

# Distortion-Free CV/CC AC Power Supply Having the Unity Input Power Factor by the Use of Variable Capacitance Devices

Akihiko Katsuki<sup>\*‡</sup>, Koichiro Yoshimatsu<sup>\*\*</sup>, Hidetaka Tanoue<sup>\*\*</sup>, Yuichi Sugimoto<sup>\*\*</sup>

<sup>\*</sup>Next Generation Switching Power Course, Faculty of Engineering, Nagasaki University, 1-14, Bunkyo-machi, Nagasaki, 852-8521 Japan

<sup>\*\*</sup>Department of Computer Science and Electronics, Faculty of Computer Science and Systems Engineering, Kyushu Institute of Technology, 680-4, Kawazu, Iizuka-shi, Fukuoka, 820-8502 Japan

katsuki@nagasaki-u.ac.jp, yoshimatsu@scorpio10.cse.kyutech.ac.jp, tanoue@scorpio10.cse.kyutech.ac.jp, sugimoto@scorpio10.cse.kyutech.ac.jp

<sup>‡</sup>Corresponding Author; Akihiko Katsuki, Next Generation Switching Power Course, Faculty of Engineering, Nagasaki University, 1-14, Bunkyo-machi, Nagasaki, 852-8521 Japan, Tel: +81 95 819 2692, Fax: +81 95 819 2692, katsuki@nagasaki-u.ac.jp

*Received: 21.06.2014 Accepted: 19.07.2014*

**Abstract-** A new CV (Constant-Voltage) CC (Constant-Current) ac power regulator is proposed. Our original Variable Capacitance Device of linear reactance device is utilized in the power stage. This device makes almost no distortion. In this circuit, a sinusoidal output voltage and a high efficiency can be obtained. For the purpose of output voltage/current control and input power-factor correction, two Variable Capacitance Devices were adopted. Two dc-dc converters were used for high-speed driver of these devices. The unity input power factor can be obtained all over the constant-voltage region and the constant-current region. Input current of the proposed power supply becomes almost zero at no load and at short-circuit load.

**Keywords-** Variable Capacitance Device; ac power supply; no distortion; unity input power factor; dc-dc converter

## 1. Introduction

As constant-voltage ac power supply, ferroresonant circuits [1, 2] are well known. Ferroresonant circuits have advantage of the current limitation against short circuit and the absorption of noise flowing from ac line. However, waveform of output voltage is distorted, because the output voltage is controlled by nonlinear elements, e.g., saturable core or magnetic-saturation simulation circuit [3]. Therefore, an additional filter is needed for suppression of higher-harmonic voltages.

So, we proposed an entirely new type of ac voltage regulator [4]. This circuit makes no distortion of output voltage waveform, because only linear reactance devices are utilized in the power stage. To control output voltage, it is needed that inductance or capacitance can be varied. The inductance should be fixed so that the maximum load current may be limited at overloading. Here, our original Variable

Capacitance Device [5] was employed as linear capacitor. A low-power boost-type switched-mode PWM (Pulse Width Modulation) dc-to-dc converter was used as high-speed low-output-impedance driver of this device. It is a remarkable advantage that this converter delivers almost no power in the steady state.

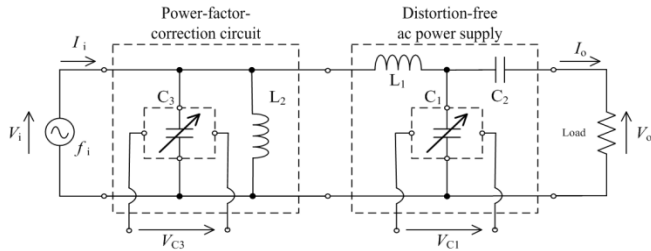
An additional Variable Capacitance Device made input power-factor correction possible except for light load [6]. Though the circuit proposed in [4] has an ability of overload protection, constant-current characteristics cannot be realized. So, we introduced a circuit technique to control the characteristics of load current limitation [7]. Moreover, power factor correction in the constant-current region was made possible [8].

In this paper, an advanced distortion-free constant-voltage constant-current ac power supply is proposed. This power supply is capable of perfect correction on input power

factor. In addition, the input power factor correction circuit brings remarkable feature. The input current becomes almost zero at no load as well as at short-circuit load.

**2. Power Stage**

Fig. 1 shows a basic circuit of power stage in the proposed power supply. In this figure,  $V_i$ ,  $I_i$ ,  $I_o$  and  $V_o$  represent the input voltage, the input current, the output current and the output voltage, respectively. The power stage of distortion-free constant-voltage constant-current ac power supply is arranged by a distortion-free ac power supply and a power-factor correction circuit.

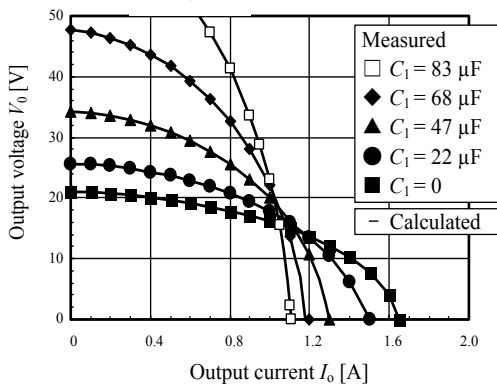


**Figure 1.** Power stage of the proposed distortion-free constant-voltage constant-current ac power supply using Variable Capacitance Devices.

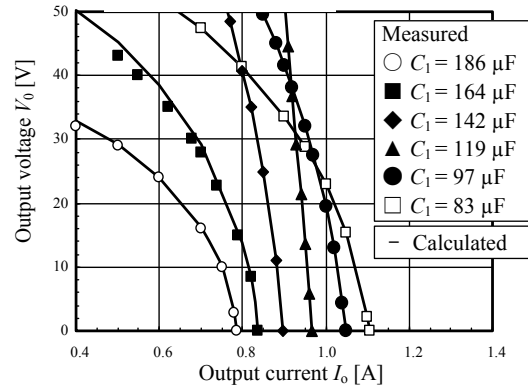
**3. Distortion-Free AC Power Supply**

Distortion-free ac power supply is constructed by the use of the inductor  $L_1$ , the capacitors  $C_1$  and  $C_2$ . Here, the capacitance  $C_1$  is variable. The load is assumed to be resistive. Characteristics of the distortion-free ac power supply are shown in Fig. 2 and Fig. 3. Fig. 2 is an example of output characteristics and Fig. 3 is that of input-output characteristics. For simplicity, measured values were obtained by using film capacitors as  $C_1$ . Equations for calculation have been given in [7]. The inductance of  $L_1$ , the loss resistance of  $L_1$ , the capacitance of  $C_2$ , and the operation frequency are  $L_1 = 58$  mH,  $r_1 = 0.6$   $\Omega$ ,  $C_2 = 290$   $\mu$ F, and  $f_i = 60$  Hz, respectively.

When  $I_o = 0$  (no load) and  $C_1 = 0$ , it is obvious from Fig. 1 that the output voltage  $V_o$  is equal to the input voltage  $V_i$ . Output characteristics depend on the input voltage. For example, the output voltage at no load or the output current at short-circuit load is proportional to the input voltage.

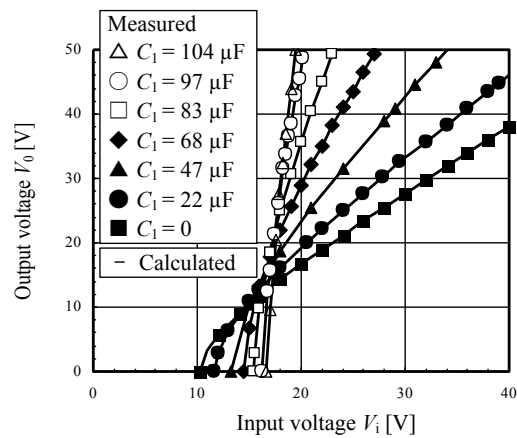


(a)  $0 \leq C_1 \leq 83 \mu\text{F}$ .

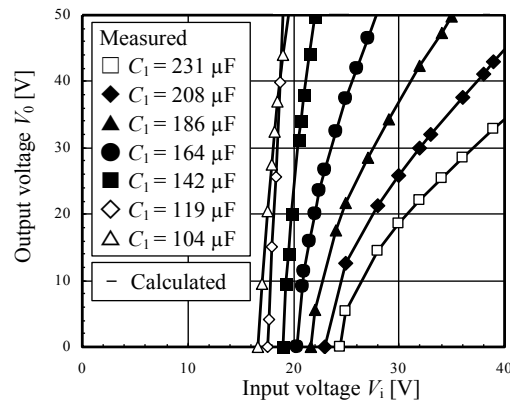


(b)  $C_1 \geq 83 \mu\text{F}$ .

**Figure 2.** Output ( $V_o$  vs.  $I_o$ ) characteristics of the distortion-free ac power supply, where  $V_i = 21$  V.



(a)  $0 \leq C_1 \leq 104 \mu\text{F}$ .



(b)  $C_1 \geq 104 \mu\text{F}$ .

**Figure 3.** Input-output ( $V_o$  vs.  $V_i$ ) characteristics of the distortion-free ac power supply, where  $I_o = 0.81$  A.

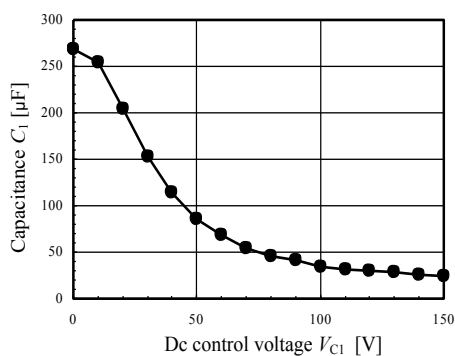
Therefore, when the input voltage  $V_i$  is selected to suitable value, we can see from Fig. 2(a) that a boost-type constant-voltage ac power supply can be constructed by the control of  $C_1$ . By utilizing the characteristics shown in Fig. 2(b), we can realize a constant-current ac power supply. Fig. 3 and other characteristics teach us the information on allowable value of  $V_i$ .

#### 4. Power-Factor Correction Circuit

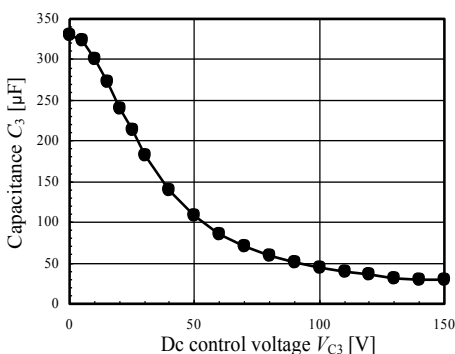
In Fig. 1, the capacitor  $C_3$  and the inductor  $L_2$  make an input-power-factor correction circuit. Here, the capacitance  $C_3$  is variable. Input power factor of the distortion-free ac power supply is leading when the load is light at the constant-voltage region. Therefore, it is supposed that  $L_2$  can make power-factor correction perfect. The inductance of  $L_2$  and the loss resistance of  $L_2$  are  $L_2 = 35 \text{ mH}$  and  $r_2 = 0.2 \Omega$ , respectively. These conditions are common through this paper. Experimental results will be presented in Chapter 8.

#### 5. Variable Capacitance Device

As a passive device capable of varying its capacitance, variable capacitance diode is well-known. However, operating current is up to about  $10 \mu\text{A}$ , because this device is a reverse-biased p-n junction diode. So, we proposed the Variable Capacitance Device for the purpose of dealing with a certain degree of power. Multilayered ceramic capacitors made of ferroelectric vary their capacitance with the dc bias voltage. The Variable Capacitance Device can be realized by utilizing these characteristics. Since well-balanced four capacitors are bridge-connected, ac leakage current flowing from the control voltage terminals is extremely small. Employment of low-output-impedance driver makes high-speed operation possible. The circuit symbol of the four-terminal Variable Capacitance Device is shown in Fig. 1.



(a)  $C_1$ .



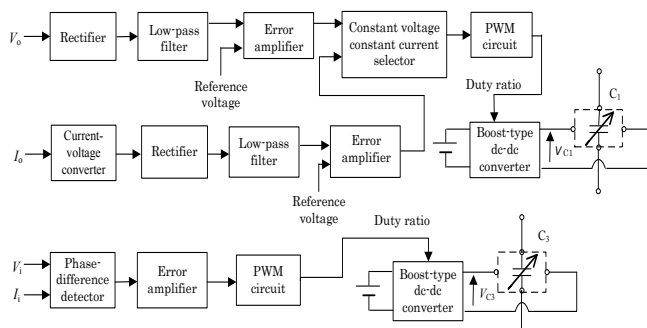
(b)  $C_3$ .

**Figure 4.** Control characteristics of the Variable Capacitance Devices  $C_1$  and  $C_3$ .

Measured characteristics of the capacitances  $C_1$  and  $C_3$  are presented at Fig. 4, where  $V_{C1}$  and  $V_{C3}$  are the dc control voltages.

#### 6. Control Circuit

An example of the block diagram of the feedback control circuit is shown in Fig. 5. One control path from  $V_o$  and  $I_o$  to  $V_{C1}$  was introduced to keep the output voltage or the output current constant. Next, the other control path from  $V_i$  and  $I_i$  to  $V_{C3}$  was introduced to maintain the unity input power factor.



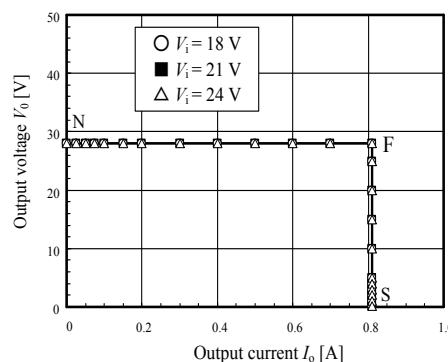
**Figure 5.** Control circuit of the proposed distortion-free constant-voltage constant-current ac power supply using Variable Capacitance Devices.

#### 7. Control Circuit Distortion-Free Constant-Voltage Constant-Current AC Power Supply Having The Unity Input Power Factor

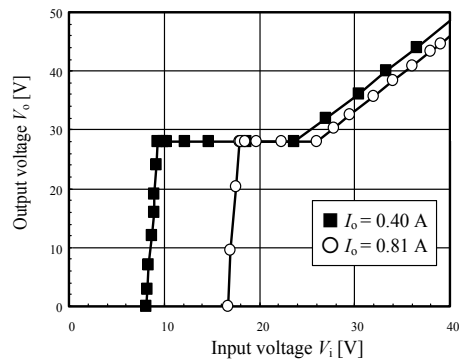
Fig. 6 presents the output ( $V_o$  vs.  $I_o$ ) characteristics of the constant-voltage constant-current ac power supply. Here, the points “N,” “F,” and “S” mean “No load,” “Full load,” and “Short-circuit load,” respectively. Next, Fig. 7 is an example of the input-output ( $V_o$  vs.  $V_i$ ) characteristics in the constant-voltage region. The minimum value of  $C_1$  was limited to  $22 \mu\text{F}$  by the control circuit.

#### 8. Input Power Factor and Input Current

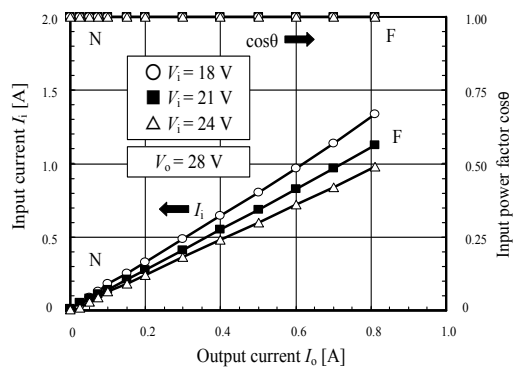
Observed characteristics of input power factor  $\cos\theta$  and input current  $I_i$  vs. output current  $I_o$  at the constant voltage region are shown in Fig. 8(a). With respect to the constant current region, experimental results of  $\cos\theta$  and  $I_i$  vs. output voltage  $V_o$  characteristics are shown in Fig. 8(b). It is seen that input power factor is perfectly corrected.



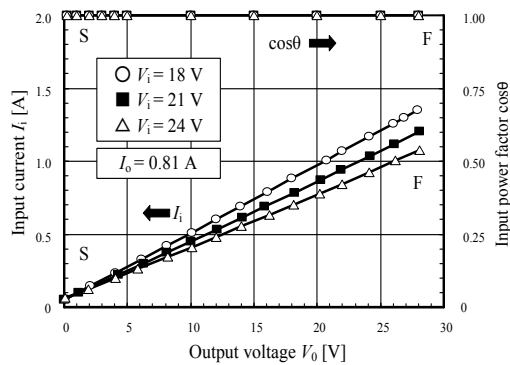
**Figure 6.** Measured output ( $V_o$  vs.  $I_o$ ) characteristics of the distortion-free constant-voltage constant-current ac power supply.



**Figure 7.** Measured input-output ( $V_o$  vs.  $V_i$ ) characteristics of the distortion-free constant-voltage constant-current ac power supply.



(a) Constant-voltage region.



(b) Constant-current region.

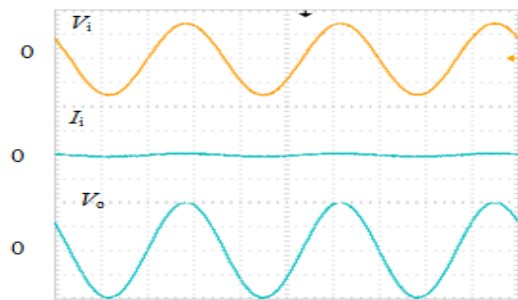
**Figure 8.** Measured characteristics of the input power factor  $\cos\theta$  and the input current  $I_i$ .

In addition, the power factor correction circuit makes the input current much smaller. Especially, the input current  $I_i$  becomes almost zero when the load is short circuited and open circuited.

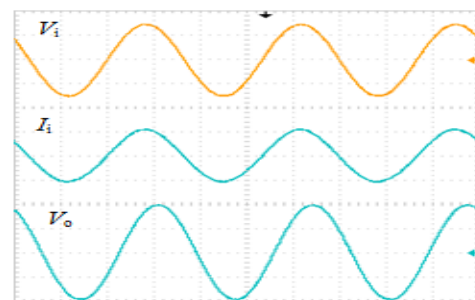
### 9. Waveforms

Fig. 9 and Fig. 10 show waveforms of the input voltage  $V_i$ , the input current  $I_i$ , and the output voltage  $V_o$  in the constant-voltage region. On the other hand, Fig. 11 and Fig. 12 are waveforms of  $V_i$ ,  $I_i$ , and the output current  $I_o$  in the constant-current region. In Fig. 9 and Fig. 11,  $V_i$  was amplified sinusoidal voltage. The commercial ac voltage in our laboratory was used as  $V_i$  in Fig. 10 and Fig. 12.

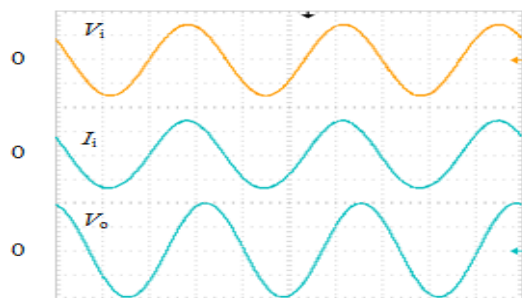
It is seen from Fig. 9 and Fig. 11 that the proposed power supply makes almost no distortion. Even if input voltage is distorted as Fig. 10 and Fig. 12, waveforms of output voltage or current become almost sinusoidal. In these figures,  $V_i$  is in phase with  $I_i$ .



(a)  $I_o = 0$  (no load).

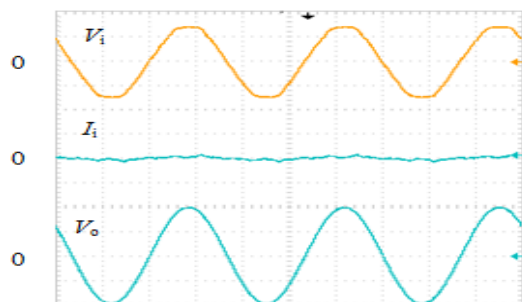


(b)  $I_o = 0.61$  A.

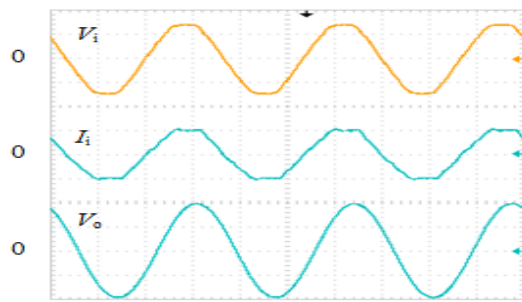


(c)  $I_o = 0.81$  A (full load).

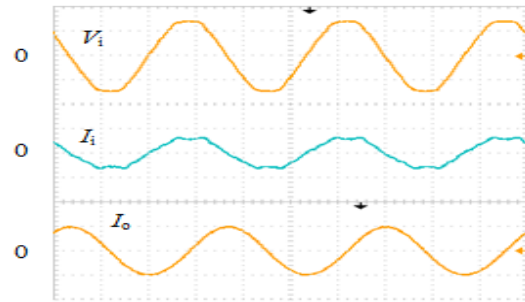
**Figure 9.** Observed waveforms of amplified sinusoidal input voltage  $V_i$ ,  $I_i$ , and  $V_o$  in the constant-voltage region ( $V_o = 28$  V), where  $V_i = 21$  V; vertical: 20 V/div for  $V_i$  and  $V_o$ , 1 A/div for  $I_i$ , horizontal: 5 ms/div.



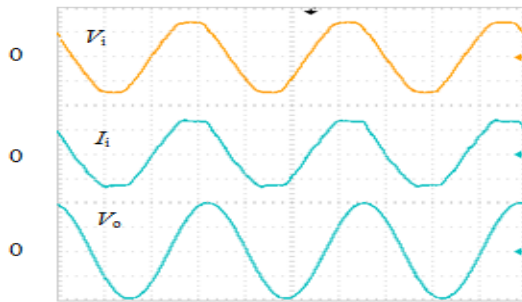
(a)  $I_o = 0$  (no load).



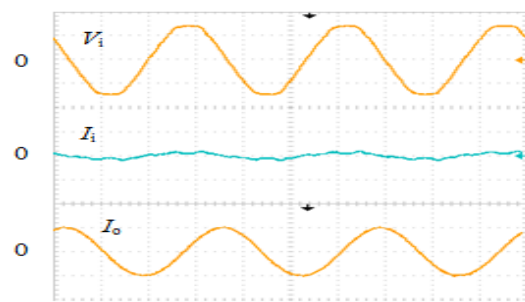
(b)  $I_o = 0.61$  A.



(a)  $V_o = 10$  V.



(c)  $I_o = 0.81$  A (full load).



(b)  $V_o = 0$  (short-circuit load).

**Figure 10.** Observed waveforms of commercial ac input voltage  $V_i$ ,  $I_i$ , and  $V_o$  in the constant-voltage region ( $V_o = 28$  V), where  $V_i = 21$  V; vertical: 20 V/div for  $V_i$  and  $V_o$ , 1 A/div for  $I_i$ , horizontal: 5 ms/div.

**Figure 12.** Observed waveforms of commercial ac input voltage  $V_i$ ,  $I_i$ , and  $I_o$  in the constant-current region ( $I_o = 0.81$  A), where  $V_i = 21$  V; vertical: 20 V/div for  $V_i$ , 1 A/div for  $I_i$  and  $I_o$ , horizontal: 5 ms/div.

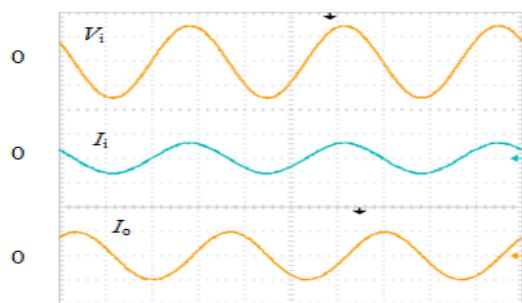
## 10. Conclusion

The proposed circuit can realize a power-factor-corrected constant-voltage constant-current ac power supply. It has the following features. (1) The unity input power factor is obtained all over the constant-voltage region and the constant-current region. (2) The input current is nearly zero at short-circuit load. (3) The input current is nearly zero at open-circuit load. (4) Waveform of output becomes almost sinusoidal against distorted input voltage.

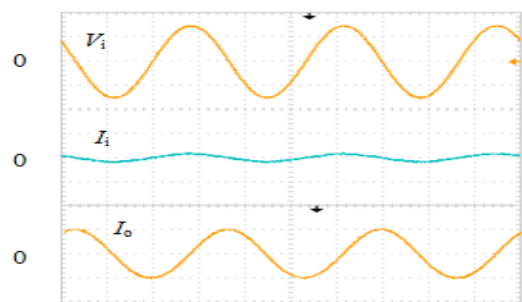
Two inductors  $L_1$  and  $L_2$  can be assembled into one transformer. By introducing a transformer, voltage compensation against boost-type characteristics is simultaneously solved including isolation.

## References

- [1] T. Hasumi, Applications of Ferroresonance, Ohm-sha, Tokyo, 1952. (in Japanese)
- [2] C. Hayashi, Nonlinear Oscillations in Physical Systems, McGraw-Hill, New York, 1964.
- [3] R. J. Kakalec, "A Feedback-Controlled Ferroresonant Voltage Regulator," IEEE Transactions on Magnetics, Vol. MAG-6, pp. 4-8, March 1970.
- [4] A. Katsuki, H. Iwata, and T. Matsui, "Distortion-Free Regulated AC Power Supply Using Variable Capacitance Device," Proceedings of PCC'97 (The 2nd Power Conversion Conference), pp. 347-354, August 1997.



(a)  $V_o = 10$  V.



(b)  $V_o = 0$  (short-circuit load).

**Figure 11.** Observed waveforms of amplified sinusoidal input voltage  $V_i$ ,  $I_i$ , and  $I_o$  in the constant-current region ( $I_o = 0.81$  A), where  $V_i = 21$  V; vertical: 20 V/div for  $V_i$ , 1 A/div for  $I_i$  and  $I_o$ , horizontal: 5 ms/div.

- [5] K. Harada, A. Katsuki, M. Fujiwara, H. Nakajima, and H. Matsushita, "Resonant Converter Controlled by Variable Capacitance Device," IEEE Transactions on Power Electronics, Vol. 8, No. 4, pp. 404-410, October 1993.
- [6] A. Katsuki, S. Ishimaru, and T. Arai, "Power-Factor-Corrected Distortion-Free Regulated AC Power Supply Using Variable Capacitance Devices," Proceedings of INTELEC'99 (The 21st International Telecommunications Energy Conference), No. 31-43, June 1999.
- [7] A. Katsuki and T. Arai, "Distortion-Free Constant-Voltage Constant-Current AC Power Supply Using Variable Capacitance Device," Proceedings of IPEC'00 (The 4th International Power Electronics Conference), pp. 1704-1710, April 2000.
- [8] A. Katsuki, T. Arai, and M. Matsushima, "Power-Factor-Corrected Distortion-Free Constant-Voltage Constant-Current AC Power Supply Using Variable Capacitance Devices," Proceedings of PCC'02 (The 3rd Power Conversion Conference), pp. 933-940, April 2002.