

Deep Water Cooled ORC for Offshore Floating Oil Platform Applications

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Abstract

Due to global warming, environmental pollution and cost reduction, increasing efficiency of electricity conversion has become a key issue for the offshore market. This paper proposes an Organic Rankine Cycle (ORC), which uses heat waste from exhaust gases of an FPSO (Floating, Production, Storage and Offloading unit) as heating source, and deep ocean water as cooling source. A genetic algorithm optimization was conducted targeting maximization of net power output, by taking in to consideration of 23 working fluids. Expander inlet temperature and pressure were set as independent variables. The analysis encompasses subcritical or supercritical conditions and recuperation was included in a second version of the system as an option. The first configuration presented ethanol as optimal fluid, followed by toluene and the second configuration indicated cyclohexane followed by ethanol. Use of recuperation, when feasible, increased power output specially for cycles operating with dry and isentropic fluids, presenting an average contribution of 22.7%. Net power and efficiency results from ORC using deep sea water in condenser were presented and compared with ORC using shallow ocean water as cooling source and with Carnot efficiency operating under the same temperatures. Use of deep water raised net power output by 23.3% (cyclohexane recuperative ORC) and 12.5% (ethanol non-recuperative ORC) for the optimal configurations.

Keywords: ORC; deep water; FPSO; power generation.

1. Introduction

The increase in energy demand over the next two decades poses a challenge for the oil and gas sector, which is already one of the major contributors of CO₂ emissions. In Brazil, for instance, oil, gas and coal industry was responsible for 37% of greenhouse gas emission in 2012 [1]. In Norway, oil and gas extraction represented about 28% of those emissions in 2014 [2]. The search for more efficient processes is important not only due to environmental issues, but also because of cost reductions, once oil production and refining consume nearly 10% of the produced oil [3].

A considerable number of studies [4-9] developed researches on efficiency evaluation for offshore oil extraction and its related processes. Nguyen et al. [4] suggested a component-by-component exergy efficiency formulation for offshore oil and gas processing. De Oliveira & Van Hombeeck [5] studied exergetic efficiency and losses of a Brazilian offshore platform. Nguyen et al. [6] pinpointed exergy losses of an offshore platform for three stages of an oil field, while an exergy accounting was performed for six cases corresponding to different reservoir fluid compositions by Nguyen et al. [7]. Voldsund et al. [8] identified exergy losses of four platforms located in the North Sea. Voldsund et al. [9] applied exergy analysis on a real production day of an offshore platform. Most of the studies [4, 6-8] stressed the importance of good use of the waste heat contained in the exhaust gases.

A possible use for the waste heat is electricity generation through an ORC (Organic Rankine Cycle).

ORCs employ organic fluids instead of water as working fluid. They are usually exploited when a low-grade energy source is available, such as waste heat, solar energy, ocean thermal energy, geothermal energy and biomass, providing better results than those from water Rankine cycles. There is an extensive literature about ORCs for waste heat recovery. Particularly, the works of Mazetto et al. [10] and Pierobon et al. [11] performed a genetic algorithm (GA) optimization for ORC recovering waste heat systems. The former targeted maximization of net power output and maximization of power to heat transfer area ratio in a petroleum refinery, whereas the later optimized thermal efficiency, total volume of the system and net present value in an offshore platform. Optimizations portrayed by Mazetto et al. [10] displayed R134a and water as the best fluids – amongst the evaluated ones, while cyclopentane and acetone were considered as optimal working fluids by Mazetto et al. [10]. Yang and Yeh [12] proposed and optimized an ORC for recovering waste heat from a large marine engine. They concluded that R600a would give the highest ratio of net power output to the total heat-transfer area. Yang and Yeh [13] optimized an ORC for marine waste heat recovery through thermo-economic indicators and found R1234yf as the best option. The integration of an ORC in a Brazilian FPSO (Floating, Production, Storage and Offloading unit) was studied by Barrera et al. [14], moreover, the study defends that there is a great potential for generating power from exhaust gases. Some studies [15-17] took in consideration the use of supercritical ORC for waste heat recovery. Glover et al [15] simulated an ORC

operating under supercritical conditions and recovering heat from internal combustion engine. Kosmadakis et al. [16] performed an experimental investigation of an ORC operating at both subcritical and supercritical conditions and using a heat source at 95°C. Le et al. [17] conducted a performance optimization of supercritical ORCs using a heat source at 150°C. Desideri et al [18] conducted an experimental comparison between the fluids SES36 and R245fa for low temperature ORC waste heat recovery systems.

Besides its application in waste heat recovery systems, ORC has also been investigated for Ocean Thermal Energy Conversion (OTEC). Ocean thermal energy is solar energy absorbed and stored as heat in the upper layer of the ocean [19]. The water becomes colder as depth increases, and at 800m to 1000m, it reaches temperatures around 4°C [20]. OTEC uses those two layers as heating and cooling sources for a heat engine. It works under either an open-cycle or a closed-cycle process [19]. The open-cycle configuration presents lower efficiency, one of the reasons why most OTEC plants operate on the Rankine closed-cycle or its variants [21]. Yuan et al. [22] proposed an absorption OTEC closed cycle, where ammonia-water was the working fluid, achieving 4.17% thermal efficiency. Yang and Yeh [23] conducted an optimization of the ratio of net power output to the total heat transfer area on an OTEC plant, using ORC, in which R717 performed optimally. Even though OTEC comes out as a low environmental impactful process, the low practical efficiency due to the small temperature gap hampers its deployment [21].

The present work proposes an ORC waste heat recovery in an offshore oil platform. While the heating source for the suggested system is the exhaust gases of an offshore engine, the cooling source is deep seawater as in the closed-cycle OTEC. In other words, the system is a combination of two different applications for ORCs, which are not usually studied together in the literature. Expander inlet pressure and temperature were the independent variables, and maximization of net power output was aimed for each one of the tested fluids. A second scenario of the system including recuperation was also studied and all results were compared with conventional ORC using surface water as cooling source in order to analyze the contribution of the utilization of deep seawater to power generation. During any simulation, supercritical conditions are accepted if they provide better results.

2. Proposed System

In this section the ORC configurations, thermodynamic equations as well as the applied methodology are described.

2.1 System Description

Recuperative ORCs (RORC) and non-recuperative ORCs (NORC) were assessed. Supercritical conditions were allowed for fluids with superior performance in these conditions.

2.1.1 Non-recuperative ORC

The first layout of the proposed ORC has two possible configurations shown in Figure 1 with their respective T-s diagrams. The system in Figure 1(a) is a non-recuperative subcritical ORC. Starting the explanation from state 1, the working fluid, at saturated liquid state, is compressed by the pump to the evaporation pressure (state 2), which is in this case lower than the critical one. Then, the working fluid

receives reject heat from the exhaust gases, firstly through the economizer, reaching the saturated temperature (state 3). Next, through the evaporator, the fluid becomes saturated vapor (state 4). Finally, if advantageous for power output (which depends on the working fluid), the saturated vapor is super-heated (state 5). From state 5 (or state 4, in case super-heating is nonexistent) the working fluid is expanded to the condensation pressure (state 6) and then it enters the cooling process. Considering that the fluid leaves the expander as super-heated vapor, a desuperheater is necessary to turn it into saturated vapor (state 7) before entering the condenser. Otherwise, the fluid is sent directly to the condenser from the expander outlet. Both desuperheater and condenser make use of seawater to remove heat from the working fluid. After the condenser, the fluid is again at state 1.

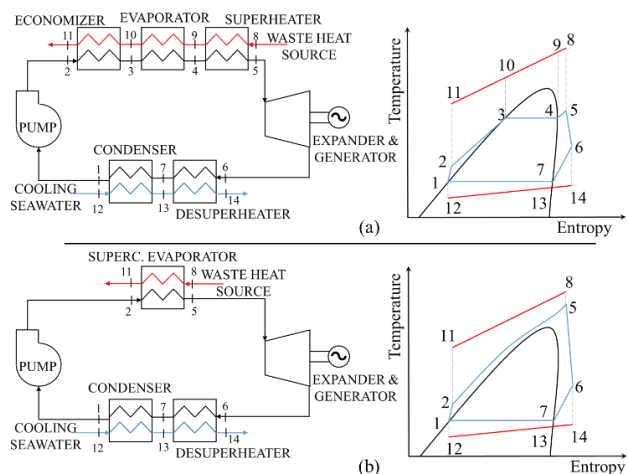


Figure 1. Configuration and T-s diagram of NORC: a) subcritical, b) supercritical.

The supercritical cycle depicted in Figure 1(b) is similar in most aspects to the previously described one. The main difference is the pump outlet pressure. In this case, the pressure is above the critical one, which means that the fluid will not face a gradual evaporation process, thus only one heat exchanger was modelled in the upper part of the cycle. The optimal expander inlet pressure indicated during the simulation is what determines if each working fluid is operating under subcritical or supercritical configuration.

2.1.2 Recuperative ORC

A second layout of the proposed system is represented in Figure 2. In this layout, a recuperator is installed. This equipment allows the flow leaving the expander to transfer heat to the one leaving the pump. The condition for applying this layout is $T_6 > T_2$. In case this condition is not met by a specific working fluid, this layout is not taken in consideration. The purpose of this recuperative process is to recover a fraction of the heat (area 1 in Figure 2) that would originally be lost from the working fluid to seawater.

Once again, the cycle can be either subcritical (Figure 2(a)) or supercritical (Figure 2(b)) depending on the same factors exposed in Section 2.1.1.

For both NORC and RORC at supercritical conditions, it was checked if the expansion process went through the two phase region by comparing the values of specific

entropy at the saturation line with the specific entropy values between point 5 and 6 (expansion process).

2.2 Thermodynamic Model

According to Brandsar [24] the main energy sources for ORCs in offshore applications are gas turbine exhausting gas, gas compressors intercoolers (compression train), and gas or diesel internal combustion engines exhausting gas. Pereira et al. [25] characterized Brazilian offshore utilities plants as 50% based on gas turbines and almost 12% based on internal combustion engines. The temperature of gas turbine and internal combustion engine exhausting gases depends whether these gases are used for petroleum heating or not. Thus, the exhausting temperature also varies with the FPSO production curve as well as its required heat load. The heat source considered in this work is the exhausting gas of an aeroderivative gas turbine (64 kg/s) after oil heating (330°C). This heat source temperature is close to the value presented by Pierobon et al. [26] (335°C) for the same application. In order to avoid uneconomical configurations the minimal temperature allowed for the exhausting gas was 105°C.

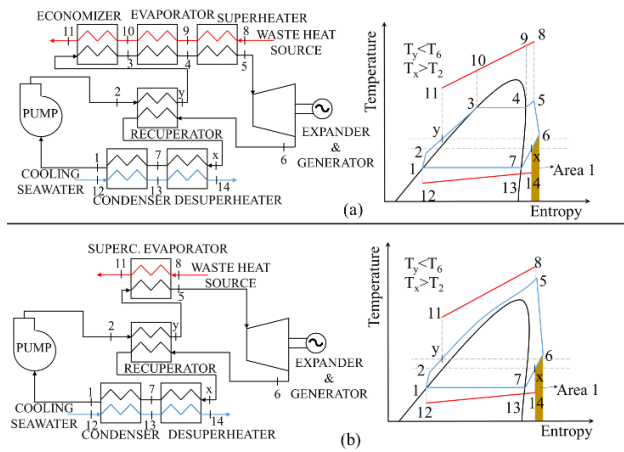


Figure 2. Configuration and T-s diagram of RORC: a) subcritical, b) supercritical.

Most of new Brazilian FPSOs are been used in deep water exploration [27]. The water temperature drops with depth down to 4°C at 1000m [28]. Thus, this cold temperature reservoir will be used to provide extra power in the proposed system. Since the deep seawater will be rejected at sea level, the required cooling water pump head is for pressure loss in pipes and heat exchanger only [29]. In this model, it is considered the power to overcome the pressure drop in the cooling water pipe, as it affects the comparison between deep and shallow water operations.

The components of the proposed system are modelled at steady state. General assumptions are: 1) the equipment as well as pipes do not lose heat to environment, 2) potential and kinetic energy variations are neglected, 3) pressure drops in pipes and heat exchangers are neglected (except deep cooling water pipe). Table 1 gives the equipment parameters for the simulations together with cooling and heating specifications.

Isentropic efficiency definitions for the expander and pump are given in Eqs. (1) and (2), respectively.

$$\eta_{t,ise} = \frac{h_5 - h_6}{h_5 - h_{6,ise}} \quad (1)$$

$$\eta_{p,ise} = \frac{h_1 - h_{2,ise}}{h_1 - h_2} \quad (2)$$

Eqs. (3) and (4) show energy balance for expander and pump, respectively.

$$\dot{W}_t = \dot{m}_{wf} \cdot (h_5 - h_6) \quad (3)$$

$$\dot{W}_p = \dot{m}_{wf} \cdot (h_2 - h_1) \quad (4)$$

Table 1. System Specifications.

Parameter	Value
Expander isentropic efficiency ($\eta_{t,ise}$)	80.0%
Pump Isentropic efficiency ($\eta_{p,ise}$)	75.0%
Recuperator effectiveness (ε_r)	85.0%
Pinch temperature difference at condenser	10.0°C
Minimum pinch temperature difference at evaporator	10.0°C
Exhaust gases temperature at state 8 (T_8)	330°C
Minimum exhaust gases temperature at state 11 (T_{11})	105°C
Exhaust gases mass flow rate (\dot{m}_{eg})	64.0 kg/s
Exhaust gases average specific heat ($c_{p,eg}$)	1.20kJ/(kg·K)
Deep seawater temperature at state 12 ($T_{12,dsw}$)	5.00 °C
Condensation temperature when using deep seawater ($T_{7,dsw}$)	18.0 °C
Shallow seawater temperature at state 12 ($T_{12,ssw}$)	32.0 °C
Condensation temperature when using shallow seawater ($T_{7,ssw}$)	45.0 °C
Cooling water pipe friction factor (f)	0.01362
Cooling deep water pipe length (L)	1000 m
Density of cooling water (ρ)	1000 kg/m ³
Cooling water flow velocity (v)	1.200 m/s
Gravitational acceleration	9.807 m/s ²

Eqs. (5), (6), (7) and (8) give the energy balance of the economizer, evaporator, super-heater and supercritical evaporator.

$$\dot{m}_{eg} \cdot c_{p,eg} \cdot (T_{11} - T_{10}) = \dot{m}_{wf} \cdot (h_3 - h_2) \quad (5)$$

$$\dot{m}_{eg} \cdot c_{p,eg} \cdot (T_{10} - T_9) = \dot{m}_{wf} \cdot (h_4 - h_3) \quad (6)$$

$$\dot{m}_{eg} \cdot c_{p,eg} \cdot (T_9 - T_8) = \dot{m}_{wf} \cdot (h_5 - h_4) \quad (7)$$

$$\dot{m}_{eg} \cdot c_{p,eg} \cdot (T_{11} - T_8) = \dot{m}_{wf} \cdot (h_5 - h_2) \quad (8)$$

Energy balance for desuperheater and condenser are given in Eqs. (9) and (10).

$$\dot{m}_{cw} \cdot c_{p,cw} \cdot (T_{14} - T_{13}) = \dot{m}_{wf} \cdot (h_7 - h_6) \quad (9)$$

$$\dot{m}_{cw} \cdot c_{p,cw} \cdot (T_{13} - T_{12}) = \dot{m}_{wf} \cdot (h_1 - h_7) \quad (10)$$

Eq. (11) shows effectiveness definition for heat exchanger applied to the recuperator. Energy balance for this equipment is shown in Eq. (12).

$$\varepsilon_r = \frac{T_y - T_2}{T_6 - T_2} \quad (11)$$

$$h_y - h_2 = h_6 - h_x \quad (12)$$

Definition of degrees of superheat is given in Eq. (13). Thus, it is directly dependent on the optimized variable T_5 .

$$\Delta T_{sup} = T_5 - T_4 \quad (13)$$

Head pressure loss (H_l) for cooling water pipe is given by Eq. (14). The pipe diameter D is calculated using Eq. (15). The value of v was adopted according to commercial values [29] (see Table 1). The friction factor, f , was calculated using Colebrook equation. Eq. (16) gives the power consumed by cooling water pump using deep water ($\dot{W}_{p,cw}$).

$$H_l = f \cdot \frac{L}{D} \cdot \frac{v^2}{2g} \quad (14)$$

$$D = \sqrt{\frac{4 \cdot \dot{m}_{cw}}{V \cdot \pi \cdot \rho_{water}}} \quad (15)$$

$$\dot{W}_{p,cw} = \frac{\dot{m}_{cw} \cdot g \cdot H_l}{\eta_{p,ise}} \quad (16)$$

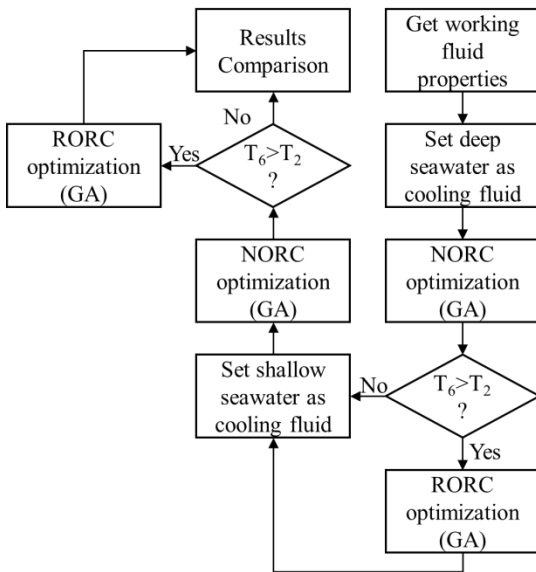


Figure 3. Simulation and optimization flowsheet.

Heat transferred from the exhaust gases \dot{Q}_h is calculated by Eq. (17). Finally, net power \dot{W}_{net} and cycle efficiency η_{tot} are given by Eqs. (18) and (19). It is important to remember that the consumed power due to the cooling water pump losses is only taken in consideration for deep water cooled systems, as earlier explained in this section.

$$\dot{Q}_h = \dot{m}_{eg} \cdot c_{p,eg} \cdot (T_{11} - T_8) \quad (17)$$

$$\dot{W}_{net} = \dot{W}_t - \dot{W}_p - \dot{W}_{p,cw} \quad (18)$$

$$\eta_{tot} = \frac{\dot{W}_{net}}{\dot{Q}_h} \quad (19)$$

2.3 Methodology

In this work, 23 organic working fluids were considered for the proposed system. The selected fluids do not include fluids prohibited by Kyoto or Montreal protocols and are the same used by Mazetto et al. [10]. The steps described in Figure 3 were applied to each of those fluids. The layouts described in 2.1.1 and 2.1.2 (whenever T_6 is higher than T_2) were simulated and optimized, firstly using deep seawater

as cooling fluid, and then using shallow seawater for the same purpose. This methodology was repeated for each one of the 23 considered fluids.

Table 2. Working Fluids Properties.

Substance	Type	T_{crit} (°C)	P_{crit} (kPa)
Benzene	Dry	289	4894
Isobutane	Dry	135	3640
n-Butane	Dry	152	3796
n-Decane	Dry	345	2103
n-Dodecane	Dry	385	1817
n-Heptane	Dry	267	2727
n-Hexane	Dry	235	3058
n-Nonane	Dry	321	2281
n-Octane	Dry	296	2497
n-Pentane	Dry	197	3364
Isopentane	Dry	187	3370
Cyclohexane	Isentropic	281	4081
Toluene	Isentropic	319	4126
R123	Isentropic	184	3668
R134a	Isentropic	101	4059
R141b	Isentropic	204	4249
R142b	Isentropic	137	4055
R245fa	Isentropic	154	3651
R502	Wet	82.2	4074
R717	Wet	132	11330
Ethanol	Wet	242	6268
Propane	Wet	96.7	4247
Water	Wet	374	22060

The optimization method is the PIKAIA version of Genetic Algorithm (GA) [30], which consists on a computational model inspired by the Theory of Evolution with efficient means of searching for the global optima. The independent variables are expander inlet pressure P_5 and temperature T_5 , while objective function is to maximize net power \dot{W}_{net} for all optimizations in Figure 3. P_5 and T_5 are selected through the GA method, where some combinations of these variables are chosen (a generation) and the output is evaluated. The process is repeated, modifying the newer generations according to the mutation rate until the global optima is found. Boundaries for those variables are also set in order to avoid unrealistic values (T_5 greater than T_8 , for instance).

Simulations were conducted on software EES [31]. Table 2 gives the list of considered working fluids and their properties taken from the software library. All properties used during simulations were taken from this same library.

3. Results

In this section, the results are presented and discussed. In section 3.1, the outputs from the configurations with and without recuperation are analyzed and compared between themselves. In section 3.2 those configurations are compared to their relative shallow water cooled versions.

3.1 Deep Seawater Cooled System

Optimal values for the independent variables (T_5 and P_5) as well as working fluid mass flow rate (\dot{m}_{wf}), degrees of superheat (ΔT_{sup}) and expander inlet pressure condition are

given in Tables 3 and 4, for NORC and RORC respectively, operating with deep seawater as cooling fluid.

Table 3. Properties of optimized NORC cooled by deep seawater.

Substance	T_5 (°C)	P_5 (kPa)	\dot{m}_{wf} (kg/s)	ΔT_{sup} (°C)	Cond.
Benzene	254	2005	23.3	32.0	Subcrit.
Isobutane	325	25600	20.3	-	Superc.
n-Butane	325	24020	19.9	-	Superc.
n-Decane	269	694.3	19.8	0	Subcrit.
n-Dodecane	263	274.9	19.8	0	Subcrit.
n-Heptane	325	8580	19.9	-	Superc.
n-Hexane	325	12200	19.9	-	Superc.
n-Nonane	276	1201	19.7	0	Subcrit.
n-Octane	325	5661	19.8	-	Superc.
n-Pentane	325	17000	19.9	-	Superc.
Isopentane	325	21460	20.1	-	Superc.
Cyclohexane	325	7372	21.1	-	Superc.
Toluene	245	1536	24.2	0	Subcrit.
R123	325	17670	48.2	-	Superc.
R134a	325	35200	41.5	-	Superc.
R141b	314	3999	36.1	114	Subcrit.
R142b	325	22680	40.7	-	Superc.
R245fa	325	25340	39.6	-	Superc.
R502	232	3945	58.9	151	Subcrit.
R717	325	2998·10	10.6	-	Superc.
Ethanol	325	8621	12.7	-	Superc.
Propane	325	3235·10	20.3	-	Superc.
Water	325	485	5.24	174	Subcrit.

Most of the substances reached supercritical condition. This was expected when relating the critical properties on Table 2 to the temperature of the exhaust gases, which is high compared to most of the critical temperatures. From a thermodynamic point of view, supercritical ORC has the advantage (over subcritical ORC) of better matching the heating source cooling curve and working fluid heating curve (closer curves) [32], since there is no horizontal evaporation step in boiler temperature profile. Therefore, it may lead to higher efficiency [33] as noted in most of the tested fluids. However, this configuration of ORC presents challenges to overcome, i.e. high pressure required and high pressure ratio in turbine (which affects selection of equipment material), supercritical heat transfer and the uncertainty of working fluid properties in the supercritical region [17].

Sixteen fluids presented the highest temperature T_5 allowed in the simulation (325°C) for the NORC system and only two fluids for the RORC. In general, recuperation led to a reduction of the optimal pressure P_5 and T_5 . This is positive from the equipment cost point of view, once lower pressure and temperature requires less robust material. On the other hand, recuperation allowed a higher mass flow rate \dot{m}_{wf} . This means that, even with the expander inlet pressure and temperature decreasing, the absolute power

produced by this equipment can increase due to the extra mass flow rate of working fluid.

Table 4. Properties of optimized RORC cooled by deep seawater.

Substance	T_5 (°C)	P_5 (kPa)	\dot{m}_{wf} (kg/s)	ΔT_{sup} (°C)	Cond.
Benzene	239	2552	27.6	0	Subcrit.
Isobutane	255	12890	34.0	-	Superc.
n-Butane	267	13030	31.0	-	Superc.
n-Decane	237	402.0	27.6	0	Subcrit.
n-Dodecane	231	141.5	28.0	0	Subcrit.
n-Heptane	277	3717	30.9	-	Superc.
n-Hexane	271	5281	30.9	-	Superc.
n-Nonane	246	753.5	27.1	0	Subcrit.
n-Octane	296	4000	28.7	-	Superc.
n-Pentane	271	8733	30.8	-	Superc.
Isopentane	256	8608	32.9	-	Superc.
Cyclohexane	303	5768	28.4	-	Superc.
Toluene	217	992.7	29.0	0	Subcrit.
R123	308	14350	63.7	-	Superc.
R134a	276	19610	61.0	-	Superc.
R141b	273	3947	50.6	73.0	Subcrit.
R142b	303	17400	54.0	-	Superc.
R245fa	280	14460	58.3	-	Superc.
R502	210	4001	95.3	129	Subcrit.
R717	325	19040	10.4	-	Superc.
Ethanol	325	6356	12.9	-	Superc.
Propane	258	17470	32.4	-	Superc.
Water	-	-	-	-	-

Figure 4 indicates optimized values of net power \dot{W}_{net} for each substance as well as cycle thermal efficiency η_{tot} for both NORC and RORC systems.

Ethanol presented the best results under non-recuperative process, with net power output of 4926kW and 28.51% of thermal efficiency. Although ethanol becomes very corrosive at high temperatures, it is a very interesting candidate because it is regarded as non-toxic, environmentally friendly and cheap working fluid [34]. Ethanol was followed by toluene (4416kW and 25.56%). The poorest performance was from R502 with a net power output of 1796kW (~2.7 times lower than ethanol) and thermal efficiency of 10.39%. Water achieved net power of 3823kW with 23.99% thermal efficiency

Under recuperative process, cyclohexane performed the best, followed by ethanol. The first presented net power of 5283kW with 30.57% thermal efficiency whereas the second had 5144kW and 29.77%. R502 once more presented the lowest net power output and thermal efficiency amongst the RORC simulations (2684 kW and 15.53%). Recuperation was not feasible for water.

Recuperation, when used, always contributed to increasing net power output as well as thermal efficiency with an average relative contribution of 22.7% for both outputs. Its contribution is not constant, however, as some

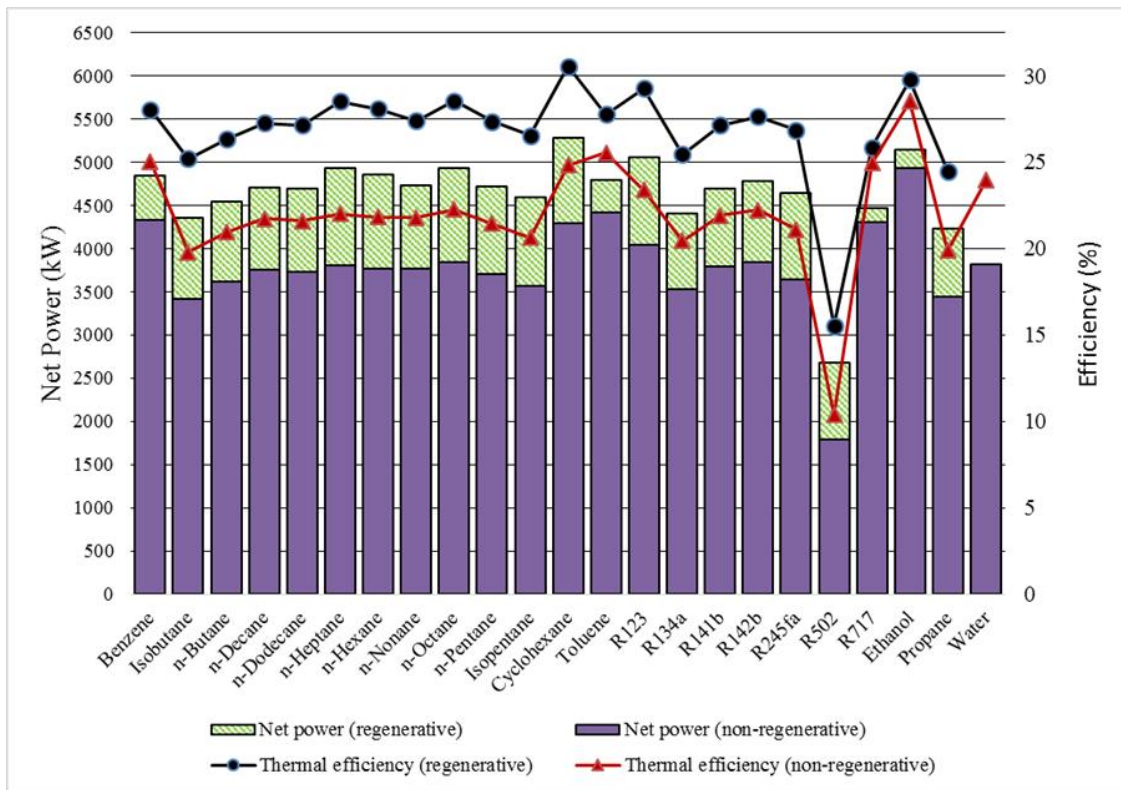


Figure 4. Optimized net power output and thermal efficiency results using deep seawater as cooling fluid.

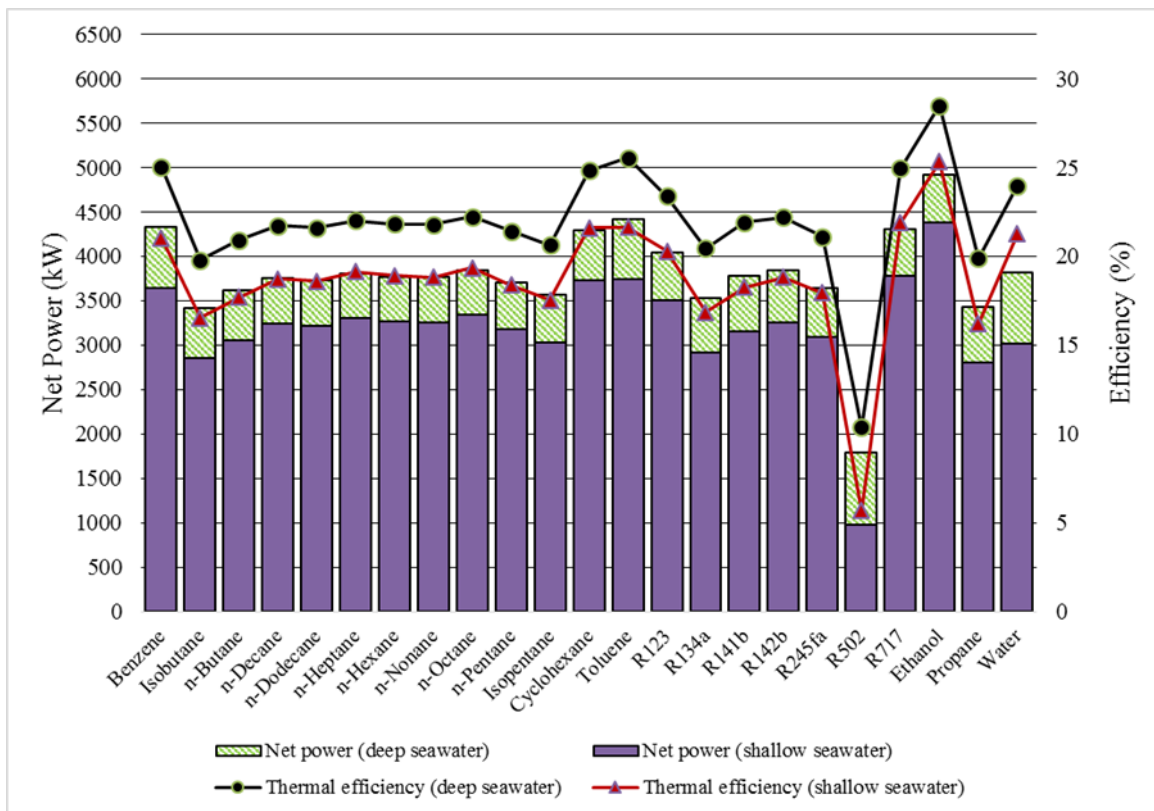


Figure 5. Comparison between deep and shallow seawater cooled systems for NORC configuration.

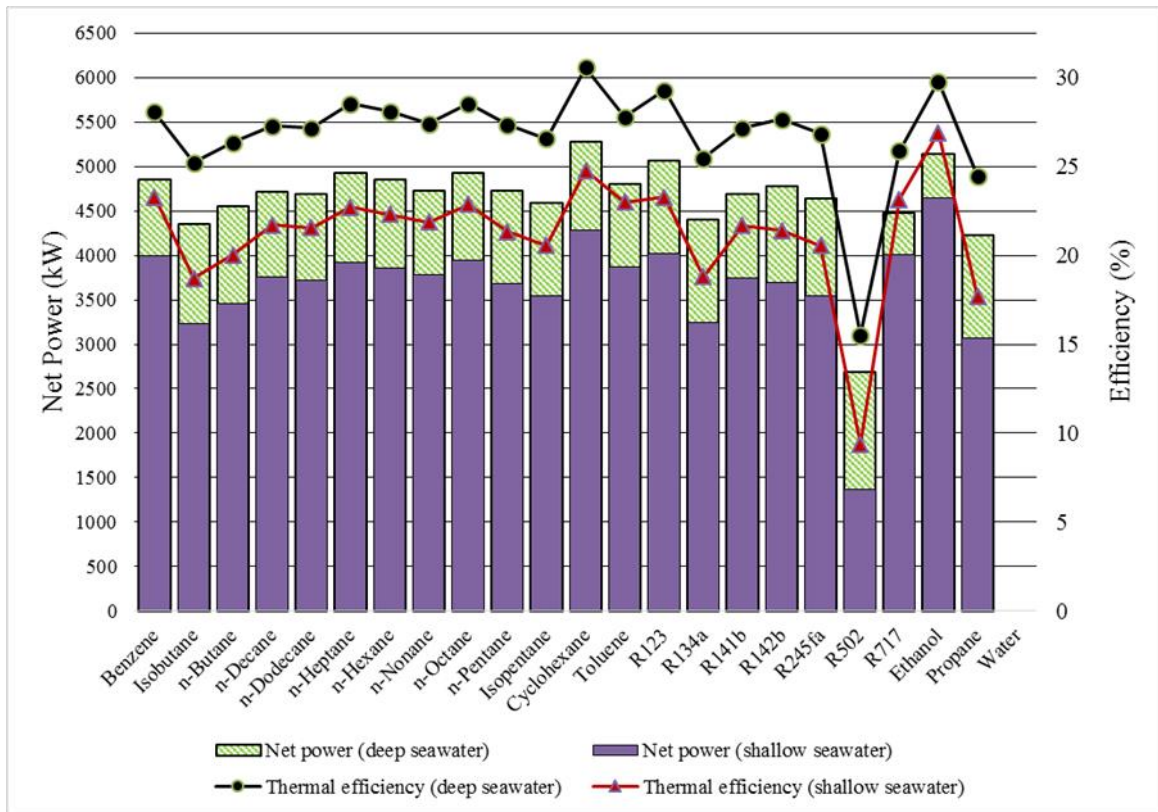


Figure 6. Comparison between deep and shallow seawater cooled systems for RORC configuration.

fluids show more potential for recuperation than others. For example, ethanol, which performed best in NORC simulation, was surpassed in RORC due to the high contribution in net power that recuperation provided to cyclohexane (994kW against 218kW). The highest relative contribution in net power comes from R502 (49.4%), and lowest from R717 (3.6%). Besides R502, wet fluids were less influenced by recuperation. This is expected as cycles operating with dry fluids (and isentropic to a lesser extent) have a characteristic high energy available at the expander outlet [35, 36]. The increment in efficiency provided by recuperation is consistent with the literature [37, 38]. Higher efficiency means that a high power output can be maintained for a decreased heat input to the ORC [38]. In this work, the heat input was not necessarily decreased from NORC to RORC, which lead to higher values for both efficiency and net power output under RORC configuration.

3.2 Shallow Seawater and Carnot Comparison

In order to evaluate the benefit of using deep sea water, comparisons with the use of shallow seawater are exposed in Figures 5 and 6.

It is noticeable that the proposed deep cooled water system performs better than a standard seawater cooled one. Deep cooled systems had an average increment of net power output of 20.4% and 29.5% for NORC and RORC configurations, respectively. Thermal efficiency relative raise, in average, corresponds to 19.8% (NORC) and 27.9% (RORC), which is remarkable. The optimal NORC, with ethanol, presented 12.5% relative increment on thermal efficiency and net power output (from 4380kW to 4926kW) while optimal cyclohexane RORC, showed an increment of 23.3% on both variables, with net power output raising from 4284kW to 5283kW. Water NORC had 12.8% relative raise on efficiency and 26.8% on net power output. The most affected system was R502 RORC, which faced 96.6%

increment on net power output and 65.6% on thermal efficiency.

As the temperatures of heat absorption and rejection are not constant, Carnot efficiency η_{carnot} must be calculated from average values. It slightly changes with the selected fluid due to the open constraints in the heating and cooling system. For cyclohexane NORC, Carnot efficiency is 41.6%, giving a relative efficiency (η_{tot}/η_{carnot}) of 73.5%. For ethanol RORC, η_{carnot} is 41.7%, with relative efficiency of 68.4%.

Gas turbines are the most used technology to generate power in Brazilian FPSOs [25] and the heat rate of these turbines is around 9300 kJ/kWh [39]. Since the cost of the natural gas produced by the FPSOs, which is also consumed by the gas turbines, must be lower than resellers price (0.02966 Euro/kWh [40]), it is possible to calculate a limiting cost for the electricity produced by the ORC of 0.077 Euro/kWh. If the ORC electricity cost is higher than 0.077 Euro/kWh it will preferable to generate it by burning natural gas in gas turbines.

4. Conclusions

A deep seawater cooled ORC for waste heat recovery on FPSO was proposed in this paper in two configurations: non-recuperative (NORC) and recuperative (RORC). Optimizations with several organic fluid candidates were conducted under a Genetic Algorithm, in order to obtain maximized net power output by searching for the optimal expander inlet temperature and pressure. The optimal indicated NORC fluid was ethanol (4926kW net power output) while cyclohexane performed best under RORC (5283kW). Recuperation contributed for higher efficiency and net power output in all applied cases with an average value of 22.7%; moreover, it tended to reduce optimal expander inlet pressure and temperature. Those results can be understood together with another pattern: Recuperation

allowed a higher working fluid mass flow rate, which contributes to higher absolute net power output.

When compared with shallow water cooled systems, the proposed system performed significantly better. The use of deep water raised net power output and thermal efficiency in all cases. For the optimal deep cooled configurations, it increases net power output by 23.3% (cyclohexane RORC) and 12.5% (ethanol NORC). The average contribution in power output from deep water use was 20.4% and 29.5% for NORC and RORC, respectively. Its average contribution on efficiency was 19.8% (NORC) and 27.9% (RORC)

The results presented in this work indicate how deep water cooled ORC for FPSO applications would behave from a thermodynamic point of view. It points that this configuration can be interesting from the same thermodynamic perspective. Future works on this matter may explore thermo-economical evaluations.

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Nomenclature

c	specific heat, kJ/(kg K)
D	pipe diameter, m
f	friction factor
g	gravitational acceleration, m/s ²
h	enthalpy, kJ/(kg K)
L	pipe length, m
\dot{m}	mass flow rate, kg/s
P	pressure, kPa
\dot{Q}	heat, kW
T	temperature, °C
v	flow velocity, m/s
\dot{W}	power, kW

Greek symbols

Δ	absolute variation
η	efficiency
ε	heat exchanger effectiveness
ρ	density, kg/m ³

Subscripts and superscripts

carnot	Carnot
crit	critical
cw	cooling water
dsw	deep seawater
eg	exhaust gases
ise	isentropic
l	loss
net	net
P	at constant pressure
p	pump
r	recuperator
ssw	shallow seawater
t	turbine
wf	working fluid

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