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RESEARCH ARTICLE

Comparative analysis between FAR and ARL based control charts with runs rules

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Abstract

In this study, we have conducted comparative analysis between false alarm rate (FAR) and average run length (ARL) based control charts with runs rules. In this regard, we have considered various univariate and multivariate control charts which include mean, standard deviation, variance, Hotelling, and generalized variance. For evaluation purpose, we have used actual false alarm rate, power, in-control actual average run length, and out-of-control average run length as performance indicators. Furthermore, the performance indicators are calculated through Monte Carlo simulation procedures. Results revealed that performance order of runs rules with FAR based control charts are persistent whereas, performance order of runs rules with ARL based control charts are dependent on the circumstances, that is, sample size, size of shift, type of control chart, and side of control limit (upper-sided and lower-sided). Besides, we have provided a real life example using the data on electrical resistance of insulation. In this approach, we have determined that behavior of FAR and ARL based control charts using the real data is recorded similar to the behavior using the statistical performance indicators.

Mathematics Subject Classification (2020). 62N05, 62F10, 62F12, 62F15, 62F25, 62F40

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1. Introduction

The theory of control charts was first proposed by Walter A. Shewhart in 1931 [17] for the detection of assignable causes of variations in a parameter (location and dispersion) of a process characteristics. The assignable causes of variations are unnaturally appeared in an ongoing process, and they are usually occurred due to improper adjustment of controller, operators error, and low quality of batch material. A control chart based on the concept of Shewhart [17] is often known as Shewhart-type control chart. The Shewhart-type control chart based on classical runs rule (any single point out-of-control) is generally considered

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less efficient for detection of small variations in a parameter [13]. However, to increase the ability of Shewhart control charts towards detection of small variations, Western [21] recommended sensitizing rules or runs rules (also known as decision rules). With passage of time, various authors introduced new forms of sensitizing rules as well as explored their behavior in forms of actual in-control average run length (abbr. as AIARL and denoted as ARL_{act}) and out-of-control average run length (abbr. as OARL and denoted as ARL_1) such as [3–6,10,15,18–20]. The AIARL is an actual value of the average number of sample points that stayed in-control before declaring a process out-of-control on the basis of decision points when in-fact process is in-control. Furthermore, OARL is the average number of sample points that stayed in-control before declaring a process out-of-control on the basis of decision points when actually process is out-of-control.

Champ and Woodall [3] investigated the AIARL as well as OARL of different sensitizing rules. In addition, they used Markov Chain approach as computational technique. Their results showed that although simultaneously implementation of sensitizing rules enhanced the detection ability of Shewhart type control chart but at the same time generated another issue. The issue stated as AIARL deviated from intended level, that is, substantially degraded. To overcome the issue of sensitizing or runs rules, many authors recommended to incorporate the correct value of in-control probability of single point (abbr. as IPSP and denoted as p_0) into the design structure of Shewhart type control chart [4, 5, 8, 10, 15, 22]. The IPSP is defined as the probability of an out-of-control signal when in-fact a process is in-control. Furthermore, IPSP is generally computed through involving an appropriate method by taking into account an independent choice of runs rules and prefix value of FAR (denoted as α) or in-control ARL (denoted as ARL_0). The prefix value of α can be defined as the prefix value of probability of decision points for a given choice of runs rule when in-fact a process is in-control. On the other hand, ARL_0 is the prefix value of the average number of sample points that should be stayed in-control before declaring a process out-of-control on the basis of decision points when in-fact process is in-control.

The appropriate method for computing the IPSP is considered important in designing of Shewhart-type control charts. For instance, Klein [5] computed IPSP based on Markov chain approach for designing and evaluating the mean (\bar{X}) control chart. Khoo [4] established graphical plots based on Markov chain approach to obtain the IPSP of existing and proposed runs rules. In addition, he applied the probabilities of single point in the construction of \bar{X} control chart. Shepherd et al. [16] computed the IPSP based on Markov chain approach for designing and evaluation of attribute control chart under runs rules. In continuation, Riaz et al. [15] utilized the proposed equation for designing the FAR based upper-sided mean (symbolized as \bar{X}_U), variance (S_U^2) , standard deviation (S_U) and range (R_U) control charts. In addition, they showed that proposed equations play its role to maintain the AFAR of FAR based \bar{X}_U , S_U^2 , S_U and R_U control charts under runs rules at α . The applications of polynomial equation by [15] can be seen in various studies such as [9, 11, 12, 22]. In this particular research direction, Mehmood et al. [8] offered new polynomial equation alternative to the study by [15] for increasing the detection ability of two sided Shewhart-type control chart under runs rules.

The aforementioned literature review is representing the FAR and ARL based control charts. A control chart depends on the α is termed as FAR based control chart such as [15, 22]. Likewise, ARL based control chart depends on the ARL_0 such as [4,5]. It is valuable to mention that numbers of studies have been seen on the topic of FAR and ARL based control charts separately. In this research direction, it is very rare to find study on the comparative analysis between FAR and ARL based control charts. This has taken as the motivation of current study.

This study aims to conduct comparative analysis between FAR and ARL based control charts with runs rules. To achieve the goal, we will construct design structures of upper-sided and lower-sided univariate and multivariate control charts with runs rules.

The upper-sided and lower-sided univariate control charts include mean $(\bar{X}_U \text{ and } \bar{X}_L)$, variance $(S_U^2 \text{ and } S_L^2)$, and standard deviation $(S_U \text{ and } S_L)$. Furthermore, upper-sided and lower-sided multivariate control charts contain generalized variance $(|S|_U, \text{ and } |S|_L)$ and Hotelling's (T_U^2) . Besides, we will evaluate the performance of FAR and ARL based control charts by considering the AFAR, power (denoted as P_I), AIARL, and OARL as performance measures. The P_I is defined as the probability of the decision points for a given choice of runs rule that are declared out-of-control when in-fact the process is out-of-control. In addition, for computation of the performance measures, we will illustrate and also employ the Monte Carlo simulation procedures without loss of generality. Furthermore, we will conduct comparative analysis on the behavior of FAR and ARL based control charts under classical and additional runs rules. All of the prescribed methods for comparative analysis cover the statistical aspects of current study. To highlight the practical significance of the study, a real life example will be presented using the data on electrical resistance of insulation.

Rest of the article is organized as follows: In Section 2, we will construct different design structures of FAR and ARL based control charts with classical and additional runs rules. In Section 3, we will discuss Monte Carlo simulation procedure for computing different performance measures of each control chart under consideration, and also conduct comparative analysis. In Section 4, we will give a real life example using the data on electrical resistance of insulation to compare the behavior of FAR and ARL based control charts with runs rules. Lastly, we will summarize and conclude the whole study in Section 5.

2. Design structures of FAR and ARL based Shewhart-type control charts under runs rules

In this section, we construct FAR and ARL based design structures of the Shewhart-type control charts under runs rules. Now assume that a process characteristic X follows a normal distribution and characteristics (Y_1, Y_2) follow bivariate normal distribution.

2.1. $ar{X}_U$ control chart

Let \bar{X}_j , j=1,2,3,... denote the jth plotting statistic of sample of size n. Thus, a process is said be out-of-control if k/k or k/k+r consecutive statistic \bar{X}_j falling above the control limit $U_{\bar{X}}$. The \bar{X}_j and $U_{\bar{X}}$ are formulated as follows:

$$\bar{X}_j = \frac{1}{n} \sum_{i=1}^n X_{ij}, \quad U_{\bar{X}} = \mu_0 + Z_{(1-p_0)} \frac{\sigma_0}{\sqrt{n}},$$

where μ_0 and σ_0 are known in-control mean and standard deviation of X, $Z_{(1-p_0)}$ is $(1-p_0)$ th percentile of standard normal distribution [13]. Furthermore, choice of p_0 depends on the prefix value of k/k or k/k+r runs rules and α or ARL_0 . The correct value of p_0 is desired to sustain the α_{act} or ARL_{act} of a control chart at α or ARL_0 , respectively. To compute the required p_0 value, one of the best solutions provided by [15] in the form of a polynomial equation for handling the FAR based control charts. Riaz et al. [15] introduced exact polynomial equation for computing the required p_0 value as per the given choice of k/k or k/k+r and α . Thus, polynomial equation for computing the p_0 as per the given choice of k/k and α or ARL_0 are given as:

$$\begin{cases}
p_0 = \sqrt[k]{\alpha}, & \text{if } \alpha \text{ is given,} \\
ARL_0(1 - p_0)p_0^k + p_0^k - 1 = 0, & \text{if } ARL_0 \text{ is given.}
\end{cases}$$
(2.1)

To cover the case of k out of k+r (denoted as k/k+r, $r \ge 1$) runs rules, expressions to obtain p_0 for the given value of α or ARL_0 are as follows:

$$\begin{cases}
\alpha = \binom{k+r}{k} p_0^k (1 - p_0)^r, & \text{if } \alpha \text{ is given,} \\
p_0 = R(k|k+r, ARL_0), & \text{if } ARL_0 \text{ is given,}
\end{cases}$$
(2.2)

where $R(k|k+r, ARL_0)$ denote a constant, lies between zero and one, and it depends on the given value of k/k+r and ARL_0 . Besides, a control chart dependent on α is termed as FAR based control chart. Similarly, a control chart contingent on ARL_0 is called ARL based control chart. The theoretical justification of Eqs.(2.1)–(2.2) when α given can be seen in [8]. In addition, theoretical illustration of Eq.(2.1) when ARL_0 given is as follows: The probability distribution (also called run length distribution) of k/k consecutive statistics breached the control limit is generalized geometric distribution of order k with parameter p_0 [2]. As our interest is to find out correct value of p_0 so that ARL_{act} of a Shewhart-type control remains equal to ARL_0 . Therefore, we equate the mean of generalized geometric distribution of order k with parameter p_0 to ARL_0 . Note that value of p_0 in Eq. (2.2) when ARL_0 given is hard to obtain by analytical approach. However, one may calculate using a computational technique (e.g. Monte Carlo simulation) with a condition that ARL_{act} remains equal to ARL_0 .

2.2. \bar{X}_L control chart

Let \bar{X}_j , j=1,2,3,... denote the jth plotting statistic of sample of size n. Thus, a process is said be out-of-control if k/k or k/k+r consecutive \bar{X}_j falling below the $L_{\bar{X}}$. The \bar{X}_j and $L_{\bar{X}}$ are formulated as follows:

$$\bar{X}_j = \frac{1}{n} \sum_{i=1}^n X_{ij}, \quad L_{\bar{X}} = \mu_0 + Z_{p_0} \frac{\sigma_0}{\sqrt{n}},$$

where Z_{p_0} is p_0 th percentiles of standard normal distribution [13]. Rest of the discussion remained similar to Section 2.1.

2.3. S_U^2 and S_L^2 control charts

Let S_j^2 , j = 1,2,3,... denote the jth plotting statistic of sample of size n. Thus, a process is said be out-of-control if k/k or k/k + r consecutive S_j^2 crossed the control limit (U_{S^2} for S_U^2 or L_{S^2} for S_L^2 control chart). The S_j^2 , U_{S^2} , and U_{S^2} are formulated as follows:

$$S_j^2 = \frac{1}{n-1} \sum_{i=1}^n (X_{ij} - \bar{X}_j), \quad U_{S^2} = \frac{w_U \sigma_0^2}{n-1}, \quad L_{S^2} = \frac{w_L \sigma_0^2}{n-1},$$

where w_U and w_L are $(1 - p_0)$ th and p_0 th percentiles of chi-squared distribution with n - 1 degree of freedom, and σ_0^2 is known in-control variance of X.

2.4. S_U and S_L control charts

Let S_j , j = 1,2,3,... denote the jth plotting statistic of sample of size n. Thus, a process is said be out-of-control if k/k or k/k + r consecutive S_j falls outside the control limit (U_S for S_U or L_S for S_L control chart). The S_j , U_S , and L_S are formulated as follows:

$$S_j = \sqrt{\frac{\sum_{i=1}^n (X_{ij} - \bar{X}_j)}{n-1}}, \quad U_S = \frac{m_U \sigma_0}{\sqrt{n-1}}, \quad L_S = \frac{m_L \sigma_0}{\sqrt{n-1}},$$

where m_U and m_L are $(1 - p_0)$ th and p_0 th percentiles of chi distribution with n - 1 degree of freedom, and σ_0 is known in-control standard deviation of X.

2.5. Bivariate T_U^2 control chart

Let T_j^2 , j = 1,2,3,... denote the jth plotting statistic of sample of size n. Thus, a process is said be out-of-control if k/k or k/k + r consecutive T_j^2 lies beyond the U_{T^2} . The T_j^2 and U_{T^2} are formulated as follows:

$$T_i^2 = n(M_j - \mu_0)^t \Sigma_0^{-1} (M_j - \mu_0), \quad U_{T^2} = t_U^2,$$

where $M_j = (\bar{Y}_{1j}, \bar{Y}_{2j})^t$ is the jth sample mean vector, $\underline{\mu_0} = (\mu_{10}, \mu_{20})^t$ is known in-control mean vector of Y_1 and Y_2 , Σ_0 is variance-covariance matrix of M_j , and t_U^2 is $(1 - p_0)$ th percentile of chi-squared distribution with two degree of freedom.

2.6. Bivariate $|S|_U$ and $|S|_L$ control charts

Let $|S|_j$, j = 1,2,3,... denote the jth plotting statistic of sample of size n. Thus, a process is said be out-of-control if k/k or k/k + r consecutive $|S|_j$ falls outside the control limit $(U_{|S|}$ for $|S|_U$ or $L_{|S|}$ for $|S|_L$ control chart). The S_j , U_S , and L_S are formulated as follows:

$$|S|_j = S_{1j}^2 S_{2j}^2 - S_{12j}^2, \quad U_{|S|} = \frac{|\Sigma_0| \ b_U^2}{4(n-1)^2}, \quad L_{|S|} = \frac{|\Sigma_0| \ b_L^2}{4(n-1)^2},$$

where S_{1j}^2 and S_{2j}^2 are jth sample variance of size n, S_{12j}^2 is sample covariance between process characteristics $(Y_I \text{ and } Y_2)$, b_U and b_L are $(1-p_0)$ th and p_0 th percentiles of chi-squared distribution with 2n-4 degree of freedom, and $|\Sigma_0|$ is the determinants of Σ_0 .

3. Computation of performance measures and comparative analysis

In this section we are intended to provide Monte Carlo simulation procedure [7,15] for computing the performance measures of upper-sided and lower-sided control charts under runs rules (see Sec. 2), and also conduct comparative analysis. The performance measures are α_{act} , P_I , ARL_{act} , and ARL_I , and their further details are given in Sec. 1. A control chart for different choices of runs rules is said to be best if α_{act} or ARL_{act} is equal to α or ARL_o , respectively. Likewise, a control chart under different choices of runs rules can be announced best for a certain choice of runs rule if it attains minimum ARL_I or maximum P_I given that the control chart has same ARL_0 or α respectively.

3.1. \bar{X}_U and \bar{X}_L control charts

To compute the P_I of \bar{X}_U control chart, generate 10⁵ random samples of size n from normal distribution with out-of-control mean $\mu^* = \mu_0 + \delta_1 \sigma_0$ (where $\delta_1 \geq 0$ represents amount of upward shift) and in-control standard deviation σ_0 followed by calculating the plotting statistics (\bar{X}_i) and comparing them with $U_{\bar{X}}$ to count the number of statistics falling above the $U_{\bar{X}}$. Finally, proportion of plotting statistics falling above the $U_{\bar{X}}$ is reported as P_1 . Similarly, one may proceed for \bar{X}_L control chart by considering $L_{\bar{X}}$ with $\mu^* = \mu_0 + \delta_2 \sigma_0$ (where $\delta_2 \leq 0$ represents amount of downward shift). Furthermore, for computing the ARL_1 , generate a random sample of size n from normal distribution followed by calculating the statistics to compare with the $U_{\bar{X}}$ or $L_{\bar{X}}$ for deciding either process is in-control or out-of-control. Afterwards, repeat the prescribed procedure until the process is declared out-of-control and then record the sample number (run length). Likewise, repeat the aforementioned procedure 10⁵ times to attain the vector of run length. Ultimately, average of the vector of run length is required ARL_1 . Note that α_{act} and ARL_{act} is the special case of P_1 and ARL_1 , respectively when $\delta_1 = \delta_2 = 0$. Based on the aforesaid procedures, we have attained α_{act} , ARL_{act} , P_1 and ARL_1 of \bar{X}_U and \bar{X}_L control charts for some selective choices of δ_1 , δ_2 , n, $\alpha = 0.0027$, $ARL_0 = 370$, k/k and k/k + r (see Tables 1–3). Thus, the results are discussed as follows:

- The α_{act} and ARL_0 of mean control charts $(\bar{X}_U \text{ and } \bar{X}_L)$ are obtained equal to α and ARL_0 (i.e. $\alpha_{act} = \alpha = 0.0027$ and $ARL_{act} = ARL_0 = 370$) for classical and additional runs rules (see Table 1). This means that Eqs.(2.1)–(2.2) plays its role for resolving the issue of Shewhart-type control charts under runs rules. The details about the issue of Shewhart-type control charts are given in Sec. 1.
- Behavior of FAR based mean control charts with runs rules are sustained in terms of P_1 (see Tables 2–3). Similarly, we have observed for the case of ARL based mean control charts in terms of ARL_1 . These outcomes can be interpreted as detection ability of \bar{X}_U control chart is similar to the \bar{X}_L control chart when in-control process mean is shifted to new level with same magnitude of distance.
- The detection ability of FAR based mean control charts are observed uniformly higher for all choices of shifts ($\delta_1 > 0$ and $\delta_2 < 0$) in terms of P_1 when additional runs rules are employed as compared to 1/1 runs rule (see Tables 2–3). In continuation, detection ability of ARL based mean control charts are found higher for only small-to-moderate shifts (e.g. $0 < \delta_1 < 1$) in terms of ARL_1 when additional runs rules are implemented relative to classical runs rule. This implies that ARL based mean control charts are efficient towards detection of small-to-moderate shifts when additional runs rules are considered, and also efficient for large shifts when classical runs rule is incorporated.
- There are relationships between detection ability and choices of k/k, k/k + r, n, δ_1 and δ_2 (see Tables 2–3). For instance, detection ability of FAR based mean control charts uniformly increase as value of k/k increases. This remains valid for all choices of n, δ_1 and δ_2 . Also, detection ability of ARL based mean control charts increase as value of k/k increases.
- Among variant choices of runs rules, the 3/4 with mean control charts is proved efficient towards detection of small-to-moderate shifts relative to the other choices. Also, based on the detection ability in terms of ARL_1 and P_1 , performance order of runs rules with mean control charts is 3/4, 3/3, 2/4, 2/2, 2/3, and 1/1.

Table 1. α_{act} and ARL_{act} at $\alpha = 0.0027$, $ARL_0 = 370$, $\delta_1 = 0$, $\delta_2 = 0$, $\delta_3 = 0$	= 1,
$\delta_4 = 1, d^* = 1, d = 0, k/k \text{ and } k/k + r$	

	1/1		2/2		3/3		2/3		2/4		3/4	
	α_{act}	ARL_{act}										
\bar{X}_U	0.0027	370.37	0.0027	370.17	0.0027	370.14	0.0027	370.18	0.0027	370.10	0.0027	370.15
\bar{X}_L	0.0027	370.37	0.0027	370.17	0.0027	370.13	0.0027	370.43	0.0027	370.53	0.0027	370.10
S_U^2	0.0027	370.17	0.0027	370.60	0.0027	370.40	0.0027	370.63	0.0027	370.13	0.0027	370.72
$S_U^2 \ S_L^2$	0.0027	370.17	0.0027	370.17	0.0027	370.14	0.0027	370.18	0.0027	370.10	0.0027	370.43
S_U^-	0.0027	370.23	0.0027	370.31	0.0027	370.13	0.0027	370.43	0.0027	370.53	0.0027	371.20
S_L	0.0027	370.21	0.0027	370.28	0.0027	370.40	0.0027	370.63	0.0027	370.13	369.71	372.42
$ S _U$	0.0027	370.25	0.0027	370.17	0.0027	370.14	0.0027	370.18	0.0027	370.10	0.0027	371.31
$ S _L$	0.0027	370.37	0.0027	370.17	0.0027	370.13	0.0027	370.43	0.0027	370.41	0.0027	372.31
T_U^2	0.0027	370.37	0.0027	370.11	0.0027	370.40	0.0027	370.63	0.0027	370.20	0.0028	371.25

3.2. S_U^2 , S_L^2 , S_U , S_L , $|S|_L$ and $|S|_U$ control charts

The mechanism for computing P_1 and ARL_1 of S_L^2 and S_U^2 control charts is similar to \bar{X}_L and \bar{X}_U control charts except in-control mean is stable μ_0 , whereas in-control variance σ_0^2 is out-of-control, that is, $\sigma_1^2 = (\delta_3 \sigma_0)^2$ and $\sigma_1^2 = (\delta_4 \sigma_0)^2$, where $\delta_3 \geq 1$ and $\delta_4 \leq 1$ are upward and downward shift. Likewise, for S_U and S_L control charts, assume that the in-control mean is stable, whereas standard deviation is out-of-control $\sigma_1 = \delta_3 \sigma_0$ and $\sigma_1 = \delta_4 \sigma_0$. Besides, procedures for computing the power and out-of-control average run length of $|S|_L$ and $|S|_U$ control charts is to assume the μ_0 is stable, whereas Σ_0 is out-of-control

						$ar{X}_U$						
	1/1		2/2		3/3		2/3		2/4		3/4	
δ_1	$\overline{P_1}$	ARL_1	P_1	ARL_1	P_1	ARL_1	P_1	ARL_1	P_1	ARL_1	P_1	$\overline{ARL_1}$
0	0.0027	370.37	0.0027	370.76	0.0027	370.03	0.0026	372.02	0.0028	371.70	0.0027	369.47
0.05	0.0038	263.16	0.0042	240.47	0.0045	228.97	0.0043	243.52	0.0047	233.21	0.0048	225.25
0.1	0.0053	188.68	0.0065	159.79	0.0074	146.52	0.0069	155.64	0.0077	151.97	0.0082	136.01
0.15	0.0072	138.89	0.0097	108.75	0.0117	96.92	0.0107	106.06	0.0122	102.20	0.0136	89.33
0.2	0.0098	102.04	0.0142	75.73	0.018	66.16	0.0164	71.05	0.019	69.54	0.0219	59.05
0.25	0.0131	76.34	0.0204	53.9	0.027	46.6	0.0244	50.62	0.0288	48.99	0.034	41.87
0.3	0.0174	57.47	0.0288	39.23	0.0392	33.84	0.0355	36.90	0.0426	34.92	0.0513	29.75
0.35	0.0228	43.86	0.0398	29.19	0.0556	25.28	0.0505	27.64	0.0615	26.00	0.0747	21.88
0.4	0.0295	33.9	0.0539	22.19	0.0767	19.41	0.0702	20.55	0.0863	19.74	0.1056	17.12
1	0.2925	3.42	0.5316	3.22	0.6708	3.88	0.7029	3.11	0.8065	3.14	0.8406	3.611

Table 2. P_1 and ARL_1 of \bar{X}_U control chart at n=5, $\alpha=0.0027$, $ARL_0=370$, k/k, k/k+r and δ_1

Table 3. P_1 and ARL_1 of \bar{X}_L control chart at n=5, $\alpha=0.0027$, $ARL_0=370$, k/k, k/k+r and δ_2

						$ar{X}_L$						
	1/1		2/2		3/3		2/3		2/4		3/4	
δ_2	P_1	ARL_1	P_1	ARL_1	P_1	ARL_1	P_1	ARL_1	P_1	ARL_1	P_1	ARL_1
0	0.0027	370.37	0.0027	370.76	0.0027	370.03	0.0026	370.15	0.0028	369.27	0.0027	367.20
-0.05	0.0038	263.16	0.0042	240.47	0.0045	228.97	0.0043	239.73	0.0047	232.81	0.0048	219.60
-0.1	0.0053	188.68	0.0065	159.79	0.0074	146.52	0.0069	158.33	0.0077	148.88	0.0082	138.42
-0.15	0.0072	138.89	0.0097	108.75	0.0117	96.92	0.0107	106.96	0.0122	101.41	0.0136	89.84
-0.2	0.0098	102.04	0.0142	75.73	0.018	66.16	0.0164	71.94	0.019	68.35	0.0219	59.87
-0.25	0.0131	76.34	0.0204	53.9	0.027	46.6	0.0244	51.56	0.0288	48.12	0.034	42.35
-0.3	0.0174	57.47	0.0288	39.23	0.0392	33.84	0.0355	37.01	0.0426	34.98	0.0513	30.04
-0.35	0.0228	43.86	0.0398	29.19	0.0556	25.28	0.0505	27.25	0.0615	26.00	0.0747	22.00
-0.4	0.0295	33.9	0.0539	22.19	0.0767	19.41	0.0702	20.38	0.0863	20.11	0.1056	16.98
-1	0.2925	3.42	0.5316	3.22	0.6708	3.88	0.7029	3.1292	0.8065	3.12	0.8406	3.60

(say Σ_1), that is,

$$\underline{\mu_0} = \begin{bmatrix} \mu_{10} \\ \mu_{20} \end{bmatrix} \quad \text{and} \quad \Sigma_1 = \begin{bmatrix} \delta_5^2 \sigma_{10}^2 & \delta_5 \delta_6 \rho \sigma_{10} \sigma_{20} \\ \delta_5 \delta_6 \rho \sigma_{10} \sigma_{20} & \delta_6^2 \sigma_{20}^2 \end{bmatrix},$$

where $\delta_5^2 \geq 1$ and $\delta_6^2 \geq 1$ are amount of shifts in the in-control variances (σ_{10}^2 and σ_{20}^2), ρ is the amount of correlation between Y_1 and Y_2 . After that, generate random sample from bivariate normal distribution with μ_0 and Σ_1 followed by calculating the $|S|_U$ and comparing with the control limit ($U_{|S|}$ or $L_{|S|}$) to decide whether the process is in-control or out-of-control. Rest of the steps for computing P_1 and ARL_1 of $|S|_L$ and $|S|_U$ control charts are identical to \bar{X}_L and \bar{X}_U control charts. It is worthy to mention that detection ability of $|S|_L$ and $|S|_U$ control charts are dependent on the product of shifts $d^{*2} = \delta_5^2 \delta_6^2$ and n in respective of the choice of other quantities such as μ_0 , and Σ_1 . This property is termed as invariance property. Therefore, one may consider the product value of shift instead of assuming each shift separately. For comparative purpose, we have obtained α_{act} , ARL_{act} , P_1 and ARL_1 of S_U^2 , S_L^2 , S_U , S_L , $|S|_L$ and $|S|_U$ control charts at $\alpha = 0.0027$, $ARL_0 = 370$, various choices of k/k, k/k + r, δ_3 , δ_4 and d^* (see Tables 4–9). Note that α_{act} and ARL_{act} is the special case of P_1 and ARL_1 , respectively when $\delta_3 = \delta_4 = d^* = 1$. Now discussions on the behavior of S_U^2 , S_L^2 , S_U , S_L , $|S|_L$ and $|S|_U$ control charts are given in the following points:

• The α_{act} and ARL_1 of S_U^2 , S_L^2 , S_U , S_L , $|S|_L$ and $|S|_U$ control charts are obtained equal to prefix values of α and ARL_0 (i.e. $\alpha_{act} = \alpha = 0.0027$ and $ARL_{act} = ARL_0 = 370$) for classical and additional runs rules (see Table 1).

- The detection ability of FAR based S_U^2 and S_U control charts uniformly increases for small n (e.g. n < 5) in terms of P_I as value of k/k increases. In comparison, detection ability of ARL based S_U^2 and S_U control charts decreases for small n in terms of ARL_I as value of k/k increases. This may illustrate as the k/k runs rules are useful for FAR based S_U^2 and S_U control charts at any choice of n relative to 1/1 runs rule, whereas k/k runs rules are not beneficial for ARL based S_U^2 and S_U control charts when n is small. However, for $n \ge 5$, detection ability of ARL based S_U^2 and S_U control charts with 2/2 and 3/3 runs rules are seen higher at wide range of shifts relative to 1/1 runs rule (see Tables 4 & 6). Between runs rules, 2/2 results in higher detection ability of ARL based S_U^2 and S_U control charts as compared to 3/3.
- The diagnosing ability of FAR based $|S|_U$ control chart uniformly increases for small n (e.g. n < 5) in terms of P_I as value of k/k increases. In contrast, detection ability of ARL based $|S|_U$ control chart reduces for small n (e.g. n < 5) in terms of ARL_I as k/k increases. This may illustrate as k/k runs rules are useful for FAR based $|S|_U$ control chart relative to 1/1 runs rule at any choice of n, whereas k/k runs rules are not useful for ARL based $|S|_U$ control chart when n is small. However, for $n \ge 5$, detection ability of ARL based $|S|_U$ control chart under k/k runs rules is seen higher than 1/1 runs rule (see Table 8) at various choices of shifts $(1 < d^* < 1.50)$. Among k/k runs rules, 3/3 results in highest detection ability of ARL based $|S|_U$ control chart for $1 < d^* \le 1.20$ relative to 2/2. Similarly, 2/2 results into highest detection ability of ARL based $|S|_U$ control chart for $1.20 < d^* \le 2.5$ relative to 3/3.
- The detection ability of FAR based S_L^2 , S_L , and $|S|_L$ control charts are uniformly higher when additional runs rules are applied relative to classical runs rule (see Tables 5,7 & 9). Similarly, detection ability of ARL based S_L^2 , S_L , and $|S|_L$ control charts are observed maximum for small-to-moderate shifts when additional runs rules are employed.
- The n, δ_3 , δ_4 and d^* have an effect on the detection ability of S_U^2 , S_L^2 , S_U , S_L , $|S|_L$ and $|S|_U$ control charts. In simple words, detection ability of FAR and ARL based control charts increases in terms of P_I and ARL_I as size of n, δ_3 , δ_4 and/or d^* increases (see Tables 4–9).
- At several choices of small-to-moderate shifts $(\delta_3, \delta_4 \text{ and } d^*)$, either 2/4 or 3/4 runs rule is proved efficient with dispersion control charts relative to k/k runs rules in general. In terms of ARL_1 and P_1 , performance order of various runs rules with dispersion control charts is as follows: 2/4, 3/4, 2/3, 2/2, 3/3, 1/1 when S_U^2 and S_U ; 3/4 3/3, 2/2, 2/3 or 2/4, 1/1 when S_L^2 and S_L . Also, for $|S|_U$ and $|S|_L$ control charts, pattern of various runs rules are almost similar to S_U^2 and S_L^2 control charts.

Table 4. P_1 and ARL_1 of S_U^2 control chart at $n=5,~\alpha=0.0027,~ARL_0=370,~k/k,~k/k+r$ and δ_3

						S_U^2						
	1/1		2/2		3/3		2/3		2/4		3/4	
δ_3	P_1	ARL_1										
1	0.0027	370.37	0.0027	370.76	0.0027	370.02	0.0026	370.30	0.0028	369.33	0.0027	368.29
1.10	0.0096	104.13	0.0104	101.86	0.0109	103.72	0.0125	96.65	0.0149	88.38	0.0137	92.38
1.21	0.0255	39.261	0.029	39.24	0.0313	41.48	0.0398	34.36	0.0509	32.29	0.0452	34.14
1.32	0.0542	18.44	0.0632	19.36	0.0692	21.39	0.0946	17.09	0.1256	15.56	0.1086	17.26
1.44	0.0977	10.23	0.115	11.44	0.1263	13.21	0.1802	10.00	0.2417	9.42	0.2056	10.54
1.56	0.1552	6.44	0.1824	7.71	0.1998	9.28	0.2901	6.77	0.3853	6.50	0.3265	7.50
1.69	0.2235	4.47	0.2609	5.72	0.2841	7.14	0.4116	5.08	0.5335	4.91	0.4555	5.80
1.82	0.2985	3.35	0.3446	4.56	0.3724	5.87	0.5313	4.12	0.6665	3.988	0.5777	4.89
1.96	0.3757	2.66	0.4284	3.83	0.459	5.06	0.6391	3.48	0.7734	3.44	0.6835	4.31
4	0.9074	1.10	0.9302	2.11	0.9401	3.12	0.9941	2.08	0.9995	2.08	0.9958	3.06

Table 5. P_1 and ARL_1 of S_L^2 control chart at $n=5,~\alpha=0.0027,~ARL_0=370,~k/k$ and δ_4

						S_L^2						
	1/1		2/2		3/3		2/3		2/4		3/4	
δ_4	P_1	ARL_1										
0.04	1	7	1	1	1	3	1	2	1	2	1	3
0.36	0.1158	8.63	0.5922	2.94	0.8862	3.21	0.66	3.11	0.7173	3.25	0.9442	3.21
0.42	0.0676	14.79	0.3642	4.31	0.6797	3.80	0.41	4.57	0.4567	4.80	0.7674	3.73
0.49	0.0401	24.96	0.1995	7.06	0.4285	5.17	0.2238	7.43	0.2494	7.79	0.4996	5.08
0.56	0.0242	41.27	0.1015	12.57	0.2269	8.17	0.1115	13.04	0.1239	13.36	0.2646	7.98
0.64	0.015	66.75	0.0496	23.74	0.1053	14.75	0.0531	24.55	0.0586	24.92	0.1202	14.64
0.72	0.0095	105.62	0.0238	46.47	0.0447	29.78	0.0249	47.61	0.0272	46.70	0.0494	29.39
0.81	0.0061	163.65	0.0114	92.65	0.0179	65.52	0.0116	93.81	0.0126	93.50	0.0192	64.05
0.90	0.004	248.51	0.0055	185.72	0.007	152.93	0.0055	186.30	0.0059	187.79	0.0072	152.44
1	0.0027	370.37	0.0027	370.76	0.0027	370.02	0.0026	377.00	0.0028	368.91	0.0027	371.57

Table 6. P_1 and ARL_1 of S_U control chart at $n=5,~\alpha=0.0027,~ARL_0=370,~k/k,~k/k+r$ and δ_3

						S_U						
	1/1		2/2		3/3		2/3		2/4		3/4	
δ_3	$\overline{p_1}$	ARL_1	p_1	ARL_1								
1	0.0027	370.37	0.0027	370.76	0.0027	370.03	0.0026	373.71	0.0028	368.81	0.0027	368.77
1.05	0.0053	189.71	0.0055	186.51	0.0057	187.42	0.006	178.51	0.0068	171.72	0.0064	174.27
1.1	0.0094	106.93	0.0101	104.6	0.0106	106.43	0.0121	97.71	0.0144	90.02	0.0132	93.83
1.15	0.0153	65.22	0.017	64.13	0.0182	66.31	0.0219	58.28	0.027	54.83	0.0245	55.96
1.2	0.0235	42.49	0.0267	42.32	0.0288	44.57	0.0363	37.09	0.0462	34.82	0.0412	36.70
1.25	0.0342	29.25	0.0393	29.68	0.0428	31.87	0.056	25.72	0.0729	24.12	0.064	26.12
1.3	0.0474	21.09	0.055	21.89	0.0602	23.98	0.0814	19.12	0.1075	17.64	0.0933	19.00
1.35	0.0632	15.82	0.0739	16.85	0.0811	18.81	0.1123	14.67	0.1498	13.64	0.1288	15.26
1.4	0.0815	12.27	0.0956	13.43	0.1051	15.28	0.1482	11.62	0.1987	10.93	0.1696	12.32
2	0.3976	2.52	0.4515	3.68	0.4828	4.89	0.6667	3.36	0.7986	3.31	0.7099	4.17

Table 7. P_1 and ARL_1 of S_L control chart at $n=5,~\alpha=0.0027,~ARL_0=370,~k/k,~k/k+r$ and δ_4

						S_L						
	1/1		2/2		3/3		2/3		2/4		3/4	
δ_4	P_1	ARL_1										
0.2	0.5616	1.78	0.9977	2	1	3	0.9997	2.00	0.9999	2.016	1	3.00
0.6	0.0191	52.43	0.0716	17.09	0.1577	10.76	0.0777	17.48	0.086	17.67	0.1824	10.75
0.65	0.0141	70.76	0.0453	25.78	0.0951	16.01	0.0483	27.41	0.0533	26.43	0.1081	15.43
0.7	0.0107	93.65	0.029	38.76	0.0566	24.46	0.0305	39.11	0.0334	40.06	0.0631	24.44
0.75	0.0082	121.81	0.0188	57.9	0.0335	38.05	0.0195	59.30	0.0212	59.07	0.0366	36.74
0.8	0.0064	156.02	0.0124	85.76	0.0199	59.81	0.0127	87.37	0.0137	86.16	0.0213	58.85
0.85	0.0051	197.07	0.0083	125.74	0.0119	94.52	0.0084	127.79	0.009	127.99	0.0125	93.10
0.9	0.0041	245.86	0.0056	182.36	0.0072	149.48	0.0056	185.15	0.006	184.65	0.0074	148.47
0.95	0.0033	303.3	0.0039	261.5	0.0044	235.78	0.0038	264.10	0.0041	264.93	0.0044	237.43
1	0.0027	370.37	0.0027	370.76	0.0027	370.03	0.0026	373.48	0.0028	372.11	0.0027	367.01

						$ S _U$						
	1/1		2/2		3/3		2/3		2/4		3/4	
d^*	P_1	ARL_1										
1	0.0027	370.37	0.0027	370.76	0.0027	370.03	0.0026	370	0.0028	370	0.0027	370
1.05	0.0040	250.79	0.0042	244.81	0.0043	243.16	0.0043	238.69	0.0048	239.53	0.0046	234.54
1.1	0.0057	176.56	0.0061	169.22	0.0064	167.88	0.0067	161.21	0.0076	155.46	0.0073	156.97
1.15	0.0078	128.55	0.0086	121.66	0.0092	120.91	0.01	116.82	0.0116	107.89	0.0111	109.15
1.2	0.0104	96.37	0.0118	90.51	0.0128	90.29	0.0142	84.36	0.017	79.37	0.0161	79.05
1.25	0.0135	74.130	0.0157	69.36	0.0172	69.58	0.0196	62.81	0.0238	58.89	0.0225	60.14
1.3	0.0171	58.31	0.0203	54.55	0.0225	55.1	0.0262	49.84	0.0324	46.04	0.0305	47.18
1.35	0.0214	46.8	0.0256	43.88	0.0287	44.67	0.0341	38.97	0.0429	37.42	0.0401	37.07
1.4	0.0262	38.23	0.0318	36.02	0.0358	36.98	0.0434	32.20	0.0552	30.25	0.0514	30.76
2	0.1234	8.11	0.1572	8.74	0.1805	10.01	0.2447	7.67	0.3238	7.40	0.2889	8.23

Table 8. P_1 and ARL_1 of $|S|_U$ control chart at n = 5, $\alpha = 0.0027$, $ARL_0 = 370$, k/k, k/k + r and d^*

Table 9. P_1 and ARL_1 of $|S|_L$ control chart at n = 5, $\alpha = 0.0027$, $ARL_0 = 370$, k/k, k/k + r and d^*

						$ S _L$						
	1/1		2/2		3/3		2/3		2/4		3/4	
d^*	P_1	ARL_1										
0.2	0.1553	6.44	0.6141	2.87	0.8693	3.26	0.7119	2.93	0.7767	3.07	0.9426	3.22
0.6	0.0109	91.36	0.0265	42.13	0.0471	28.6	0.0287	43.38	0.0319	41.87	0.0542	27.44
0.65	0.0088	113.24	0.019	57.38	0.0318	39.98	0.0202	57.79	0.0224	57.09	0.0358	38.11
0.7	0.0072	138.38	0.0139	77.26	0.0216	55.79	0.0145	79.31	0.016	77.62	0.0239	53.49
0.75	0.006	167	0.0102	102.89	0.0149	77.58	0.0106	104.58	0.0116	102.30	0.0161	76.19
0.8	0.005	199.34	0.0077	135.57	0.0104	107.36	0.0078	139.23	0.0085	132.88	0.011	104.68
0.85	0.0042	235.62	0.0058	176.81	0.0073	147.72	0.0059	174.74	0.0063	172.15	0.0076	146.35
0.9	0.0036	276.07	0.0045	228.36	0.0052	201.98	0.0044	232.46	0.0048	228.26	0.0053	194.40
0.95	0.0031	320.91	0.0035	292.25	0.0037	274.33	0.0034	294.21	0.0037	286.50	0.0038	278.27
1	0.0027	370.37	0.0027	370.76	0.0027	370.03	0.0026	374.14	0.0028	369.12	0.0027	370.25

3.3. T_U^2 control chart

The procedure for computing the P_1 and ARL_1 of T_U^2 control chart is similar to $|S|_U$ and $|S|_U$ control charts except difference is at least one elements of $\underline{\mu}_0$ is shifted (say $\underline{\mu}_1$), whereas Σ_0 is stable, that is,

$$\underline{\mu_1} = \begin{bmatrix} \delta_7 \\ \delta_8 \end{bmatrix}, \ \delta_7 = \delta_8, \ \text{and} \ \Sigma_0 = \begin{bmatrix} \sigma_{10}^2 & \rho \sigma_{10} \sigma_{20} \\ \rho \sigma_{10} \sigma_{20} & \sigma_{20}^2 \end{bmatrix}$$

where $\delta_7 \in \Re$ and $\delta_8 \in \Re$ represent amount of shift in the in-control process means, thats is, μ_{10} and μ_{20} respectively. After that, generate random sample from bivariate normal distribution with μ_0 and Σ_1 followed by calculating the T_j^2 and comparing with U_{T^2} to decide whether the process is in-control or out-of-control. Rest of the steps for computing P_1 and ARL_1 of T_U^2 control chart are similar to \bar{X}_U control chart. It is valuable to mention that detection ability of T_U^2 control chart is dependent on the Mahalanobis distance d, that is,

$$d = \sqrt{(\mu_1 - \mu_0)^t \Sigma_0^{-1} (\mu_0 - \mu_1)},$$

and n in respective of the choice of other quantities (μ_1 , and Σ_0). This property is termed as directional invariance [14]. Therefore, we have considered shift in form of d as can be seen in many existing studies such as Mehmood et al. [7] and Pignatillo and Runger [14]. Also, for $\alpha = 0.0027$, $ARL_0 = 370$, and some choices of n, d, k/k and k/k + r, we have provided α_{act} , ARL_{act} , P_1 and ARL_1 in Table 10. Similarly one may proceed for other

choices of α , ARL_0 , n, d, k/k and k/k+r. Furthermore, results are described in following points:

- The α_{act} and ARL_1 of T_U^2 control chart are determined equal to α and ARL_0 (i.e. $\alpha_{act} = \alpha = 0.0027$ and $ARL_{act} = ARL_0 = 370$), respectively for classical and additional runs rules (see Table 1).
- The detection ability of FAR based T_U^2 control chart is uniformly outstanding at various choices of d when additional runs rules are plugged relative to classical runs rule in general. In comparison, ARL based T_U^2 control chart is noted superior for small-to-moderate d when additional runs rules are integrated relative to classical rule (see Table 10).
- The n and d are associated with the detection ability of T_U^2 control chart. It is summarized as detection ability of T_U^2 control chart in terms of P_1 and ARL_1 increases as size of n and/or d increases (see Table 10).
- The 2/4 runs rule is performed superb with T_U^2 control chart for detection of small-to-moderate d relative to the other runs rules schemes. Also, performance order of various runs rules is as follows: 2/4 is ranked at 1st position followed by 3/4 at 2nd, 2/3 at 3rd, 3/3 at 4th, 2/2 at 5th, and 1/1 at last.

Table 10. P_1 and ARL_1 of T_U^2 control chart at n = 5, $\alpha = 0.0027$, $ARL_0 = 370$, k/k, k/k + r and d.

						T_U^2						
	1/1		2/2		3/3		2/3		2/4		3/4	
d	P_1	ARL_1										
0	0.0027	370.37	0.0027	370.76	0.0027	370.03	0.0026	374.76	0.0028	367.76	0.0027	367.97
0.4	0.0094	106.89	0.011	97.04	0.0119	96.42	0.0173	72.709	0.0208	67.74	0.0198	69.14
0.5	0.0149	67.11	0.019	57.89	0.0215	57.15	0.0332	41.84	0.0411	37.78	0.0403	38.57
0.6	0.0236	42.34	0.0327	35.04	0.0387	34.54	0.0614	24.60	0.0778	22.67	0.0781	22.74
0.8	0.056	17.85	0.0884	14.35	0.1113	14.52	0.1756	9.74	0.2265	9.26	0.2324	9.31
0.9	0.0829	12.06	0.1362	9.86	0.1739	10.25	0.2682	6.85	0.3434	6.72	0.352	6.76
1	0.1191	8.4	0.1999	7.12	0.2558	7.67	0.3817	5.9	0.4802	4.10	0.4893	5.56
1.1	0.1657	6.03	0.2792	5.4	0.3542	6.05	0.5076	4.99	0.6214	3.15	0.628	4.41
1.2	0.2233	4.48	0.3714	4.29	0.4627	5.01	0.6335	3.78	0.7494	2.1	0.7515	3.72
1.4	0.3681	2.72	0.5728	3.05	0.6767	3.86	0.8383	2.8	0.9206	2	0.9161	2.15

4. Real life example

In this section, we conduct a comparative analysis between FAR and ARL based control charts with runs rules by using the practical data sets. The purpose of comparative analysis with aid of practical data sets is to know whether the behavior of FAR and ARL based control charts remains similar as described in Section 3 using the statistical performance indicators. To achieve the purpose, we consider a data set from Alwan [1] which refers back to [17] containing the data on 204 consecutive measurement on the electrical resistance of insulation in megohms. The data set is normally distributed with mean=4498.076 and the standard deviation=328. Afterwards, we have developed a code in R language to implement the FAR and ARL based \bar{X}_U control charts for $k/k = 1/1, 2/2, 3/3, \alpha = 0.0027$, and $ARL_0 = 370$ (see Figures 1–2).

The FAR based X_U control chart shows 3, 5 and 6 out-of-control signals for the 1/1, 2/2 and 3/3 runs rules, respectively (see Figure 1). It is worthy to mention that numbers of out-of-control signals given by ARL based \bar{X}_U control chart with varying choices of runs rules are equal to the case of FAR based \bar{X}_U control chart (see Figure 2). This indicates that behavior of FAR and ARL based \bar{X}_U control charts are identical. Also, additional runs rules contributes towards detection of small and moderate variations. This comparative

discussion is in accordance with the statistical results provided in Section 3.1. On the similar lines, one may attempt for the other choices of control charts.

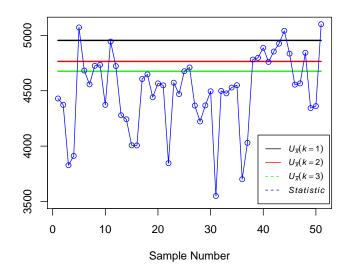


Figure 1. FAR based \bar{X}_U control chart for varying choices of runs rules (k = 1, 2, 3) and $\alpha = 0.0027$

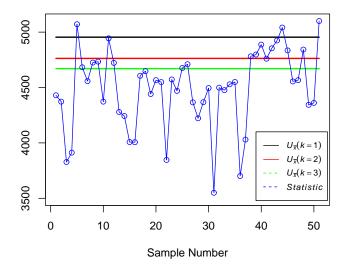


Figure 2. ARL based \bar{X}_U control chart for varying choices of runs rules (k = 1, 2, 3) and $ARL_0 = 370$

5. Summary, conclusions and future recommendations

In this article, we have described comparative behavior of false alarm rate (FAR) and average run length (ARL) based control charts with runs rules. In the list of univariate

and multivariate control charts, we have included upper-sided and lower-sided mean, variance, standard deviation, generalized variance, and Hotelling's. For comparative analysis and discussions, we have included actual false alarm rate, power, in-control actual average run length, and out-of-control average run length as performance measures. Furthermore, performance measures are computed by using Monte Carlo simulation procedures as computation methodology. Besides, diverse results are presented by taking into account numbers of factors. The detection ability of FAR based lower-sided and upper-sided control charts are remained uniformly higher when additional runs rule are incorporated relative to classical runs rule. Also, detection ability of ARL based lower-sided control charts are recorded outstanding for small-to-moderate shifts when additional runs rules are employed relative to classical runs rules. In brief, performance order of decision rules with FAR based lower-sided and upper-sided control charts are persistent, whereas performance order of decision rules with ARL based control charts are dependent on the circumstances, that is, sample size, size of shift, class of control chart (location and dispersion), and side of control limit (upper-sided and lower-sided). Lastly, we have provided a real life example using the data on electrical resistance of insulation. In the real life example, we have recorded that behavior of FAR and ARL based control charts using the real data sets are similar to the behavior using the statistical measures.

The scope of current study covers the processes in which characteristics follows normal distribution and parameters are known. It is often that process distribution is non-normal or unknown, and parameters are unknown. Therefore, it would be excellent to conduct an efficient study in future for non-normal distribution and parameters are unknown. Likewise, one may contribute a study by involving robust techniques (e.g. robust estimators and non-parametric) with control charts. An interesting study can be added on the topic of comparative analysis between cumulative sum (CUSUM) and exponentially weighted moving average (EWMA) control charts with runs rules.

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