
.4.9	4.9	2	6.2	-0.1	-0.1	4.5	4.5	0.0020	1.3004	7.4852	198

Table 4. The loss function values for the different initials

4.3. Results of the Nelder-Mead simplex method. The tests have been made on starting points chosen near the optimum and quite far from the optimum generated inside the parameter interval. Four scalar parameters must be specified to define a complete Nelder-Mead simplex method; coefficients of reflection ρ , expansion χ , contraction γ , and shrinkage σ . These parameters are chosen to satisfy $\rho > 0, \chi > 1, 0 < \gamma < 1, and 0 < \sigma < 1$. In this study, Nelder-Mead simplex algorithm, composed by [14], is applied to the source parameter estimation scheme. The coefficients of reflection, expansion, contraction and shrinkage are choosen $\rho = 1, \chi = 2, \gamma = \frac{1}{2}, \text{ and } \sigma = \frac{1}{2}$, respectively. The stopping criteria is considered $\varepsilon = 0.00001$. The results of Monte Carlo simulations are given in Table 5. It can be seen from the results that the Nelder-Mead simplex method requires stringent initial estimates for the model parameters. The method is only advantageous when a good initial estimate is provided. If the initial vertices are generated far from optimum, the loss function (f) can not reach the global minimum and CPU time gets large.

	A	$y = 1$ $\chi = 2$	$\gamma=1/2 \sigma=1/2$	$\varepsilon = 0.00001$	
			I nitial ver	tices	
		Near t	he optimum	Far from t	he optimum
	1	59.9806	62.6735	210.5092	124.2562
Ē	w	12.3626	11.2466	21.9962	143.5803
Ĩ	d	1.2088	0.6408	-4.63	8.2891
Ξ,	e 8	1.2243	1.2026	1.925	1.0454
ě,	α	5.497	5.4962	4.1669	5.5432
- 74 S	xf	-20.0571	-19.9768	-210.6472	-243.9392
	Уſ	-40.1067	-39.8784	107.3864	-85.8237
Esti	SS	1.9611	2.1012	27.4546	1.2652
	DS	0.1945	0.2214	-35.0457	-5.8005
	f	0.00043	0.0014	7.2495	7.2273
	CPU (in second	s) 2	4	7	5

Table 5. The simulation results of Nelder-Mead simplex algorithm

5. Conclusions

Estimation of fault plane parameters using classical optimization methods, e.g., derivative-nonderivative based optimization methods, Monte-Carlo methods, Least Squares methods, etc. is often difficult because of the nonlinearity of the problem. These methods need some assumptions to implement on problems and also may fail to get global solutions of optimization problems. In this paper, SA algorithm is presented and compared with a derivative-free optimization method, Nelder-Mead simplex method, for estimating the source parameters. The SA algorithm has many advantages over other optimization methods. The method has advantages in dealing with strong nonlinearities and discontinuities. The SA algorithm sometimes goes uphill as well as downhill unlike other direct optimization methods. This is an ability to avoid becoming trapped at local minima.

During the Monte Carlo simulation study, it's realized that assessing the performance of the Nelder-Mead simplex method is generally problematic due to the nonconverge of optimal parameter values even if it is more efficient than other direct search optimization methods. The simplex method requires strict initial conditions, whereas the SA algorithm is able to explore the parameter space and focus on the most promising area without prior knowledge of its location. The simulation results show that the SA algorithm is an efficient derivative-free optimization algorithm with respect to Nelder-Mead simplex method. However, the SA has some drawbacks. The most remarkable disadvantages of the SA algorithm are (i) spending much computing time to find the optimum solution and (ii) determining the proper cooling schedule. In order to obtain better results, the various tunable parameters used (e.g. initial temperature, final temperature, cooling rate etc.) needed to be chosen carefully depending on the problem variety. Due to its versatility and independence on prior knowledge of the parameter values, the SA algorithm is particularly applicable to estimate the parameters of fault plane model that are not solvable using analytical methods. It can be said that the SA algorithm is a promising tool for estimation of parameters in geosciences. However, the utility of this procedure to estimate fault plane parameters from real data has yet to be proven. In the later studies, it's possible to improve the algorithm by using different cooling schedules. Using a hybrid optimization strategy based on SA and gradient based or direct optimization algoritm can provide more efficient and accurate estimation of parameters. On the other hand as there are other well-established heuristics, such as genetic algorithms, Bee and Ant Colony, etc., a discussion of how good the estimation can be achieved by using them, may lead to a better estimation procedure.

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