



SAKARYA ÜNİVERSİTESİ

# FEN BİLİMLERİ ENSTİTÜSÜ DERGİSİ

Sakarya University Journal of Science  
SAUJS

e-ISSN 2147-835X | Period Bimonthly | Founded: 1997 | Publisher Sakarya University |  
<http://www.saujs.sakarya.edu.tr/en/>

Title: Parameter Optimization of Frequency Selective Surfaces Made of Composite Materials

Authors: Abdullah Oğuz KIZILÇAY

Received: 2020-10-28 00:00:00

Accepted: 2021-02-03 00:00:00

Article Type: Research Article

Volume: 25

Issue: 2

Month: April

Year: 2021

Pages: 357-363

How to cite

Abdullah Oğuz KIZILÇAY; (2021), Parameter Optimization of Frequency Selective Surfaces Made of Composite Materials. Sakarya University Journal of Science, 25(2), 357-363, DOI: <https://doi.org/10.16984/saufenbilder.817605>

Access link

<http://www.saujs.sakarya.edu.tr/en/pub/issue/60672/817605>

New submission to SAUJS

<https://dergipark.org.tr/en/journal/1115/submission/step/manuscript/new>

## Parameter Optimization of Frequency Selective Surfaces Made of Composite Materials

Abdullah Oğuz KIZILÇAY\*<sup>1</sup>

### Abstract

Debye model is used for approximating the frequency dependent complex effective permittivity of the composite structures in filter and shielding applications at microwave frequencies. In Debye model, desired shielding effectiveness (SE) is obtained by determining the Debye parameters using trial and error method. But this may result in wasting time or not converging to an optimum solution. In this work to overcome this problem Debye parameters were optimized by using Differential Evolution (DE) algorithm. A Maxwell Garnett (MG) mixing rule was applied to these optimized parameters to obtain frequency selective surface (FSS) parameters. 12dB shielding threshold was chosen between 0.05 – 5GHz frequency range. In accordance with the obtained parameters of FSS, a structure was designed in CST simulation software and simulations had been conducted to obtain SE results. It was seen that the results obtained from analytical computations agree with those obtained from simulations.

**Keywords:** Frequency selective surface, Debye model, composite material, differential evolution algorithm

### 1. INTRODUCTION

Composite structures which include conductive inclusions such as carbon rods, spheres have become widely used materials in electromagnetic (EM) shielding problems. Filters, integrated

optical microwave guides, thin films, memory devices, new generation antennas, radar absorbing materials can be counted as application areas where composite structure are used [1-6].

Covering such a wide usage area makes researchers more involved in this subject.

Currently, many composite shield materials are designed with random parameters and numerically analyzed with software like CST, HFSS, FEKO and etc [7-8]. The obtained results are checked whether they meet expectations, before production process is initiated. However, these commercial simulation programs conducted with trial error method do not bring success and

\*Corresponding author: oguzkizilcay@yyu.edu.tr

<sup>1</sup>Van Yuzuncu Yil University, Engineering Faculty, Electrical and Electronics Engineering Department, 65080, Van, Turkey , E-Mail: oguzkizilcay@yyu.edu.tr  
ORCID: <https://orcid.org/0000-0002-7607-0924>

they also waste time. Fortunately, heuristic algorithms have a special place as an alternative way of overcoming similar problems.

One of the simplest optimization heuristic algorithms is Differential Evolution algorithm [9]. It was derived from genetic algorithm which can be come across widely in literature. Compared to its counterparts, DE algorithm is relatively easy to apply on problems. In this work, since there were few parameters to be optimized, DE was used.

The main principle of DE is to find local minimum or local maximum value of cost function. Thus, it would be easy to find maximum shielding with given Debye parameters. However, the main feature of FSS is to shield waves in specific frequency band. Because of that, in our case algorithm will converge to desired shielding effectiveness in 0.5 - 5GHz frequency range.

In literature, design parameters of shield materials developed by using Debye model are determined by trial error method. Also, researchers investigating different mathematical approaches did not make use of optimization method either. Seager [3] in his work produce FSS by sewing fiber on fabric. Mannaa and Aldhaferi [5] proposed FSS design aiming to shield GSM 900 and 1800 MHz frequencies. Ghosh et. al. [10] derived transmission line model for their FSS design. Kiermier and Biebl [6] also developed a transmission line model and calculated cutoff frequencies. They aimed to shield GSM and WLAN frequencies. Wang et al. [4] computed the shielding effectiveness of homogenous composite materials with cylindrical inclusions by FDTD method. They observed frequency selective attributes of composite materials. Nisanci et. al. [11] in their work analyzed the effect of physical and electrical parameters of composite structure on shielding efficiency. The common point of all these studies is that produced FSS models were developed by trial and error method. Therefore, literature lacks analytical or optimized solution in designing FSS structure. This work will be promising in optimizing the parameters needed in FSS design.

Within the scope of the study firstly the boundaries of Debye parameters and of physical parameters of material were defined. After, optimum values were selected from inside the boundaries by DE algorithm. These values were put into MG equations to get physical dimensions of FSS model. Proposed FSS was tested with numerical method FDDT widely used in solving EM problems.

## 2. MATERIALS AND METHODS

Dielectric materials or composite materials with dielectric properties have low reflection loss and considerably absorption loss [12-14]. The dielectric of the material directly affects its conductivity, the impedance of the environment and thus the propagation of the EM wave. One of the models that associate this relation with the shielding effect is Debye model.

### 2.1. Debye Parameters in SE calculation

Dielectric varies depending on frequency [15]. The dielectric of the composite material according to the single-term Debye model is defined as

$$\varepsilon_D = \varepsilon_\infty + \frac{\varepsilon_s - \varepsilon_\infty}{1 + j\omega\tau} \quad (1)$$

$$\tau = \frac{1 + \sqrt{2}}{2\pi F_{Low}} \quad (2)$$

where  $\varepsilon_s$  is the static relative permittivity,  $\varepsilon_\infty$  is the relative high-frequency limit permittivity,  $\tau$  is the relaxation time,  $F_{Low}$  is the lowest boundary and  $\varepsilon_D$  is the complex frequency dependent relative permittivity of the equivalent homogeneous material described by the single-term Debye model [16-17]. In shielding problems  $\varepsilon_D$  determines the impedance of the material.

$$Z_m = Z_0 / \sqrt{\varepsilon_D} \quad (3)$$

where  $Z_m$  is the impedance of the material. Reflection and transmission at the boundaries in depends on the impedance of the material.

$$R_1 = \frac{Z_m - Z_n}{Z_m + Z_n} \quad (4)$$

$$R_2 = \frac{Z_0 - Z_m}{Z_0 + Z_m} \quad (5)$$

$$T_1 = \frac{2Z_m}{Z_m + Z_0} \quad (6)$$

$$T_2 = \frac{2Z_0}{Z_m + Z_0} \quad (7)$$

where  $R_{1,2}$  and  $T_{1,2}$  are reflection and transmission coefficients respectively.

Total transmittance depends on reflection coefficients  $R_{1,2}$  and transmission coefficients  $T_{1,2}$ . These quantities are defined as [1],[17-18].

$$T = \frac{T_1 T_2 e^{-\gamma_m W}}{1 + R_1 R_2 e^{-2\gamma_m W}} \quad (8)$$

$$\gamma_m = j\omega \sqrt{\mu_0 \epsilon_0} \sqrt{\epsilon_D} \quad (9)$$

where  $\gamma_m$  is the propagation constant. And the relation between SE with transmittance is as follows.

$$SE = -20 \log(|T|) \quad (10)$$

As can be seen from Equation 2-9,  $\epsilon_D$  in the Debye model can be used to determine the SE value. Therefore, it is possible to find the desired SE value by changing the value of  $\epsilon_D$ .

Debye parameters and physical properties of FSS describe the flatness and the strength of SE.  $b_\infty$  is the parameter that determines the flatness of SE. This parameter is defined as

$$b_\infty = \frac{(\epsilon_s - \epsilon_\infty)W}{2 \cdot c_0 \cdot \tau \sqrt{\epsilon_\infty}} \quad (11)$$

where  $b_\infty$  is dependent on  $\epsilon_s$ ,  $\epsilon_\infty$  and  $W$  values which will be involved in optimization processes.  $b \in [0.8 - 1.6]$  ensures the flatness of shielding line [16] above the threshold between the  $F_{Low}$  and  $F_{High}$  which were set to 0.5GHz and 5GHz respectively.

## 2.2. Differential Evolution Algorithm

The algorithm has the following steps: Initialization, Mutation, Recombination, Selection and Termination [9], [21].

### 2.2.1. Initialization

In this stage constant values are defined as:

Number of individuals,  $NP \geq 4$

Crossover ratio,  $CR \in [0 \ 1]$

Mutation factor,  $F \in [0 \ 2]$

Generation number,  $G$

### 2.2.2. Mutation

First, target individual is selected. Then 3 random distinct individuals inside population  $x_{r_1,G}$ ,  $x_{r_2,G}$  and  $x_{r_3,G}$  are selected so that  $r_1 \neq r_2 \neq r_3 \neq target$ .

Create a trial individual by adding weighted difference of 2 randomly selected individuals to third one.

$$V = x_{r_1} + F \cdot (x_{r_2} - x_{r_3}) \quad (12)$$

### 2.2.3. Recombination

The values of parameters inside trial individual are replaced with the value of corresponding parameter inside target individual with probability CR.

$$u_{j,i,G+1} = \begin{cases} u_{j,i,G+1} & \text{if } rand_{j,i} \leq CR \text{ or } j = I_{rand} \\ x_{j,i,G} & \text{if } rand_{j,i} > CR \text{ and } j \neq I_{rand} \end{cases} \quad (13)$$

where  $i = 1, 2, \dots, NP$ ;  $j = 1, 2, \dots, D$ ;  $rand_{j,i} \sim U[0 \ 1]$  and  $I_{rand}$  is a random integer from in  $[1, 2, \dots, D]$ .  $D$  is the solution's dimension.

### 2.2.4. Selection

The calculated cost value of target individual is compared with the one of trial vector  $V$ . A vector with better cost value is admitted to the next generation.

### 2.2.5. Termination

The algorithm terminates when the defined generation number is reached or stopping criteria is met.

### 2.3. Optimizing Parameters

The main purpose of the optimization is to obtain the physical properties of the shielding material. Additionally, final output must be available in the market or can be produced by use of composites. Therefore, computations must be carried out regarding these cases. For this, boundaries of Debye parameters were chosen specifically.

In order to start the algorithm several configurations must be done. Accordingly, width  $W \in [1 \text{ } 4]mm$ , dielectric constant  $\epsilon_{\infty} \in [1 \text{ } 100]$  and Debye parameter  $\epsilon_s \in [1000 \text{ } 4000]$  was set [16] and DE algorithm parameters were initialized. The pseudocode of the algorithm is given in the Appendix.

As it is seen from the pseudocode the algorithm converges to the solution in iteration T. A variable T was assigned as 20, which was adequate to find the solution. A case of failure may be faced with if only desired shielding is unattainable because of narrow boundaries of Debye parameters. In this case, desired shielding should be lowered or Debye parameters boundaries should be widened. After, algorithm may be initiated from the beginning.

Population size was determined as 20 and they filled with random numbers not exceeding boundaries. Inside iteration, a random target individual was chosen among individuals in population. Once a target individual was chosen it was exposed to mutation and recombination which resulted in new individual called trial vector. Afterwards the fitness of trial vector was evaluated at frequency  $F_{Low}$ . The fitness results included SE and b values. If newly found SE was greater than desired SE, then trial vector is reevaluated and SE was checked whether it was greater than desired SE for whole frequency range from  $F_{Low}$  to  $F_{High}$ . In case of failure, code would run from the beginning of current loop and another target would be chosen for further operations. However, in case of success and if variable b fitted in its defined boundaries then the code will print results and terminate.

### 3. RESULTS AND DISCUSSION

As a result of code run, Debye parameters were found as  $\epsilon_{\infty} = 11.056$ ,  $\epsilon_s = 3826$ ,  $W = 3.97mm$ . The host permittivity was chosen as  $\epsilon_e = 11.5$  that is close to permittivity of inclusion. It was determined with accordance of availability of this material. Other physical parameters of shield material was found by evaluating Debye parameters in Maxwell Garnet equations [22-23]. As a result of computation, physical parameters of material were found as  $s = W/4$ , conductivity  $\sigma = 103.93 S/m$ , length  $l = 177.7mm$  and radius  $r = 0.46mm$ . Figure 1a shows physical dimensions of every single inclusion.

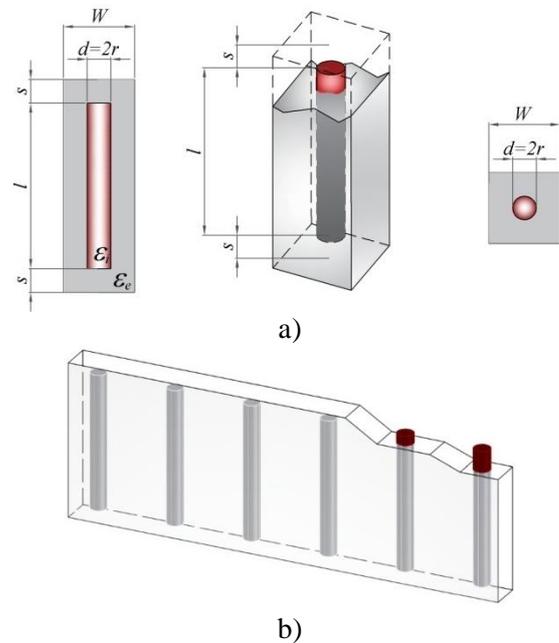


Figure 1. a) Cylindrical inclusion and its extent, b) 3D shielding material

Obtained physical parameters indicated low conductive dielectric material. 3D FSS (Figure 1b) was designed in CST simulation software [24], where electric field polarized plane wave excitation was used. Electric field probe was placed behind the shielding material. After setting other physical parameters, simulation was started (Figure 2).

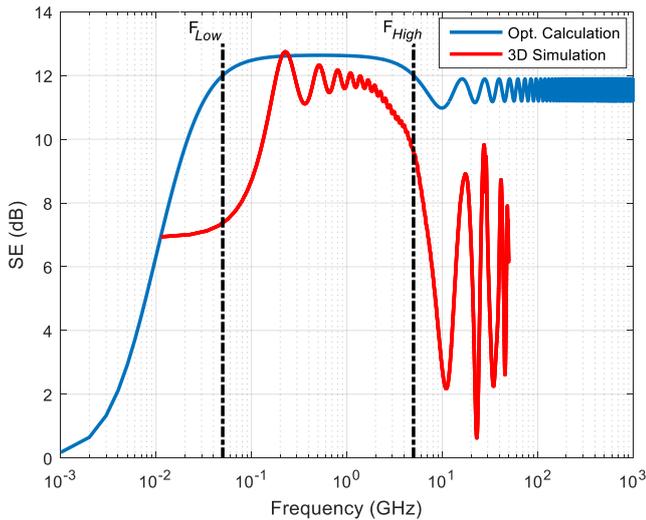


Figure 2. Comparison of Debye model with CST simulation

Debye parameters were evaluated in Eq. 1-10 and obtained SE values were simulated as in Figure 2. It is obvious that SE above threshold is quite flat. This is also guaranteed by value  $b$  which was found as 0.98.

In the Figure a red line indicates the simulation result whereas blue line indicates the optimized calculation. As it is seen from Figure, between  $F_{Low}$  and  $F_{High}$ , CST simulation results are similar to those obtained by analytical computation.

#### 4. CONCLUSION

In this work, despite traditional trial and error method, Debye parameters were optimized with the help of Differential Evolution algorithm and obtained in a much faster and precise way. Afterwards, in order to obtain physical parameters of FSS, these parameters were evaluated in Maxwell Garnett solutions. Then, a shield was modeled and simulated in CST Studio software which analysis EM interference problems with FDTD method. The SE results from proposed work and simulation was compared. It was seen that they nearly overlapped between  $F_{Low}$  and  $F_{High}$ . It can be concluded that, the performance of thought shield model can be predicted before production. This will save time and ease the computation process.

#### Appendix

A pseudocode given below is referred in section 2.3. It describes an implementation of DE algorithm on Debye parameters.

initialize algorithm, define Debye parameters and set their boundaries

for (iteration from 1 to T)

    for (target from 1 to population)

        determine target

        follow mutation and recombination steps

        evaluate trial vector fitness at  $F_{Low}$

        if ( $SE \geq desiredSE$ )

            target = trial

            for (frequencies from  $F_{Low}$  to  $F_{High}$ )

                evaluate trial vector fitness at  $F$

                if ( $SE < desiredSE$ )

                    set flag

                    break loop

                end

            end

            if(not set flag &&  $b \in [0.8 - 1.6]$ )

                set foundFlag

                break loop

            end

        end

    end

    if(foundFlag)

        break loop

    end

end

print target

#### Funding

The author(s) has no received any financial support for the research, authorship or publication of this study.

#### The Declaration of Conflict of Interest/Common Interest

No conflict of interest or common interest has been declared by the authors.

#### Authors' Contribution

The authors contributed equally to the study

***The Declaration of Ethics Committee Approval***

This study does not require ethics committee permission or any special permission

***The Declaration of Research and Publication Ethics***

The authors of the paper declare that they comply with the scientific, ethical and quotation rules of SAUJS in all processes of the paper and that they do not make any falsification on the data collected. In addition, they declare that Sakarya University Journal of Science and its editorial board have no responsibility for any ethical violations that may be encountered, and that this study has not been evaluated in any academic publication environment other than Sakarya University Journal of Science.

**REFERENCES**

- [1] B. Kanberoğlu, M. H. Nisanci, A. Ş. Demirkıran. "Electromagnetic characterization of ceramic material produced with natural zeolite", *Materials Science in Semiconductor Processing*, Vol.38, pp.352, 2015.
- [2] M. H. Nisanci, F. De Paulis, D. Di Febo, and A. Orlandi, "Synthesis of composite materials with conductive aligned cylindrical inclusions," *Prog. Electromagn. Res. Symp.*, no. May 2015, pp. 646–649, 2012.
- [3] R. D. Seager, A. Chauraya, J. Bowman, M. Broughton, and N. Nimkulrat, "Fabrication of fabric based Frequency Selective Surfaces (FSS)," *8th Eur. Conf. Antennas Propagation, EuCAP 2014*, no. September 2017, pp. 1978–1980, 2014.
- [4] J. Wang, B. Zhou, L. Shi, C. Gao, and B. Chen, "Analyzing the electromagnetic performances of composite materials with the FDTD method," *IEEE Trans. Antennas Propag.*, vol. 61, no. 5, pp. 2646–2654, 2013.
- [5] Y. Manna and R. W. Aldhaheri, "New dual-band frequency selective surface for GSM shielding in secure-electromagnetic buildings using square loop fractal configurations," *Mediterr. Microw. Symp.*, pp. 1–4, 2017.
- [6] W. Kiermeier and E. Biebl, "New dual-band frequency selective surfaces for GSM frequency shielding," *Proc. 37th Eur. Microw. Conf. EUMC*, no. October, pp. 222–225, 2007.
- [7] S. Kovar, J. Valouch, H. Urbancokova, M. Adamek, and V. Mach, "Simulation of Shielding Effectiveness of Materials Using CST Studio," *Wseas Trans. Commun.*, vol. 16, pp. 131–136, 2017.
- [8] E. Delihanlar and A. H. Yuzer, "Wearable Textile Fabric Based 3D Metamaterials Absorber in X-Band," vol. 35, no. 2, pp. 230–236, 2020.
- [9] R. Storn and K. Price, "Differential Evolution - A Simple and Efficient Heuristic for Global Optimization over Continuous Spaces," *J. Glob. Optim.*, vol. 11, pp. 341–359, 1997.
- [10] S. Ghosh and S. Lim, "Fluidically reconfigurable multifunctional frequency-selective surface with miniaturization Characteristic," *IEEE Trans. Microw. Theory Tech.*, vol. 66, no. 8, pp. 3857–3865, 2018.
- [11] M. H. Nisanci, F. De Paulis, D. Di Febo, and A. Orlandi, "Sensitivity analysis of electromagnetic transmission, reflection and absorption coefficients for biphasic composite structures," *IEEE Int. Symp. Electromagn. Compat.*, vol. 0, pp. 438–443, 2014.
- [12] D.D.L. Chung, "Materials for Electromagnetic Interference Shielding," *J. Mater. Eng. Perform.*, vol. 9, no. 3, pp. 350–354, 2000.
- [13] Y. Akinay and A. O. Kizilcay,

- “Computation and modeling of microwave absorbing CuO/graphene nanocomposites” *Polym. Compos.*, vol. 41, no. 1, pp. 227–232, 2020.
- [14] S. Kashi, R. K. Gupta, T. Baum, N. Kao, and S. N. Bhattacharya, “Dielectric properties and electromagnetic interference shielding effectiveness of graphene-based biodegradable nanocomposites,” *Mater. Des.*, vol. 109, no. February 2018, pp. 68–78, 2016.
- [15] E. Delihasanlar and A. H. Yuzer, “Simulation modelling and calculation of dielectric permittivity of Opuntia at 1.7–2.6 GHz,” *J. Microw. Power Electromagn. Energy*, vol. 51, no. 2, pp. 150–158, 2017.
- [16] F. De Paulis, M. H. Nisanci, A. Orlandi, M. Y. Koledintseva, and J. L. Drewniak, “Design of homogeneous and composite materials from shielding effectiveness specifications,” *IEEE Trans. Electromagn. Compat.*, vol. 56, no. 2, pp. 343–351, 2014.
- [17] C. D. Erbaş and S. Kent, “Ekranlama Verimliliği Karakteristiği Baz Alınarak Madde Sentezlenmesi İçin Analitik Bir Yaklaşım,” *Uludağ Univ. J. Fac. Eng.*, vol. 22, no. 1, pp. 95–95, 2017.
- [18] N. N. Rao, *Elements of Engineering Electromagnetics*, Fifth Ed. Upper Saddle River, NJ: Prentice-Hall, Inc, 2000.
- [19] L. Jebaraj, C. Venkatesan, I. Soubache, and C. C. A. Rajan, “Application of differential evolution algorithm in static and dynamic economic or emission dispatch problem: A review,” *Renew. Sustain. Energy Rev.*, vol. 77, no. March 2020, pp. 1206–1220, 2017.
- [20] H. Lei, L. Li, and C. H. Wu, “Evolutionary model selection and parameter estimation for protein-protein interaction network based on differential evolution algorithm,” *IEEE/ACM Trans. Comput. Biol. Bioinforma.*, vol. 12, no. 3, pp. 622–631, 2015.
- [21] D. Karaboğa and S. Ökdem, “A simple and global optimization algorithm for engineering problems: Differential evolution algorithm,” *Turkish J. Electr. Eng. Comput. Sci.*, vol. 12, no. 1, pp. 53–60, 2004.
- [22] A. . De Paulis, Francesco; Nisanci, M. Hilmi; Koledintseva, M.Y.; Drewniak, J.L.; Orlandi, “Derivation of Homogeneous Permittivity of Cal Inclusions for Causal Electromagnetic,” vol. 37, no. July 2011, pp. 205–235, 2012.
- [23] D. Micheli, A. Vricella, R. Pastore, and M. Marchetti, “Synthesis and electromagnetic characterization of frequency selective radar absorbing materials using carbon nanopowders,” *Carbon N. Y.*, vol. 77, pp. 756–774, 2014.
- [24] Computer Simulation Technology, CST Studio Suite 2019, Available: <http://www.cst.com/>