



## Characterization of Asphalt Binder Containing Microcapsules

### Mikrokapsül içeren asfalt malzemelerin özelliklerinin Araştırılması

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#### Abstract

Asphalt pavements are exposed to traffic loading and adverse environmental effects such as rain and oxidation which result in decreasing their relaxation capabilities and the initiation of cracks. Recent research highlights the importance of developing long life pavements. One of the possible ways is to utilize innovative maintenance techniques such as self-healing technologies in order to reverse the aging process in asphalt binder. So as to achieve this goal, self-healing microcapsules seems to be an effective way to autonomously repair the micro-cracks, restore original mechanical properties, then further slow fatigue cracks growth and increase the fatigue life of the pavement.

In this study urea formaldehyde (UF) self-healing microcapsule were prepared by in-situ polymerization method. Following the characterization of microcapsules, different amount of microcapsules (6, 8, 9, 10, 11 and 12%) were added into bitumen. Rheological properties of the samples have been determined by means of Dynamic Shear Rheometer. Ductility test was also employed to characterize the mechanical properties of the bitumen samples.

Based on results the produced microcapsules can endure high temperatures, which indicate that these microcapsules can resist the thermal influence of bitumen in application. Besides, bitumen samples involving microcapsules exhibit satisfactory results in terms of complex modulus ( $G^*$ ) and bitumen recovery tests. The recovery value of the modulus increased first and then decreased with the amount of microcapsules. Microcapsules containing rejuvenator will be a promising product to realize the smart pavements.

**Keywords:** Bitumen, Self-healing, Microencapsulation, Rejuvenator, In-situ polymerization

#### Öz

Asfalt kaplamalar, trafik yükleri, yağmur ve oksidasyon gibi yol kaplamaları için olumsuz çevresel etkilerine maruz kalarak mekanik özelliklerini kaybetmektedir. Son zamanlardaki araştırmalar uzun ömürlü kaplamaların önemini vurgulamaktadır. Sürdürülebilirlik kapsamında bitümlü sıcak

karışımlarının ömrünü korumak ve arttırabilmek amacı, asfalt endüstrisini farklı araştırmalara itmiş ve günümüzde “kendi kendini iyileştiren” (Self Healing) teknikler üzerine yoğunlaştırmıştır.

Bu hedefe ulaşmak için, kendi kendini onaran mikrokapsüller, mikro çatlakları otonom olarak onarmanın ve orijinal mekanik özellikleri geri kazanmanın, daha sonra mikro çatlaklarının büyümesini daha da yavaşlatmanın ve kaplamanın ömrünü uzatmanın etkili yöntemlerden biri olarak görünmektedir.

Bu çalışmada, üre ve formaldehit (UF) karışımı ile kendi kendini iyileştiren mikrokapsüller, in situ polimerizasyon yöntemi ile hazırlanmıştır. Mikro kapsüllerin karakterizasyon araştırılması ve asfalt içinde gösteren iyileşme oranını incelemek amacı ile bitüm içine farklı miktarda mikro kapsül (6, 8, 9, 10, 11 ve %12) eklenmiştir. Numunelerin reolojik özellikleri Dinamik Kesme Reometresi ile incelenmiştir. Ayrıca mikrokapsül içeren bitüm numunelerinin mekanik özelliklerinin tespiti için çekme testi yapılmıştır.

Üretilen mikro kapsüller uygulamada bitümün termal etkisine dayanabileceğini gösteren yüksek sıcaklıklara dayanabilmektedir. Ayrıca, mikro kapsülleri içeren bitüm numuneleri, kompleks modülü ( $G^*$ ) ve bitümün mekanik özellikleri açısından tatmin edici sonuçlar göstermektedir. Araştırmaya göre İyileşme değeri ilk etapta artıyor ve bu mikrokapsüllerin asfalt malzemesinin mekanik özelliklerini geri kazanma göstergesidir. İyileştirici madde içeren mikro kapsüller, yeni nesil kaplamaları gerçekleştirmek için umut verici bir ürün olacaktır.

**Anahtar Kelimeler:** Bitüm, kendiliğinden iyileşen, mikro kapsül, iyileştirici madde, polimerizasyon

## 1. Introduction

The global road network distances 16.3 million kilometers [1], of which 5 million kilometers is in the EU, 4.4 million kilometers in the USA and 3.1 million kilometers in China [2]. Road networks fulfill a major economic and social goal by facilitating the movement of goods and people. As a result, governments invest heavily in the development and maintenance of national and regional road networks. In 2009, EU governments invested 42% of the EU transport network fund into the development and maintenance of road networks. The development and maintenance of the global road network are crucial for the growth and competitiveness of the worldwide economy.

Recent research highlights indicate that a classic road system involves double or triple asphalt layers with an expected service life of 20-40 years. The aging of bitumen leads to pavement failure after years of utilization. The stiffness of asphalt materials increases while the relaxation capacity decreases, and the bitumen converts to more brittle materials as well as this issue resulting the progress of cracks and ultimately cracking of the interface between aggregates and bitumen [3,4]. The key cause of this phenomenon is the increment in the asphaltene/maltene ratio in bitumen. Under the combined action of traffic load, and environmental factors, micro cracks occur in the asphalt pavement. Then the micro cracks, with the continuous expansion and

accumulation, expand into macroscopic cracks. If being not repaired in time, these cracks will affect the driving comfort and service life of pavement [5].

An increase in the application of a higher percentage of the preservation and renovation of asphalt pavement is achievable using a rejuvenator. The self-healing or self-repair material/system is considered to be the ability of the material to substantially return to the initial properties by making the necessary adjustments to restore to normality and the ability to resist the formation of irregularities and defects [6]. Self-healing asphalt pavement can detect and repair cracks by itself to some extent. In recent years, some procedures including microwave heating, induction heating, microcapsule and ion polymer and so on, have been used to heal the cracks in pavement. In other words, our ultimate aim is to develop an asphalt pavement material that will rejuvenate itself in the service life. In comparison with existing maintenance procedures, self-healing asphalt has the potential to improve traffic flow, reduce demand for fresh aggregate, reduce CO<sub>2</sub> emissions and enhance road safety[7-11].

However, the use of rejuvenators presents a challenge as it is difficult to penetrate into the asphalt layer, which is necessary to rejuvenate the mix [12]. Therefore, encapsulation methods have been studied as an alternative in order to incorporate the use of rejuvenators into the mix

during production[13]. The use of self-healing microencapsulation has been investigated to enhance the efficiency of self-healing processes [14]. Microcapsules may therefore break at different times during the bitumen aging history. The remaining microcapsules near the micro crack can then leak rejuvenator later when another micro crack is generated with an even higher crack tip strain. It has previously been reported that microcapsules containing rejuvenator can be fabricated with various shell thickness and size distributions [15-16]. The size and shell thickness are both important influencing factors of the micromechanical properties of the microcapsules. Firstly, the structure of microcapsules is taken into account for the specific requirement such as size distribution and encapsulation ratios; subsequently this affects their service performance.

In the light of the above information, the aim of this paper is to investigate the self-healing capability of bitumen including microcapsules filled with rejuvenator. Various samples were fabricated to investigate the healing performance of bituminous materials. Most of studies on the healing performance of microcapsule were more confined to evaluate the performance of microcapsule itself, but not the performance of asphalt containing microcapsule [16-17]. Therefore, for this purpose the bitumen tests focused on the bituminous material to evaluate the healing

performance of the asphalt. In order to observe the self-healing performance, ductility test under low temperature conditions and fatigue load tests was performed to spot the recovery properties. Virgin and rejuvenated bitumen properties were compared to evaluate the recovery behaviors of bituminous materials.

## 2. Material and Method

### 2.1 Materials

Self-healing microcapsules were prepared by in-situ polymerization method [18]. Urea and formaldehyde (37 % aqueous) was used as the shell wall forming monomers which purchased from Merck KGaA Company . Polyvinyl alcohol (PVA) and Sodium dodecyl sulphate (SDS) which used as emulsifiers were procured from Acros Organics Company Bitumen rejuvenator which used as core material in microcapsules was prepared by mixing the lightweight organic oil containing high contents of aromatics.

Sodium hydroxide and citric acid were used for pH adjustment. The bitumen with a 50/70 penetration grade was procured from Aliaga/Izmir Oil Terminal of the Turkish Petroleum Refinery Corporation. In order to characterize the properties of the base bitumen, conventional test methods such as: penetration test and softening point test were performed. These tests were conducted in conformity with the relevant test methods that are presented in Table 1.

**Table 1.** Properties of base bitumen

Test	Specification	Results	Specification limits
Penetration(25°C;0.1mm)	ASTM D5	55	50-70
Softening point(°C)	ASTM D36 EN 1427	49.1	46-54
Viscosity at(135°C)Pa.s	ASTM D4402	0.413	-
TFOT(163 °C; 5h)	ASTM D1754	137.5	-
Change of mass(%)		0.04	0.5 (max)
Retained penetration(%)	ASTM D5 EN 1426	51	50 (min)
Specific gravity	ASTM D70	1.030	-

## 2.2 Core synthesis and preparation of microcapsules

To prepare the microcapsules by in-situ polymerization method, first emulsion was created in 1000 ml reactor. 600 ml distilled water; 11 g emulsifier PVA and 2.5 g surfactant sodium dodecyl sulfate was added and thoroughly mixed. Pre-polymer was created to form the shell of the microcapsules. 18 gr urea reacts by 36 gr formaldehyde at 55-65°C for 1 h in another container with adjusting the PH to 8-8.5 by using sodium hydroxide to obtain pre-polymer. On the otherhand 15 gr rejuvenator composed from organic oil prepared for using in core section. Reactor (containing the emulsion) Installation was prepared in a bath and the core solution added and mixed at 55-65°C for 30 min. Then the pre-polymer added slowly and stirred at 250 rpm and wait to reacting for 4 h while adjusting pH to 3 by using citric acid. The emulsion solution has been washed and filtered using water containing 10% methanol then separated microcapsules have been dried in a vacuum oven at 30 °C for 8 h.

## 2.3 Characterization of microcapsules

### 2.3.1 Morphology

Morphology of the microcapsules was examined by scanning electron microscopy (SEM) using a Carl Zeiss 300VP microscope. The samples were vacuum dried and then mounted on aluminum stubs with double-stick tape. Then a layer of gold was evaporated onto the sample surface in a vacuum metallizing unit using QUORUM Q150.

## 2.3.2 Chemical structure

Attenuated Total Reflectance-Fourier Transform Infrared Spectroscopy (ATR-FTIR) (Perkin Elmer Spectrum BX) was used to determine the chemical structures of the microcapsules in the wave number range of 4000-500  $\text{cm}^{-1}$  with the resolution of 4  $\text{cm}^{-1}$  and 25 scans per sample to confirm that the microcapsules were filled with rejuvenator.

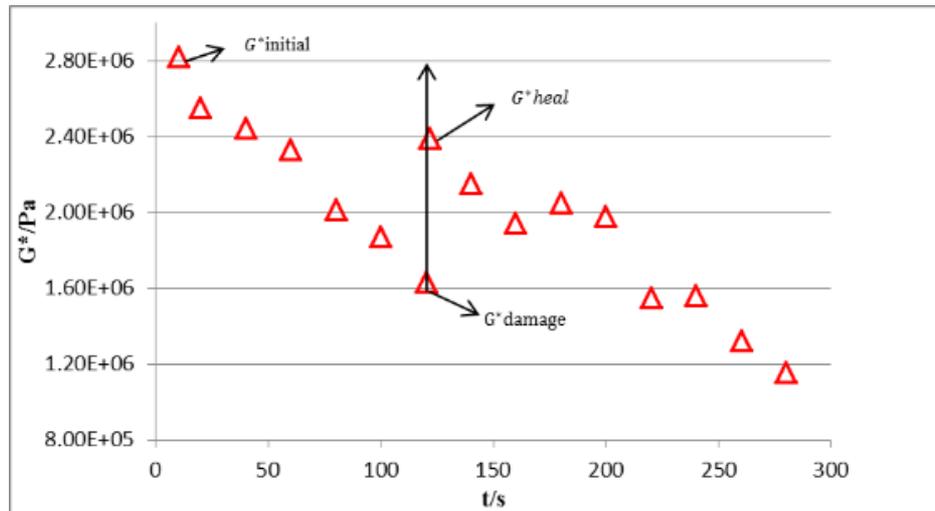
## 2.4 Healing performance

### 2.4.1 Fatigue Test

Asphalt fatigue test was performed to study healing performance under fatigue-load condition according to ASTM D7175-15. The test temperature was adjusted to 20 °C, and stress control mode (0.3 MPa) was adopted and the loading frequency was 10 Hz. The loading process have divided into two stages: In the first load stage, the load stops until the modulus decreases to 60% of the initial modulus. A duration of 30 min is required for the bitumen to heal. After the end of heal stage, a second load stage begins, and the test finally ends till the modulus decrease to about 60% of the initial modulus again. A typical test result is shown in Fig. 1. Based on the variation of the modulus the healing indexes can be obtained by the following equations:

$$\text{Healing index1} = \frac{G_{\text{heal}}^*}{G_{\text{initial}}^*} \quad (1)$$

$$\text{Healing index2 (Pa)} = (G_{\text{heal}}^* - G_{\text{damage}}^*)10^6 \quad (2)$$



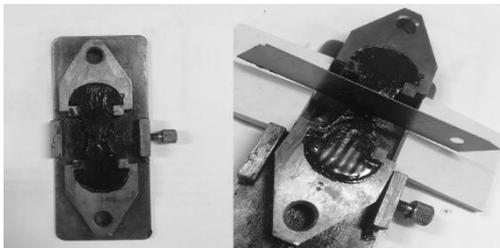
**Figure 1** Typical fatigue load test consequences

#### 2.4.2 Ductility Test

Ductility test was used to investigate the healing performance of microcapsules under low temperature condition according to ASTM D113-07. Test temperature was 5°C and tensile speed was adjusted at 1cm/min. Before the test, the samples should have a pre-cut crack about 4 mm depth and then a 4 hour duration time is needed for the samples to heal [18] A typical procedure is presented in Fig. 2. The low-temperature healing efficiency (HE) can be expressed by following Equation:

$$HE = \frac{L_{Heal}}{L_{Original}} \quad (3)$$

Where HE is the healing efficiency,  $L_{heal}$  is the ductility of the sample with pre-cut crack after healing for 4 hours, and  $L_{original}$  is the ductility of intact sample.



**Figure 2.** Preparation of sample for healing performance

### 3. Results

#### 3.1 Morphology

Urea formaldehyde (UF) resin successfully applied to fabricate microcapsules containing rejuvenator by the in situ polymerization method. The shell thickness, surface morphology and average size of microcapsules were controlled by regulating the core/shell ratio, pre-polymer adding speed and emulsion stirring rate. The microcapsules were fabricated with a core/shell ratio of 1/2 fabricated by 1500 r.min<sup>-1</sup> emulsion stirring rates.

Fig. 3 shows the SEM micrograph of microcapsules. The surface of microcapsule is rough and scraggly, and it is composed of UF nanoparticles protruding from the surface. The protuberant nanoparticles can increase the surface areas of microcapsules and enhance surface adhesion. It is observed that the organic core material is dispersed into particles in water and finally formed microcapsules with a mean sizes are about 100µm.

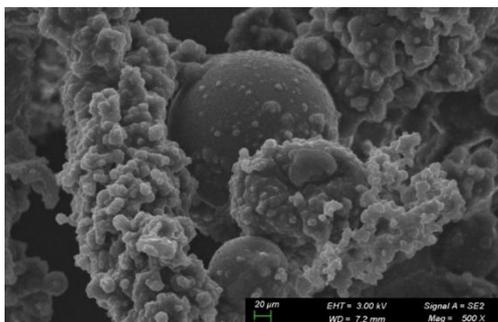


Figure 3. Morphology of microcapsules

### 3.2 Chemical Structural characterization of microcapsules

Fig. 4 presents the FTIR spectra of pre-polymer, a mixture of bitumen rejuvenator and UF core/shell material of microcapsules. As seen in Fig 4., the microcapsule has some different characteristic absorption peaks with bitumen rejuvenator, such as a vibration peak at 2917  $\text{cm}^{-1}$ , an absorption peak at 1739  $\text{cm}^{-1}$  and an absorption peak at 1176  $\text{cm}^{-1}$ . This indicates that the formation of the capsule shell has been established. In addition, some same characteristics peak with rejuvenator still exists, which fully verify that asphalt rejuvenator has been successfully covered by resin materials.

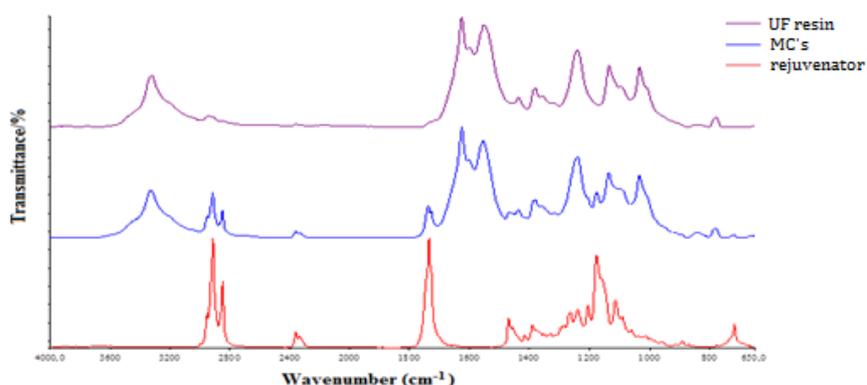


Figure 4. FTIR spectrogram of microcapsule and rejuvenator.

### 3.3 Self-healing performance

#### 3.3.1 Fatigue Test

Dynamic shear rheometer was used to investigate the healing properties of the control sample and the bitumen samples involving different amount of microcapsules (6, 8, 9, 10, 11 and 12%wt) Table 2 shows the healing performance of rejuvenator in bitumen under fatigue loading conditions.

As presented in Table 2, the complex modulus of bitumen containing rejuvenator depicts

variation with the increment in the amount of microcapsules. Moreover, after healing for 0.5 h, all asphalt samples containing different amounts of microcapsules displayed expected recovery performance. However, the recovery value of the modulus increased first and then decreased with the amount of microcapsules, and the asphalt containing 10%wt microcapsules had the maximum recovery value of 2.4 MPa, by contrast, the recovery value of control sample (0% microcapsules) was 1.27MPa.

Table2. The healing performance (fatigue load) of asphalt with microcapsules

Complex Modulus	Control sample (without microcapsule)	Bitumen sample involving microcapsule					
		6%	8%	9%	10%	11%	12%
G*Initial	2.002	2.1203	2.552	2.621	2.827	3.135	3.125
G*Damage	1.135	1.194	1.5172	1.435	1.635	1.805	1.791
G* heal	1.278	1.359	1.76972	1.923	2.394	2.491	2.427

Figure 5 presents the results of healing indexes. Based on Fig.5, both of the calculated healing indexes increase with increase in the rate of microcapsule up to 10%, however the index values depicts a decrease at 11 and 12 % microcapsule %. This indicates that 10%wt microcapsules content yields the better recovery results against the other contents of rejuvenator.

An appropriate amount of microcapsules can effectively recover the flexibility of asphalt to improve the anti-fatigue performance of the bitumen; however excessive microcapsules will lead to the unnecessary flow deformation and bring in failings after the separation of capsules.

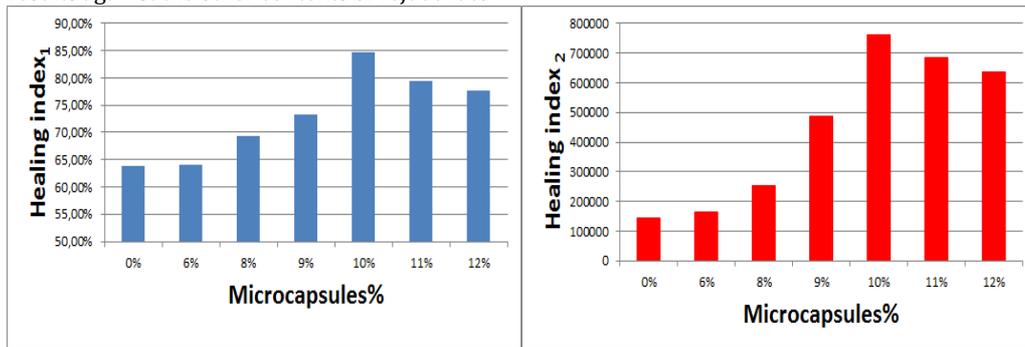


Figure 5. Healing Indexes based in microcapsule rate

### 3.3.2 Ductility Test

Ductility test was conducted with the 6, 8, 9, 10, 11 and 12 wt% additive amount of microcapsules and also pure bitumen to investigate the self-healing performance of bitumen under low-temperature condition. As shown in Figure 6, the healing efficiency HE increased first and then decreased with the additive amount of microcapsules. The healing

efficiency reached maximum as high as 84.25% when the additive amount of microcapsules was 10 wt% of the asphalt. The rejuvenator flowed out from the microcapsule to increase the liquidity of the asphalt, resulting in the increase of the ductility of asphalt. However, excessive microcapsule left too many holes in asphalt after the flow of rejuvenator, which led to the decrease of ductility of asphalt.

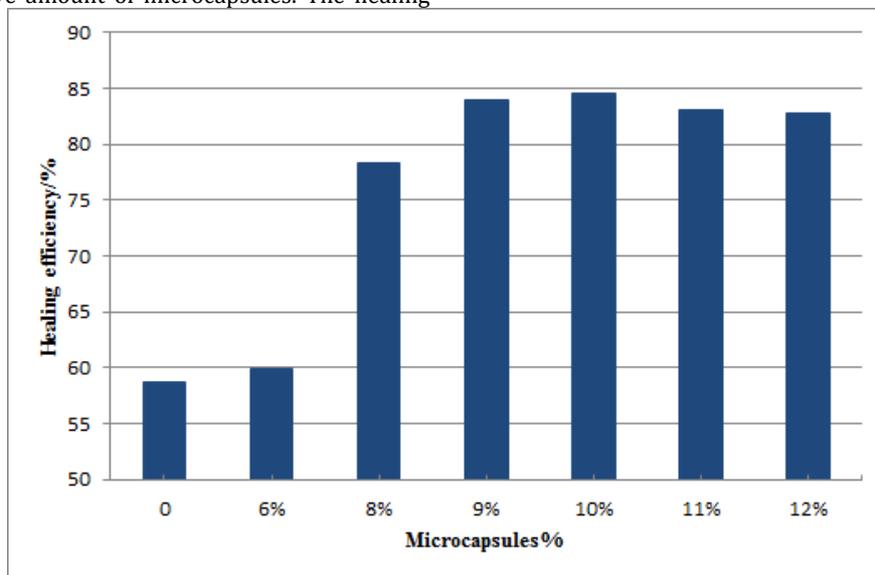


Figure 6. The healing performance of asphalt with microcapsules under low temperature conditions (5°C).

#### 4. Discussion and Conclusion

The self-healing and recovery behaviors of bitumen containing microcapsules had been investigated by using fatigue test and low temperature ductility test. The obtained values had been documented to evaluate the recovery efficiency of rejuvenated bitumen. The structure of microcapsules had been investigated to understanding the healing procedure of bitumen. Based on the test results, the following conclusions can be drawn.

(1) Microcapsules containing oily rejuvenator were successfully fabricated. They could be dispersed in bitumen homogeneously. Oily rejuvenator can easily penetrate and diffuse into bitumen.

(2) The morphology and chemical structure characterization of microcapsules indicate that the microcapsules containing the functional groups of the capsule wall and the capsule core and the cores are successfully coated. The microcapsules are fairly stable and can withstand the procedure of preparation of asphalt pavement.

(3) Fatigue load test was used to investigate the healing performance of the bitumen with different amount of microcapsules. The complex modulus of bitumen containing rejuvenator presents variance with the amount of microcapsules. All samples containing microcapsules displayed expected recovery performance. The recovery value of the modulus increased first and then decreased with the amount of microcapsules, and the bitumen containing 10%wt microcapsules demonstrates the maximum recovery value.

(4) Recovery test indicated that the microcapsules had good healing efficiency for the bitumen under conditions of low temperature. The healing efficiency increased up to 10% microcapsule rate; and then a slight decrease is maintained above 10%. It can be deduced that the optimal amount of microcapsules to show better performance was 10wt% of the bitumen.

(5) The conclusion of this research covers the preparation of UF microcapsules filled with rejuvenator and characterization of the mechanic properties of self healing asphalt. More research should be carried out by using different test methods such as penetration, softening point,

IZOD impact strength test and creep test in order to perform more validation.

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